

*NASA CR-165,932*

## NASA Contractor Report 165932

NASA-CR-165932  
19820021412

# Development of Flying Qualities Criteria for Single-Pilot Instrument Flight Operations: Interim Report

Aharon Bar-Gill, W. Barry Nixon  
and George E. Miller

FLIGHT RESEARCH LABORATORY  
PRINCETON UNIVERSITY  
Princeton, N.J. 08544

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June 1982

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National Aeronautics and  
Space Administration

Langley Research Center  
Hampton, Virginia 23665  
AC 804 827-3966



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N82-29288 #

### ABSTRACT

Research is being conducted to develop flying qualities criteria for Single Pilot Instrument Flight Rule (SPIFR) operations. Significant progress has been made with regard to most of the key issues encompassed in the SPIFR research program. The ARA aircraft has been modified and adapted for SPIFR operations. Aircraft configurations to be flight-tested have been chosen and matched on the ARA in-flight simulator, implementing modern control theory algorithms. Mission planning and experimental matrix design have been completed. Microprocessor software for the onboard data acquisition system has been debugged and flight-tested. Flight-path reconstruction procedure and the associated FORTRAN program are at a final stage of development. Work has begun on algorithms associated with the statistical analysis of flight test results and the SPIFR flying qualities criteria deduction.

## PREFACE

This investigation is being conducted by the Flight Research Laboratory at Princeton University, Princeton, New Jersey under Contract No. NAS1-15764 for the NASA Langley Research Center. This is the first annual technical report, and it reflects the SPIFR research effort through May 1981.

The principal investigator for the study is Professor Robert F. Stengel. He is assisted by W. Barry Nixon, senior technical staff member, George E. Miller, technical staff member, Aharon Bar-Gill, graduate student, Thomas O. Williams, technical staff member, Barton C. Reavis, technical associate and electronic technicians Louis Pokrocos, Thomas Frobose and Karl Thomas.

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## LIST OF SYMBOLS

<u>Variables</u>	<u>Description</u>
$\underline{a}_B$	acceleration vector in body axes, "g"
$a_x, a_y, a_z$	cartesian components of $\underline{a}_B$ , "g"
C	implicit model following gain matrix
F	system dynamics matrix
$\underline{f}$	nonlinear functions for vehicle equations of motion
G	control effects matrix
g	gravitational acceleration, ft/sec <sup>2</sup>
H	observation matrix
	transformation matrix
h	altitude, ft
$\underline{h}$	nonlinear measurement functions
I	identity matrix
K	Kalman gain matrix
L	transformation matrix
M ( )	pitch moment stability-and-control derivative
n ( )	random noise associated with the ( ) variable
P	state covariance matrix
p	roll rate, deg/sec
Q	process noise covariance matrix
q	pitch rate, deg/sec
R	measurement noise covariance matrix
r	yaw rate, deg/sec
S	intermediate command output matrix
s	Laplace transform variable
T	duration of flight segment to be reconstructed, sec

$t$	time, sec
$u$	x-axis velocity, ft/sec
$\underline{u}$	control vector
$\underline{V}_{\text{air}}$	airspeed vector, ft/sec
$v$	y-axis velocity, ft/sec
$\underline{v}$	measurement noise
$w$	z-axis velocity, ft/sec
$\underline{w}$	process noise vector
$\underline{W}_I$	wind vector in inertial frame, ft/sec
$X( )$	(aerodynamic + thrust)-force along the x-axis derivative
$x_I$	axial position in inertial frame, ft
$\underline{x}$	state vector
$y_I$	lateral position in inertial frame, ft
$\underline{y}$	command vector
$Z( )$	(aerodynamic + thrust)-force along the z-axis derivative
$z_I$	vertical position in inertial frame, ft
$\underline{z}$	observation vector

#### Variables (Greek)

$\alpha$	angle of attack, deg
$\beta$	angle of sideslip, deg
$\delta E$	elevator deflection, deg
$\delta F$	flap deflection, deg
$\delta T$	throttle deflection, percent
$\theta$	pitch attitude angle, deg
$\Sigma$	summation
$\Phi$	state transition matrix
$\phi$	roll attitude angle, deg
$\psi$	yaw attitude angle, deg
$\tilde{\omega}$	body angular rate skew matrix
$\underline{\omega}$	angular rate vector

### Superscripts

B	transformation <u>to</u> body axes
I	transformation <u>to</u> inertial axes

### Subscripts

A	kinematic model A
ARA	Avionics Research Aircraft
B	body-axis frame <u>from</u> body axes (with transformation matrix) kinematic model B feedback backward filter
comm	commanded (desired) value
F	feed forward
I	inertial frame <u>from</u> inertial axes (with transformation matrix)
i	navigation station sequencing index
k	sampling instant index
M	model
o	nominal value
q	sensitivity to pitch rate
u	sensitivity to x-axis velocity
w	sensitivity to z-axis velocity
$\delta E$	sensitivity to elevator deflection
$\delta F$	sensitivity to flap deflection
$\delta T$	sensitivity to throttle deflection

### Punctuation

( $\dot{\phantom{x}}$ )	derivative of quantity with respect to time
( $\underline{\phantom{x}}$ )	vector quantity
$\delta( \ ) / \delta( \ )$	partial derivative of one variable with respect to another

$\Delta( )$	perturbation variable
$( )^*$	steady-state variable
$( )^T$	transpose of a vector or matrix
$( )^{-1}$	inverse of a matrix
$(\hat{ })$	estimated value of a variable
$( )^\#$	pseudoinverse of a matrix
$s( )$	$\sin( )$
$c( )$	$\cos( )$

### Acronyms

A/D	analog-to-digital
ADF	automatic direction finder
ARA	Avionics Research Aircraft
CDU	control-display unit
CHR	Cooper-Harper Rating
D/A	digital-to-analog
DME	distance measuring equipment
FBW	fly-by-wire
FRL	Flight Research Laboratory
GA	general aviation
GDOP	geometric dilution of precision
IAS	indicated airspeed
IFR	instrument flight rule
I/O	input/output
POR	pilot opinion rating
PROM	programmable read-only memory
RAM	random access memory
SBC	single-board computer
SPIFR	single-pilot instrument flight rule
TAS	true airspeed
VFR	visual flight rule
VOR	very-high-frequency omni-range



1.

## INTRODUCTION

### 1.1 BACKGROUND AND GOALS

This investigation of Single-Pilot Instrument Flight Rule (SPIFR) flying qualities criteria focuses on General Aviation (GA) operations. General Aviation plays an important role in this nation's transportation network (there are about 200,000 active GA aircraft, with the projected number for 1990 being about 300,000), but the difficulty of piloting and the inherent hazards associated with the SPIFR flight regime pose obstacles to continued growth of this mode of transportation (Ref. 1).

An important effect which contributes to an increased hazard for SPIFR operation is the low-frequency dynamic response of a GA aircraft, which does not have to comply with any federal aviation regulation (Ref. 2). As a result, most contemporary GA aircraft have, at best, a marginally stable phugoid mode which may become divergent under wind shear conditions (Ref. 3). This dynamic response problem generally can be coped with under VFR conditions, although it increases pilot's workload significantly. In typical commercial flight, the IFR workload is shared by two pilots; however, GA IFR flight often is controlled by a single pilot. Airframe dynamic deficiencies, finite capabilities of the human operator, and the often limited capabilities of communications and navigation equipment available in typical GA aircraft compound the flight problem under SPIFR conditions.

Prior research has addressed separately various issues, which coupled together, result in this unique flight mission/regime. For example, Ref. 4 and 5 look into the dynamic response

characteristics of GA aircraft, Ref. 6 presents the effect of advanced cockpit controls and displays, and Ref. 7 addresses the pilot workload issue. The SPIFR research initiated by the Flight Research Laboratory (FRL) at Princeton University is an integrated theoretical and flight test program, whose principal objectives are:

- To pursue the trends revealed in previous research,
- To develop new methodologies for analysis of complete SPIFR missions,
- To obtain statistically significant flying qualities criteria for single-pilot instrument flight operations.

## 1.2 ORGANIZATION OF THE REPORT

Chapter 2 describes the preparation of the ARA for SPIFR mission flights and the onboard experimental setup -- in particular, the hardware and software aspects associated with the data acquisition process. Chapter 3 presents theoretical aspects of the SPIFR research, including modern estimation and control theory algorithms for in-flight simulation and flight path reconstruction. Chapter 4 refers to preliminary flights and to the post-flight data preprocessing procedure verification. Conclusions are contained in Chapter 5. The four appendices contain additional theoretical derivations, program listings for onboard and post-flight processing, description of computer systems employed in this research, and the hardware scheme of the unique DME integration into the SPIFR experimental setup.



## 2. AIRCRAFT AND DATA ACQUISITION SYSTEM PREPARATION

This chapter describes the preparation of the in-flight simulator and of the onboard digital data acquisition system for SPIFR flight testing. Extensive engineering and technical effort was required for aircraft modifications and rewiring, for new avionics system installation, and for onboard experimental setup integration. The results of this effort are summarized in the following sections.

### 2.1 AIRCRAFT SYSTEM MODIFICATIONS

The Avionics Research Aircraft (ARA) is a Ryan Navion (N5113K) that has been modified into a fly-by-wire (FBW), variable-stability aircraft (Fig. 2-1). It is capable of simulating a variety of other aircraft using feedback control and command augmentation. The ARA is equipped to measure attitude, angular rates, and linear accelerations in three axes, aerodynamic angles ( $\alpha$ ,  $\beta$ ), airspeed, altitude, and a number of other flight variables. Details of the ARA FBW system can be found in Ref. 8.

The evaluation pilot is to fly a SPIFR mission with the ARA responding as a desired configuration. In an emergency, the safety pilot can override the FBW system and take direct control of the aircraft, (Fig. 2-2).

To be used with the SPIFR program, the ARA had to undergo extensive modifications:

- Design and installation of a modular instrument panel.
- Acquisition and installation of a modern navigation/communication instrument package.
- Addition of secondary workload devices in the cockpit.

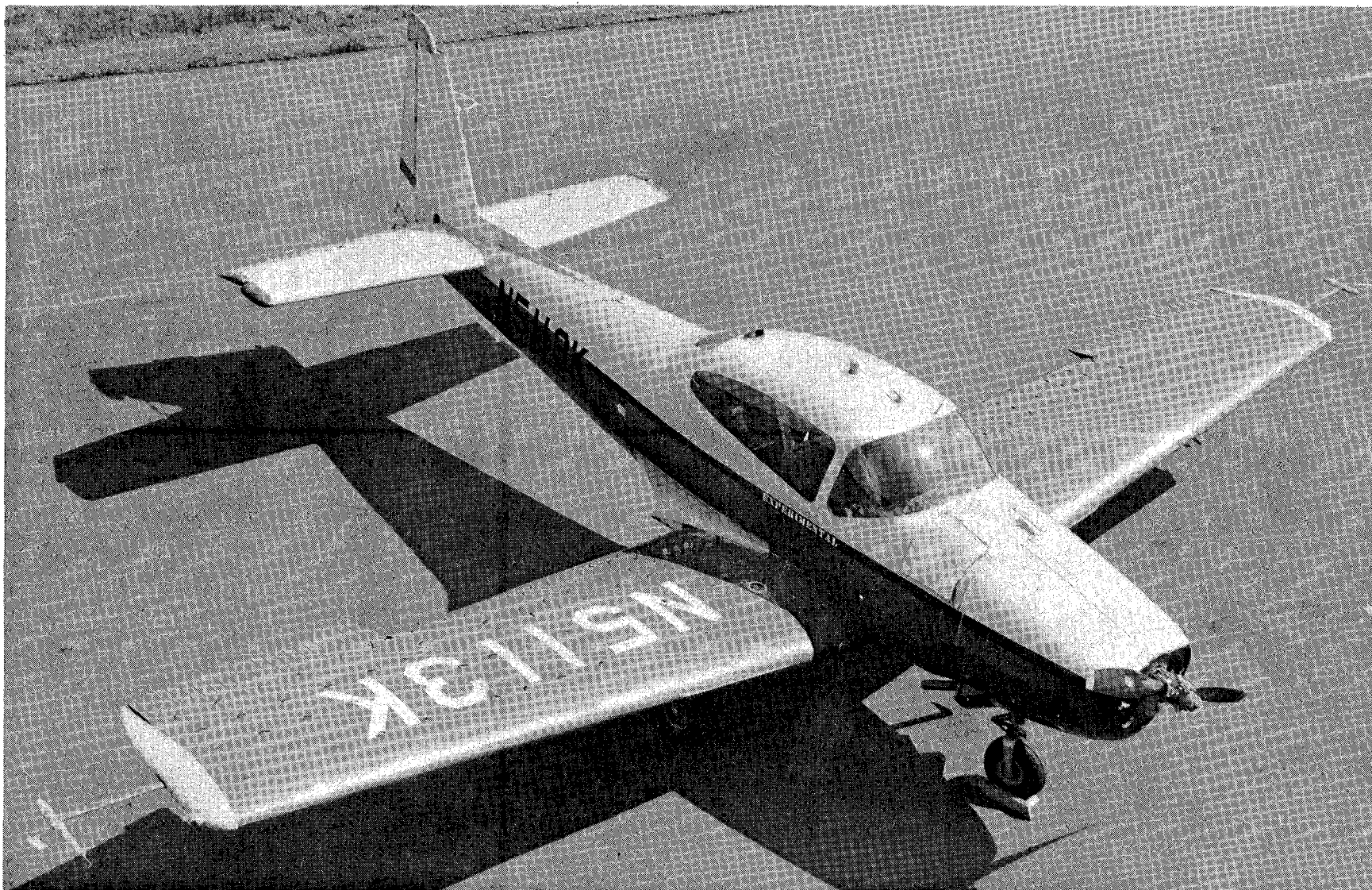


Figure 2-1. Avionics Research Aircraft, Navion N5113K.

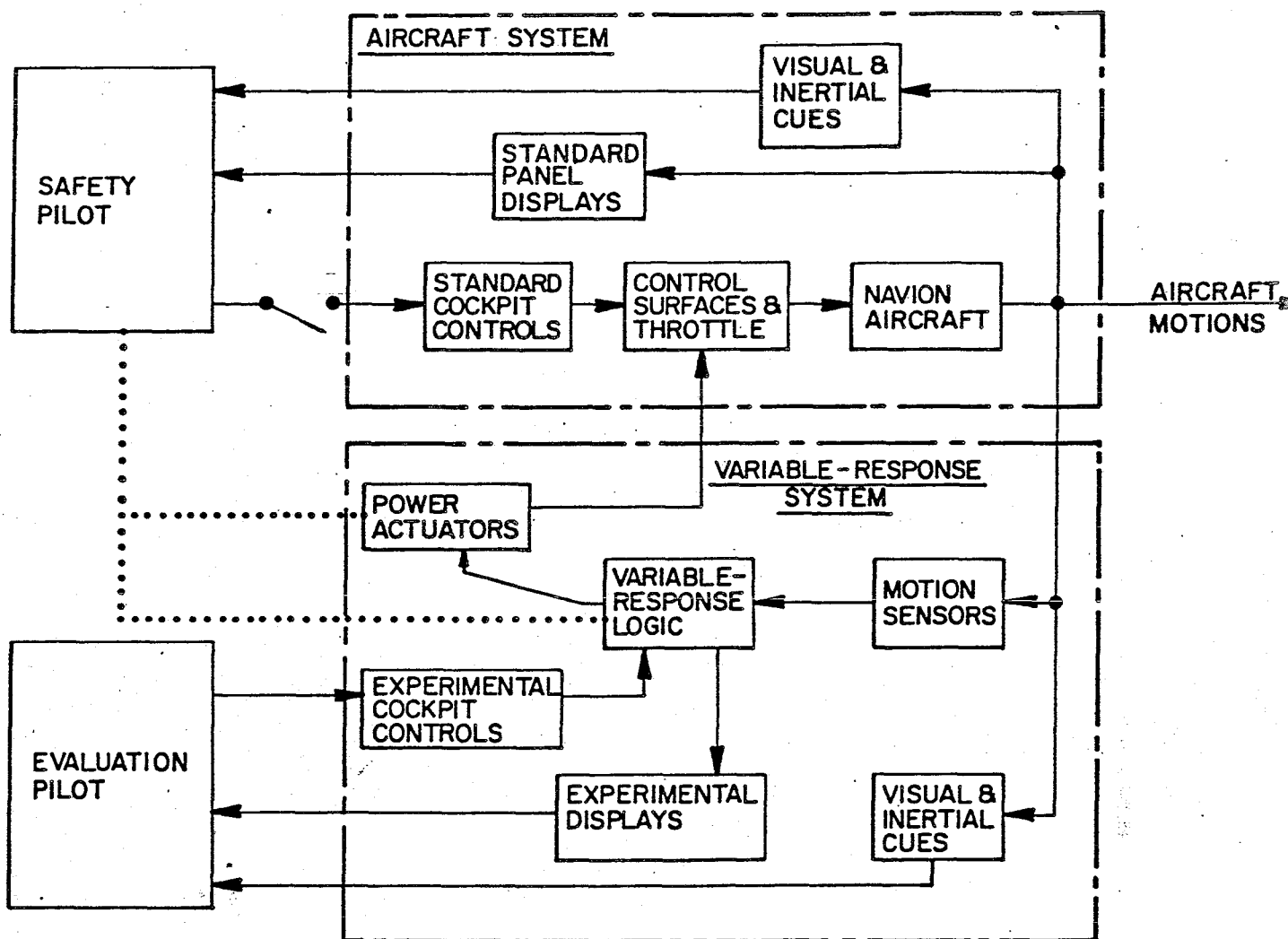


Figure 2-2. Overview of the ARA in-flight Simulator System.

Figure 2-3 illustrates the ARA's modular display panel configuration, with the evaluation pilot's station on the left, the safety pilot's station on the right, and the Bendix BX-2000 navigation/communication stack separating the two. The Distance Measuring Equipment (DME) readout is mounted on a switching panel at the top of the radio stack. The Very-high-frequency Omni-Range (VOR) navigation/communication unit is located under the switching panel. The blank space below this unit is reserved for the Automatic Direction Finder (ADF) and for the transponder.

The DME unit has been integrated into the onboard experimental setup, maintaining the capability to sequence the available navigational stations automatically (through microprocessor control). The importance of this option is discussed in Section 3.5. The technical implementation details are presented in Appendix D.

The safety pilot's panel is a permanent fixture, with conventional instruments and elements for control of the variable-stability system. The latter occupy the right side of the panel and the lower and middle consoles. The evaluation pilot's panel can be removed as a unit to facilitate installation of alternate panels for other investigations. Secondary workload meters, lights, and switches also have been added to the panel.

The secondary workload meters are additional instruments slaved to the onboard microprocessor, which occasionally forces the needles into their "red zones". The evaluation pilot is instructed to keep them "green". Alternately, the pilot can be asked to extinguish lights turned on (pseudo-randomly) by the microprocessor program. It is also possible to

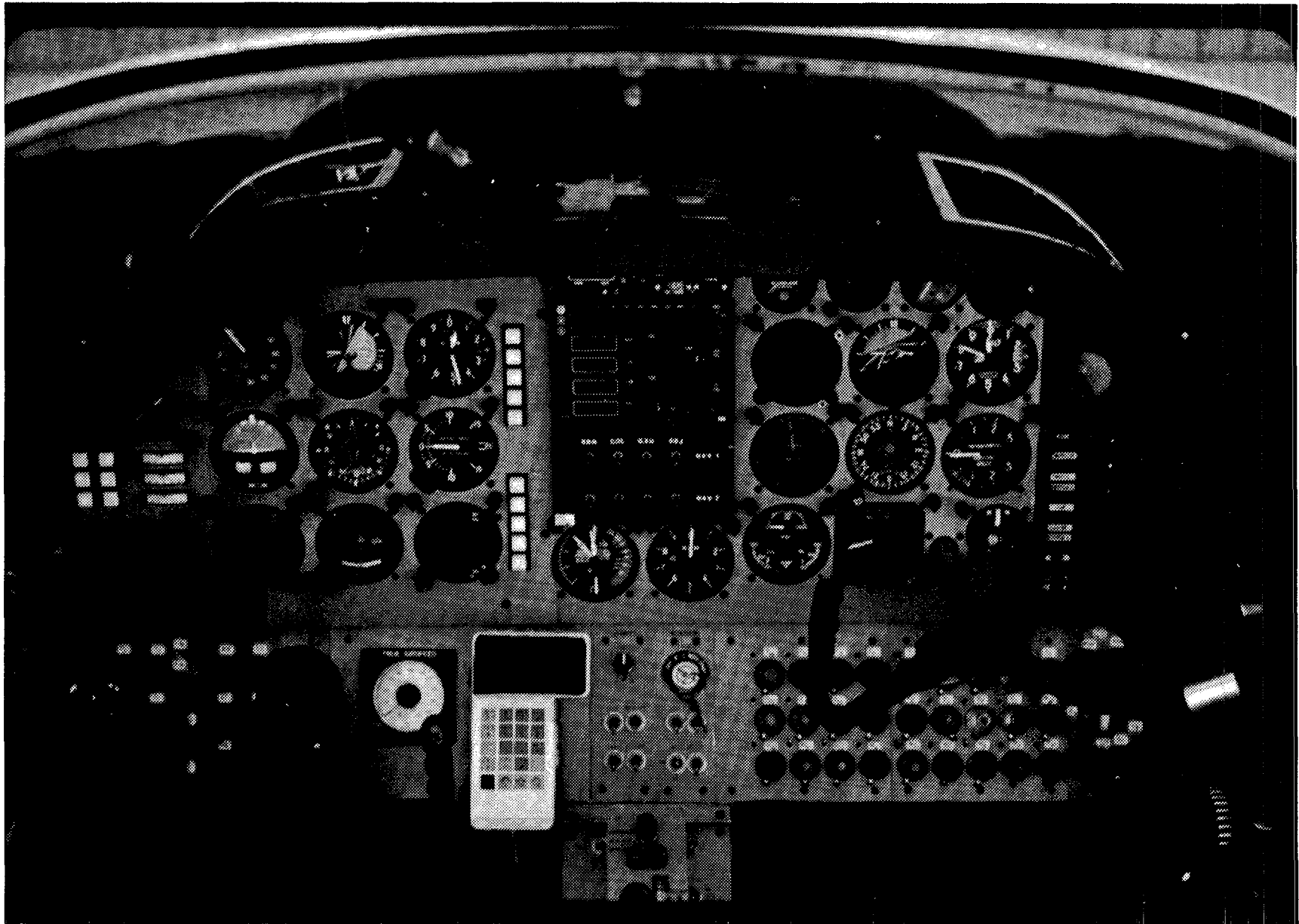


Figure 2-3. Cockpit Displays of the Avionics Research Aircraft. Modular SPIFR Evaluation Pilot Panel at Left.

simulate typical communications workload by blending audio inputs from a pre-recorded tape with specific instructions radioed from the ground on the flight test frequency.

## 2.2 INSTRUMENTATION AND DATA RECORDING SYSTEM

The SPIFR digital data acquisition system is illustrated in Fig. 2-4. It is built around the SPIFR microcomputer, which uses the Z-80A central processing unit and the Am9511 mathematics processor in a Multibus<sup>TM</sup> architecture. As currently configured, the SPIFR microcomputer contains 48K bytes of RAM (random access memory) and 16K bytes of PROM (programmable read-only memory). It accepts 32 analog inputs and produces 6 analog outputs.

The ARA's safety pilot communicates with the SPIFR Microcomputer through a hand-held control/display unit (CDU), the Termiflex HT/4. The pilot is able to start and stop processing or recording through the CDU, change stored numerical values, and so on. Conversely, the CDU can display internally triggered error messages to the safety pilot. The evaluation pilot normally is unaware of the SPIFR Microcomputer's operation, other than through secondary workload stimuli and responses.

Analog and digital inputs and outputs shown in Fig. 2-4 are, for the most part, self-explanatory. Tables 2-1 and 2-2 contain lists of inputs and outputs. The SPIFR Microcomputer obtains its analog inputs from the Digital Avionics Research System (DARE) junction box (J-Box) previously installed in the ARA for another Langley Research Center program. Thus, there is a high degree of "plug compatibility" between the SPIFR and DARE programs.

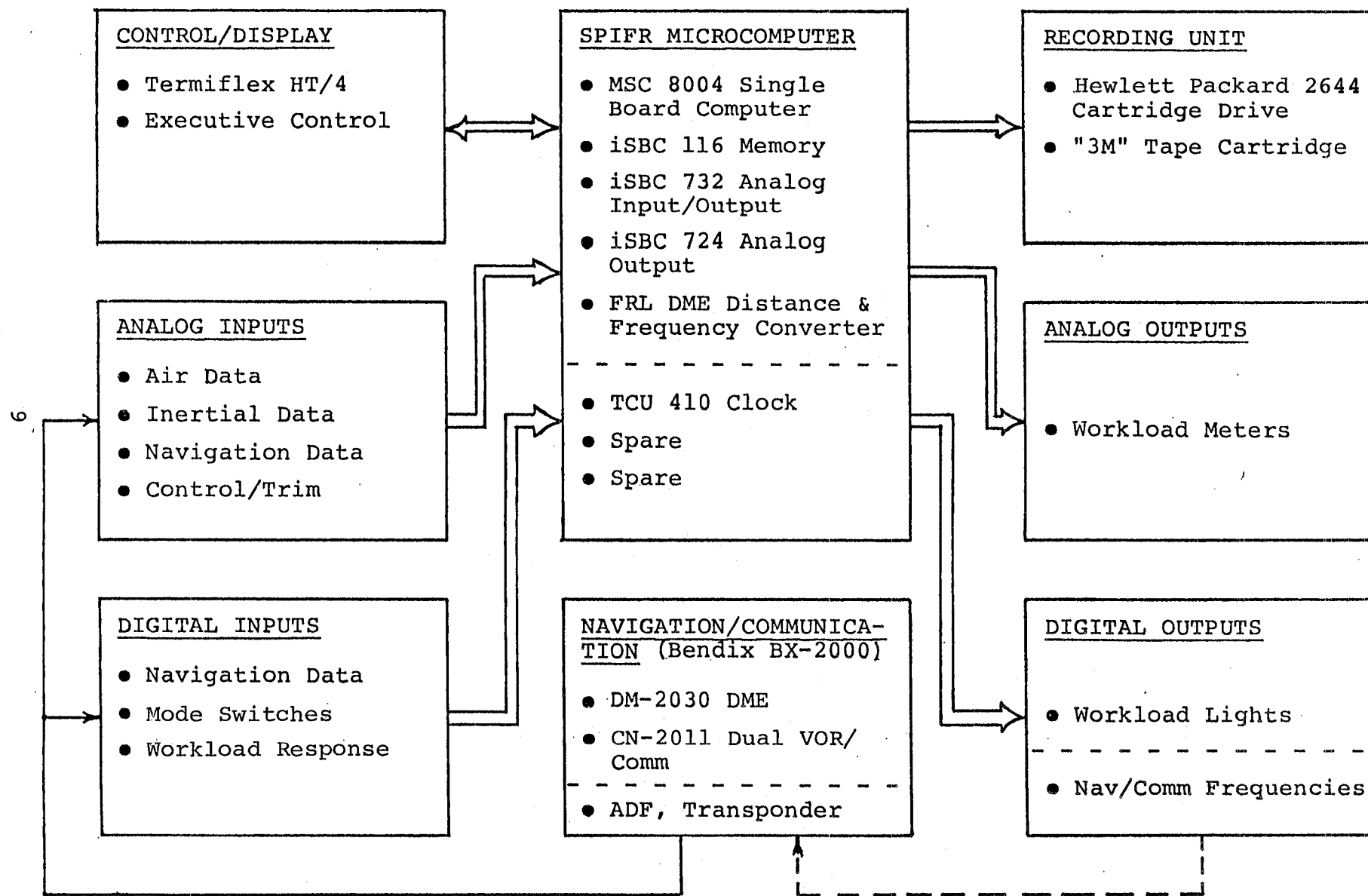


Figure 2-4. SPIFR Digital Data Recording System.

TABLE 2-1  
Input Assignments For  
SPIFR Digital Data Recording System

Analog Inputs

- |                         |                                |
|-------------------------|--------------------------------|
| 1. Control Column Angle | 17. Yaw Trim                   |
| 2. Throttle Setting     | 18. Normal Acceleration        |
| 3. Flap Command         | 19. Axial Acceleration         |
| 4. Angle of Attack      | 20. Lateral Acceleration       |
| 5. Pitch Angle          | 21. VOR#1 Azimuth              |
| 6. Pitch Rate           | 22. VOR#2 Azimuth              |
| 7. Airspeed             | 23. Glide Slope Elevation      |
| 8. Control Wheel Angle  | 24. MLS Azimuth                |
| 9. Foot Pedals          | 25. MLS Elevation              |
| 10. Sideslip Angle      | 26. Radar Altitude             |
| 11. Roll Angle          | 27. Barometric Altitude        |
| 12. Yaw Angle           | 28. Stick Force (3rd Year)     |
| 13. Roll Rate           | 29. Simulated Turbulence Level |
| 14. Yaw Rate            | 30. Landing Gear               |
| 15. Pitch Trim          | 31. Wind Shear                 |
| 16. Roll Trim           | 32. System Engage              |

Digital Inputs

- |                    |                                     |
|--------------------|-------------------------------------|
| 1. DME Distance    | 6. Barometric Altitude              |
| 2. VOR#1 Frequency | 7. ADF Bearing                      |
| 3. VOR#2 Frequency | 8. Variable-Stability System Status |
| 4. DME Frequency   | 9. Pilot Mode Switches (8)          |
| 5. Time            | 10. Avionics System Status (8)      |



TABLE 2-2  
Output Assignments For  
SPIFR Digital Data Recording System

Analog Outputs

- |                                |          |
|--------------------------------|----------|
| 1. Secondary workload meter #1 | 4. Spare |
| 2. Secondary workload meter #2 | 5. Spare |
| 3. Secondary workload meter #3 | 6. Spare |

Digital Outputs

- |                          |                                  |
|--------------------------|----------------------------------|
| 1. DME tuning            | 4. Avionics System status lights |
| 2. DME station indicator |                                  |
| 3. Pilot workload lights | 5. Tape recorder                 |

A presampling filter (16 Hz break-point frequency) has been introduced for each analog channel to filter out the engine-vibration-induced noise.

Figure 2-4 also illustrates the digital radio tuning feature that will be put to use during the second phase of the project. Error budget analyses conducted during the first phase confirmed the superiority of DME over VOR for position fixing, even at the short ranges to be used in our flight tests. Consequently, it is advantageous to substitute multiple DME measurements for VOR measurements in flight data reduction. The BX-2000 DME unit can acquire and lock on a new station in considerably less than one second; this feature will be used in DME-only "round-robin" position fixing for flight path determination.

The digital tape recording unit is the Hewlett Packard (HP) 2644 terminal, which houses two DC100A magnetic tape cartridge drive units. Its built-in memory enables transition from one cartridge to the other without losing any information. Such a pair of cartridges has a storage capability of about 220K bytes, which is more than enough for a complete SPIFR mission run.

To accommodate the complete experimental setup, a pallet to fit into the ARA-aircraft behind the pilots' seats has been designed and built by the FRL technical staff. It weighs 215 lb. and uses the same mounting brackets as the DARE pallet.

### 2.3 SOFTWARE DEVELOPMENT

The SPIFR program focuses on the low-frequency dynamic response of the airframe and on navigation-related information,

whose rate of change is low as well. On the other hand, as discussed in Section 3.5, simulated SPIFR flight duration has to be about 30 min, during which all the data channels have to be recorded at least every second. Thus, the main objectives of the onboard software design are to:

- Sample the analog data at a high enough rate to avoid aliasing.
- Compress the high frequency data so that the most significant flight test information can be recorded efficiently with minimal error.
- Trigger preprogrammed sequences of the secondary workload devices (lights, dummy meters).
- Enable the safety pilot to operate the data acquisition system via the hand-held CDU.

The information recorded in flight can be separated into "slow" and "fast" variables. The "slow" variables are principally the positional measurements, which can be sampled once per second with minimal aliasing effect. The "fast" variables -- for example, angular rates and linear accelerations -- are sampled 10 times per second. For the sake of data compaction, they are averaged and recorded once each second. The simple averaging process is analogous to "low-pass" filtering. Thus, low-frequency information is passed with little modification, while high-frequency signals are attenuated.

The HP 2644's recording format uses 16-bit binary words. The SBC 732 A/D board is designed to fill in the 12 left-most bit positions of a 16-bit field, and an appropriate shift is performed to comply with the standard output format. Appendix B contains additional detail with regard to the software aspects of the SPIFR onboard data acquisition system, plus the complete listing of the microprocessor assembly program.

## 3.

THEORETICAL ASPECTS OF EXPERIMENT  
DESIGN AND FLIGHT PATH RECONSTRUCTION

This chapter starts with the presentation of the 6-DOF dynamic model of aircraft motion, as it is applied in the subsequent sections. Section 3.2 discusses the output command algorithm and its implementation to set up a priority list of aircraft configurations to be simulated in the first SPIFR flight test series. The experimental matrix design, based on statistical reasoning, follows in Section 3.3; the application of the chosen configurations on the ARA-in-flight simulator, via the implicit model following algorithm appears in Section 3.4. SPIFR mission planning (Section 3.5) is based mainly on mathematical-statistical modeling of the en-route navigational errors. Finally, the algorithm for post-flight optimal smoothing and flight path reconstruction is presented in Section 3.6.

## 3.1 AIRCRAFT DYNAMIC MODEL

The general formulation of a nonlinear dynamic model of a system is:

$$\dot{\underline{x}} = \underline{f}(\underline{x}, \underline{u}) \quad (3-1)$$

where  $\underline{x}$  is the state vector and  $\underline{u}$  is the control vector. The state vector  $\underline{x}$  used here contains three components each of translational rate ( $u, v, w$ ), translational position ( $x_I, y_I, z_I$ ), angular rate ( $p, q, r$ ) and angular attitude ( $\phi, \theta, \psi$ ). Both body and inertial axis frames are taken right-handed and with  $z$  pointing downward. The translational rate equation of the aircraft mathematical model is:

$$\dot{\underline{V}}_{\text{air}} = \underline{a}_B + \tilde{\omega} \underline{V}_{\text{air}} + H_{I-I}^B \underline{g}_I \quad (3-2)$$

The airspeed, expressed in body axes, is:

$$\underline{v}_{\text{air}} = [u \ v \ w]^T \quad (3-3)$$

Acceleration, expressed in body axes, is:

$$\underline{a}_B = [a_x \ a_y \ a_z]^T \quad (3-4)$$

The angular rate cross-product-equivalent matrix  $\tilde{\omega}$  is defined as:

$$\tilde{\omega} \triangleq \begin{bmatrix} 0 & r & -q \\ -r & 0 & p \\ q & -p & 0 \end{bmatrix} \quad (3-5)$$

The gravity vector in an assumed local level/local north inertial axis system is:

$$\underline{g}_I \triangleq [0 \ 0 \ g]^T \quad (3-6)$$

The transformation matrix  $H_I^B$  from inertial (I) to body (B) axes, with  $[\psi \ \theta \ \phi]$  Euler rotations in the specified order, is:

$$H_I^B \triangleq \begin{bmatrix} c\psi c\theta & s\psi c\theta & -s\theta \\ c\psi s\theta s\phi - s\psi c\phi & s\psi s\theta s\phi + c\psi c\phi & c\theta s\phi \\ c\psi s\theta c\phi + s\psi s\phi & s\psi s\theta c\phi - c\psi s\phi & c\theta c\phi \end{bmatrix} \quad (3-7)$$

where

$$\begin{aligned} s( ) &\triangleq \sin( ) \\ c( ) &\triangleq \cos( ) \end{aligned} \quad (3-8)$$

The second equation of the aircraft motion 6-DOF mathematical model describes the transformation of body-axis rates to Euler angle rates, and it is

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = L_B^I \begin{bmatrix} p \\ q \\ r \end{bmatrix} \quad (3-9)$$

where

$$L_B^I \triangleq \frac{1}{c\theta} \begin{bmatrix} c\theta & s\theta s\phi & s\theta c\phi \\ 0 & c\theta c\phi & -c\theta s\phi \\ 0 & s\phi & c\phi \end{bmatrix} \quad (3-10)$$

The third aircraft equation combines the effects of airspeed  $V_{\text{air}}$  and of the wind vector  $\underline{W}_I$  (expressed in inertial axes) to compute translational rate:

$$\dot{\underline{x}}_I = H_{B\text{-air}}^I V_{\text{air}} + \underline{W}_I \quad (3-11)$$

where  $\underline{x}_I$  is the position vector expressed in inertial axes:

$$\underline{x}_I \triangleq [x_I \ y_I \ z_I]^T \quad (3-12)$$

Based on the orthonormality of  $H_I^B$  in eq. (3-7):

$$H_B^I = (H_I^B)^{-1} = (H_I^B)^T \quad (3-13)$$

The following relationships constitute the algebraic part of the model, yielding the output or the measurement models. The airspeed absolute value is:

$$|\underline{V}_{\text{air}}| = (u^2 + v^2 + w^2)^{1/2} \quad (3-14)$$

The angle of attack is given by:

$$\alpha = \tan^{-1}\left(\frac{w}{u}\right) \quad (3-15)$$

The sideslip angle is:

$$\beta = \tan^{-1}\left(\frac{v}{u}\right) \quad (3-16)$$

The definition of the aerodynamic angles with respect to body axes is compatible with the actual measurement mechanization in the ARA.\* Assuming that the origin of the inertial frame is at sea level, the altitude  $h$  is:

$$h = -z_I \quad (3-17)$$

The acceleration vector  $\underline{a}_B$  of eq. (3-2) and (3-4) reflects the effect of aerodynamic and thrust forces, which act on the airframe. For example, the linearized version of eq. (3-1) for the longitudinal case is:

$$\begin{bmatrix} \Delta \dot{u} \\ \Delta \dot{w} \end{bmatrix}_{\underline{a}_B} = \begin{bmatrix} X_u & X_w & X_q \\ Z_u & Z_w & Z_{\dot{w}} \end{bmatrix} \begin{bmatrix} \Delta u \\ \Delta w \\ \Delta q \end{bmatrix} + \begin{bmatrix} X_{\delta E} & X_{\delta T} & X_{\delta F} \\ Z_{\delta E} & Z_{\delta T} & Z_{\delta F} \end{bmatrix} \begin{bmatrix} \Delta \delta E \\ \Delta \delta T \\ \Delta \delta F \end{bmatrix} \quad (3-18)$$

The control vector here is:

---

\* The sideslip angle definition differs from the conventional definition, which is:

$$\beta = \sin^{-1}\left(\frac{v}{|\underline{V}_{\text{air}}|}\right)$$

$$\underline{u} = [\Delta\delta E \ \Delta\delta T \ \Delta\delta F]^T \quad (3-19)$$

where  $\delta E$  is the elevator deflection,  $\delta T$  is the throttle travel and  $\delta F$  is the flap deflection.

To complete this illustration of aerodynamic and thrust effects within the context of longitudinal dynamics, the pitch moment (about the center of gravity of the airplane) equation must be introduced:

$$\Delta\dot{q} = M_u \Delta u + M_w \Delta w + M_q \Delta q + M_{\delta E} \Delta\delta E + M_{\delta T} \Delta\delta T + M_{\delta F} \Delta\delta F \quad (3-20)$$

Combining eq. (3-18) with eq. (3-20) and fully accounting for the physical effects reflected in eq. (3-2) to (3-10), we obtain:

$$\begin{bmatrix} \Delta\dot{u} \\ \Delta\dot{w} \\ \Delta\dot{q} \\ \Delta\dot{\theta} \end{bmatrix} = \begin{bmatrix} X_u & X_w & -w+X_q & -gc\theta \\ Z_u & Z_w & u+Z_q & -gs\theta \\ M_u & M_w & M_q & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} \Delta u \\ \Delta w \\ \Delta q \\ \Delta \theta \end{bmatrix} + \begin{bmatrix} X_{\delta E} & X_{\delta T} & X_{\delta F} \\ Z_{\delta E} & Z_{\delta T} & Z_{\delta F} \\ M_{\delta E} & M_{\delta T} & M_{\delta F} \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \Delta\delta E \\ \Delta\delta T \\ \Delta\delta F \end{bmatrix} \quad (3-21)$$

Equation (3-21) is of the form of a state equation:

$$\underline{\Delta\dot{x}} = F \underline{\Delta x} + G \underline{\Delta u} \quad (3-22)$$

where  $F$  is the state matrix and  $G$  - the control matrix.

### 3.2 CANDIDATE SPIFR CONFIGURATIONS VIA THE OUTPUT COMMAND ALGORITHM

The basic assumption underlying the following derivation



is that if a configuration requires large state and control variations to retrim from one nominal SPIFR flight equilibrium to another, it may also be problematic for the pilot.\* Thus, to pick the candidate configurations for SPIFR in-flight simulation, we first choose initial configuration parameters and flight equilibrium. Then we examine the required variations in state and control variables, which correspond to various retrimming requirements. The retrimming requirement may be formulated in terms of flight path variables, e.g., variation in airspeed  $\Delta V^*$  or in flight path angle  $\Delta \gamma^*$ .

The mathematical formulation uses the output command algorithm (Ref. 9). The following output equation is added to the state equation eq. (3-22):

$$\underline{\Delta y} = H_x \underline{\Delta x} + H_u \underline{\Delta u} \quad (3-23)$$

where  $\underline{\Delta y}$  represents the required retrimming flight-path variations. An ideal transition to the new flight equilibrium is assumed:

$$\left. \begin{aligned} 0 &= F \underline{\Delta x}^* + G \underline{\Delta u}^* \\ \underline{\Delta y}_{\text{comm}} &= H_x \underline{\Delta x}^* + H_u \underline{\Delta u}^* \end{aligned} \right\} \quad (3-24)$$

where  $()^*$  symbolizes the steady-state variations in state and control that correspond to  $\underline{\Delta y}_{\text{comm}}$ .

As shown in Ref. 9, the solution to eq. (3-24) is:

---

\* As used here, a configuration is a set of aerodynamic coefficients which characterizes the dynamic response of the aircraft.

$$\underline{\Delta x}^* = - F^{-1} G S \underline{\Delta y}_{\text{comm}} \quad (3-25)$$

$$\underline{\Delta u}^* = S \underline{\Delta y}_{\text{comm}} \quad (3-26)$$

where:

$$S \triangleq (-H_x F^{-1} G + H_u)^{-1} \quad (3-27)$$

As a result of application of the output command algorithm, variations in the following aerodynamic parameters have received priority in the context of SPIFR flight testing:

- a)  $X_u$  ,  $Z_u$  ,  $Z_\alpha$  ,  $M_u$
- b)  $Z_{\delta E}$  ,  $Z_{\delta T}$  ,  $M_{\delta T}$

Stability and control derivatives to be varied in the flight tests fall into two categories: those that affect only trim and those that affect both trim and stability. Control derivatives (list in (b) above) fall into the first category because, as demonstrated by eq. (3-21), they appear in the control matrix G, thus affecting  $\underline{\Delta x}^*$  and  $\underline{\Delta u}^*$ . Stability derivatives (list in (a) above) fall into the second category because they appear in the F matrix, thus affecting both trim and stability.

The ranges of variation of the aerodynamic parameters must reflect the trends in GA aircraft design. These are discussed in the context of the experimental matrix design in the next section.

### 3.3 EXPERIMENTAL MATRIX DESIGN

The high-priority list of configurations of the previous section has been limited to seven configurations, as we must tradeoff between:

- Number of configurations to be flight-tested.
- Number of replications of SPIFR mission with a given configuration (important for statistical soundness).
- Number of evaluation pilots.

All of this must be done under the constraint of about 25 flight hours.

These tradeoff considerations resulted in the following:

- 15 configurations (nominal ARA and plus/minus variations of each of the 7 coefficients).
- Two test pilots plus one GA pilot.
- Numbers of replications are shown, along with all the other information relevant to the experimental matrix, in Table 3.1. The pluses and the minuses to the right of the numbers of replications describe how many positive and how many negative parameter variations (with respect to nominal) are simulated for each of these numbers.

Parameter to be varied	Test pilot 1	Test pilot 2	GA pilot	Number of mission runs
Nominal	2	2	2	6
$X_u$	2 <sub>+</sub>	2 <sub>+</sub>	3 <sub>++</sub>	7
$Z_u$	2 <sub>+</sub>	2 <sub>+</sub>	3 <sub>++</sub>	7
$M_u$	2 <sub>+</sub>	2 <sub>+</sub>	3 <sub>++</sub>	7
$Z_\alpha$	2 <sub>+</sub>	2 <sub>+</sub>	3 <sub>++</sub>	7
$M_{\delta T}$	2 <sub>+</sub>	2 <sub>+</sub>	3 <sub>++</sub>	7
$Z_{\delta E}$	2 <sub>+</sub>	2 <sub>+</sub>	2 <sub>+</sub>	6
$Z_{\delta T}$	2 <sub>+</sub>	2 <sub>+</sub>	2 <sub>+</sub>	6
				Sum = 53

Table 3.1: Experimental Matrix for the First SPIFR Flight Series.

The ranges of the variations in the aerodynamic parameters are intended to reflect possible trends in GA aircraft design. For example, if the design goal is a configuration with a shorter body, an increase in elevator area may be required in order to preserve its moment effectiveness  $M_{\delta E}$ . Such an area change may affect the vertical force sensitivity of the elevator  $\Delta Z_{\delta E} < 0$ . On the other hand, introduction of a canard control surface may result in  $Z_{\delta E} > 0$ . Another example may be of a configuration design that features a high wing for improved cabin visibility and wing-mounted shrouded propellers for increased thrust. As a result  $M_u$  and  $M_{\delta T}$  may be affected by the variations in the aerodynamic forces and the moment arms.

### 3.4 IMPLEMENTATION OF SPIFR CONFIGURATIONS VIA IMPLICIT-MODEL-FOLLOWING ALGORITHM

The chosen SPIFR configurations are implemented on the in-flight simulator via the implicit-model-following algorithm (Ref. 10). State equations of the type of eq. (3-21) may be written for the nominal ARA configuration (subscript ARA) and for the configurations to be simulated (subscript M),

$$\dot{\underline{\Delta x}}_{ARA} = F_{ARA} \underline{\Delta x}_{ARA} + G_{ARA} \underline{\Delta u}_{ARA} \quad (3-28)$$

$$\dot{\underline{\Delta x}}_M = F_M \underline{\Delta x}_M + G_M \underline{\Delta u}_M \quad (3-29)$$

Our objective is to obtain the control vector  $\underline{\Delta u}_{ARA}$ , which will make the ARA respond as the required configuration. The perfect model following condition is:

$$\dot{\Delta x}_{ARA} = \dot{\Delta x}_M \quad (3-30)$$

Substituting eq. (3-28) and (3-29) into eq. (3-30) and rearranging:

$$\begin{aligned} \Delta u_{ARA} &= G_{ARA}^{\#} [(F_M - F_{ARA}) \Delta x_{ARA} + G_M \Delta u_M] \triangleq \\ &= C_B \Delta x_{ARA} + C_F \Delta u_M \end{aligned} \quad (3-31)$$

where:

$$G_{ARA}^{\#} \triangleq [G_{ARA}^T G_{ARA}]^{-1} G_{ARA}^T \quad (3-32)$$

Eq. (3-30) renders:

$$\Delta x_{ARA} = \Delta x_M \quad (3-33)$$

Thus,  $\Delta x_{ARA}$  is the solution of eq. (3-29). A block diagram of the derived algorithm is presented in Figure 3.1.

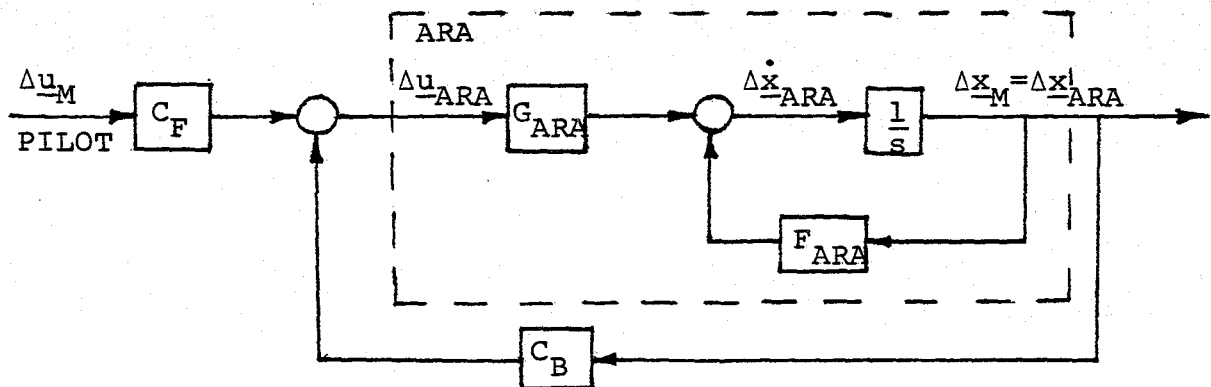


Figure 3.1. Block Diagram for Implementation of a SPIFR Configuration on the ARA In-Flight Simulator.

### 3.5 EFFECTS OF NAVIGATIONAL ACCURACY AND THE "LEARNING CURVE" EFFECT ON MISSION PLANNING

To simulate realistic SPIFR conditions, the mission has to contain several typical flight-path segments, including

- Climb, acceleration and cruise with airspeed retrimming.
- Holding pattern.
- Deceleration and descent.
- Localizer and glide slope interception.
- Approach and missed-approach go-around.

Also, a realistic VOR-radial navigation should consist of at least once switching navigational stations in the "TO"-mode and of a leg in the "FROM"-mode. The above considerations roughly size the SPIFR mission simulation to a minimum flight duration of about 30 minutes and the geometry shown in Fig. 3-2.

One problem associated with deciding the flight path geometry is the "learning curve" effect. The "learning curve" is the ability of a human being to improve his performance by taking advantage of past experience. Flying all missions along the same trajectory invokes memorization by the pilot, reducing the navigation workload to a level unrealistic for a SPIFR-type mission. To cope with this issue, additional flight path variants have been devised (Fig. 3-3, 3-4, 3-5). All variants are of comparable structure and flight duration.

The other problem associated with the decision of flight path geometry is navigational accuracy. Conclusions of the following discussion with regard to this issue have been implemented with the SPIFR missions of figures 3-2 to 3-5 and, as will be shown, they also contribute to post-flight flight-path reconstruction accuracy improvement.

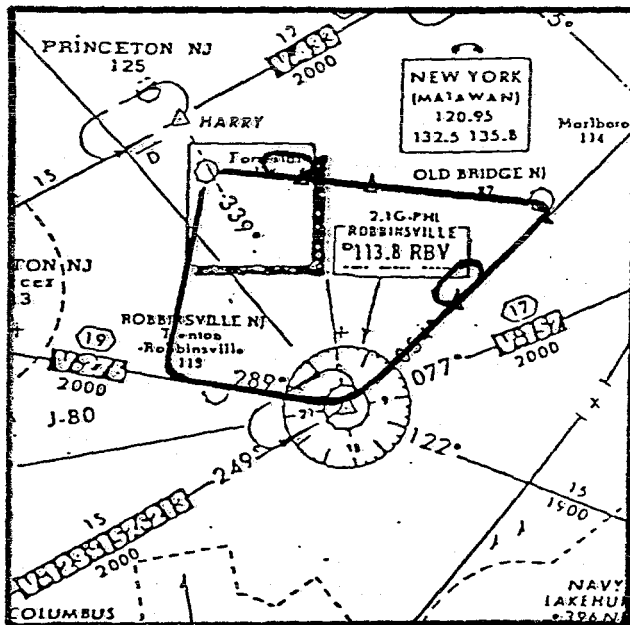


Figure 3-2. Variant I.

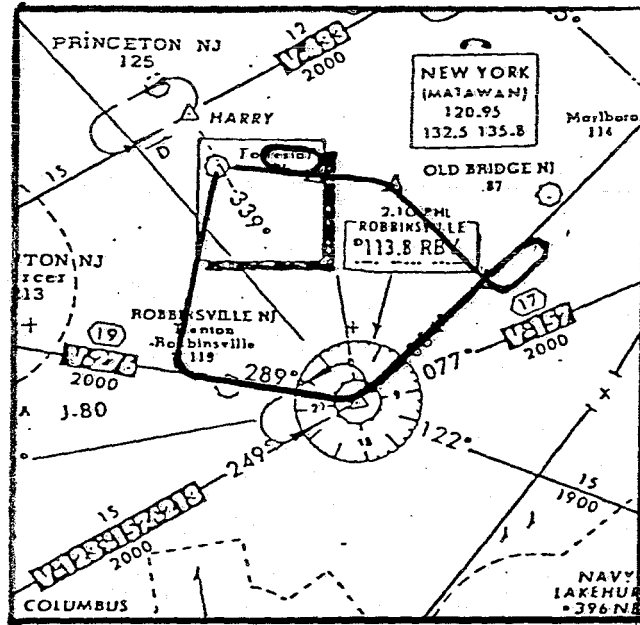


Figure 3-3. Variant II.

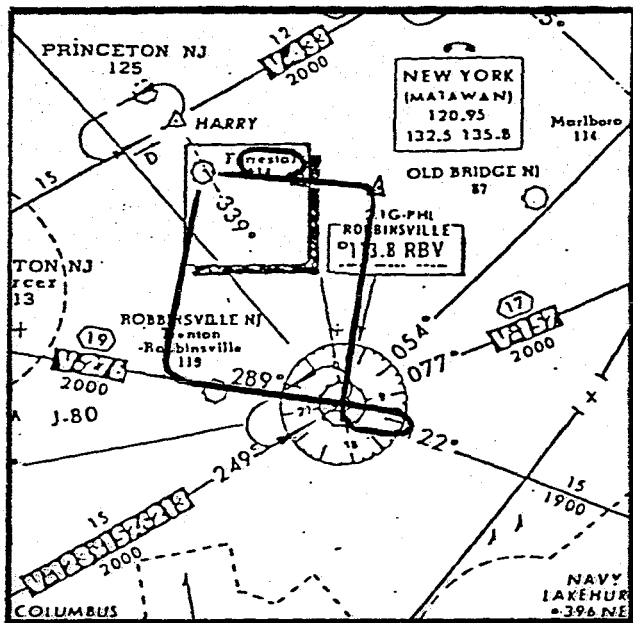


Figure 3-4. Variant III.

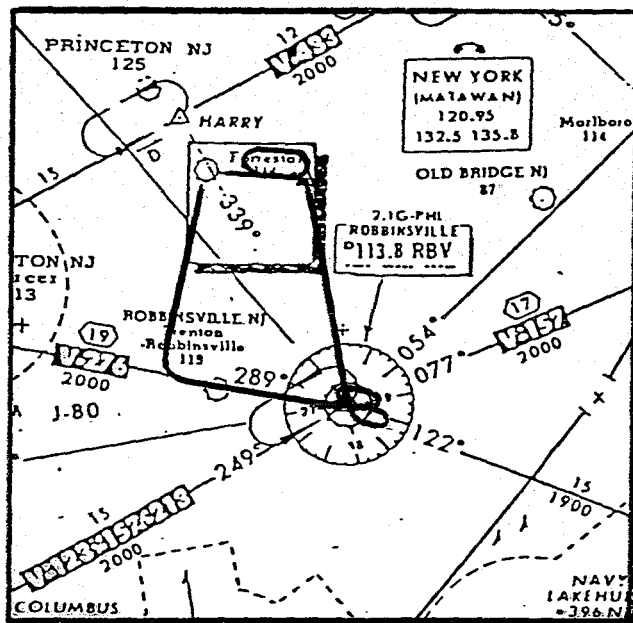


Figure 3-5. Variant IV.

Figures 3-2 to 3-5. SPIFR Flight Path Variants.

The standard navigational modes for GA are VOR/VOR, VOR/DME and DME/DME. At least two navigation stations are required to achieve a horizontal "fix" of the aircraft's position. With proper geometry any of these combinations can provide a fix; however the accuracy of the fix is subject to several factors. The accuracy requirements have been imposed by the Federal Aviation Administration (FAA), and their numerical values appear in Ref. 11.

$$\sigma_{\psi} \equiv \sigma_{\text{VOR}} = 1.9^{\circ}$$

$$\sigma_R = \sigma_{\text{DME}} = .15\% \text{ range or } .1 \text{ mile:} \\ \text{whichever is larger}$$

(3-34)

These navigational errors are with respect to a single ground station. The position errors associated with a navigational mode have to be computed accounting for the Geometric Dilution of Precision (GDOP) effect. GDOP is an inaccuracy due to the nonperpendicularity of the lines connecting the aircraft with the engaged stations.

Applying analytical geometry to the typical situation depicted in Fig. 3-6 and assuming that the two navigational-

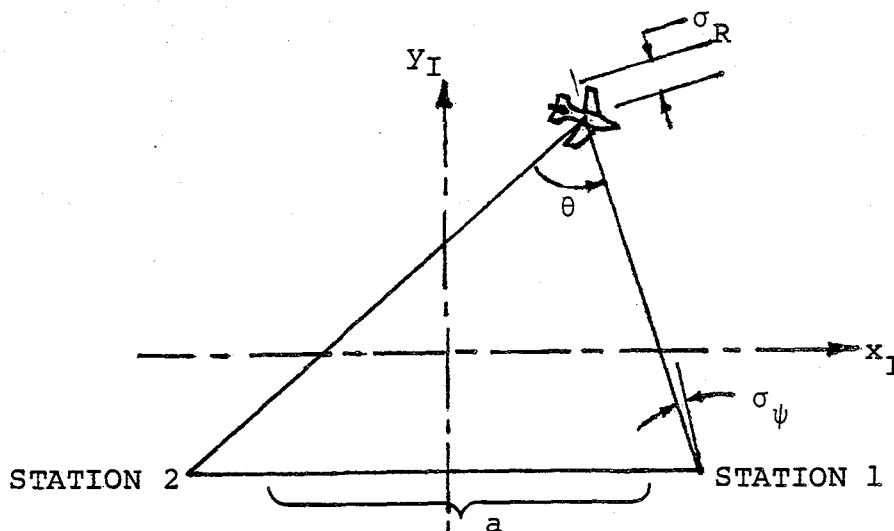


Figure 3-6. Ground Stations Engagement in the VOR/VOR or the DME/DME Modes.



stations' errors are statistically uncorrelated, we obtain:

$$\sigma = (1/s\theta) [\sigma_1^2 + \sigma_2^2]^{1/2} \quad (3-35)$$

The  $1/s\theta$  term reflects the GDOP effect. For angles between radials in the vicinity of  $\theta = 0^\circ$  or  $\theta = 180^\circ$ , the position error becomes very large, becoming infinite in the limit. To improve position accuracy using two similar ground stations while flying a given leg, it is desirable that the stations be as nearly perpendicular as possible. For VOR/VOR, eq. (3-35) can be rewritten as,

$$\sigma = \frac{a\sigma_\psi}{\sqrt{2} s^2\theta} (1+s^2\theta)^{1/2} \quad (3-36)$$

For DME/DME, eq. (3-35) becomes

$$\sigma = \sqrt{2} \sigma_R / s\theta \quad (3-37)$$

Numerical values of eq. (3-34) and dependence of  $\sigma_{\text{VOR/VOR}}$  on the  $\sin^2\theta$  suggest that this navigational mode is much less accurate than the DME/DME mode. For example, at a range of 50 miles from both stations and for  $\theta = 30^\circ$  the VOR/VOR error is 2.71 miles, while the DME/DME error is 0.28 miles and the results favour the DME/DME pairing at greater ranges. Based on this observation and on the feasibility of microprocessor-controlled sequential engagements of several DME stations, this technique will be employed to improve the flight path reconstruction accuracy. In particular, this accuracy improvement may be achieved by making use of redundant measurements, while applying the optimal Kalman filtering/smoothing algorithm.

### 3.6 OPTIMAL SMOOTHING OF FLIGHT-TEST RECORDS AND FLIGHT-PATH RECONSTRUCTION

One way to smooth flight test records is to pass the data through a filter, which chops off the high frequency content of the recorded information. A better way is to account for the particular system's dynamic characteristics. This can be done applying the extended Kalman filter algorithm.

For post-flight analysis, even higher accuracy may be achieved by accounting for the "future" information. This improvement is obtained by using an optimal smoothing algorithm. An additional advantage of this algorithm is that it estimates flight path variables that have not been measured directly. Thus, smoothing and flight path reconstruction are obtained via a single algorithm implementation (as in Ref. 12, 13). For this application we need the system state eq. (3-1), which constitutes a concise representation of eq. (3-2) to (3-13),

$$\dot{\underline{x}} = \underline{f}(\underline{x}, \underline{u}) + \underline{w} \quad (3-38)$$

and the measurement equation,

$$\underline{z} = \underline{h}(\underline{x}, \underline{u}) + \underline{v} \quad (3-39)$$

which stands for relationships of the type of eq. (3-14) to (3-17). Equation (3-38) differs from eq. (3-1) by the additional term  $\underline{w}$ , which is referred to in the literature as "process noise". The vector  $\underline{v}$  in eq. (3-39) is the "measurement noise".

Equations (3-18) to (3-31) need not be used in the post-flight optimal smoothing and flight-path reconstruction because the accelerations  $\underline{a}_B$  are measured directly. Equations (3-2) to (3-17) constitute a kinematic model, as they do not reflect the dynamic mechanism by which  $\underline{a}_B$  is actually produced.

The differential equations of the kinematic model (3-2), (3-9) and (3-11) constitute the "state model" and the algebraic relationships (3-14) to (3-17) the "measurement model". Even without accounting for the  $\underline{a}_B$  -producing-mechanism, the kinematic model is nonlinear and high-dimensional. Thus, it is more efficient to tackle it in two steps. This is made possible by the fact that the SPIFR experimental setup records both  $[p \ q \ r]^T$  and  $[\phi \ \theta \ \psi]^T$ . The first step is to smooth these six measurements. Treating all six as state variables and using eq. (3-9) we may write:

$$\text{STATE MODEL A} \left\{ \begin{array}{l} \dot{p} = n_p \\ \dot{q} = n_q \\ \dot{r} = n_r \\ \dot{\phi} = p + \tan \theta (s\phi * q + c\phi * r) \\ \dot{\theta} = c\phi * q - s\phi * r \\ \dot{\psi} = \frac{1}{c\theta} (s\phi * q + c\phi * r) \end{array} \right. \quad (3-40)$$

$$\text{MEASUREMENT MODEL A} \left\{ \begin{array}{l} \underline{z}_A = H_A \underline{x}_A + \underline{v}_A \end{array} \right. \quad (3-41)$$

The state vector for model A is:

$$\underline{x}_A = [p \ q \ r \ \phi \ \theta \ \psi]^T \quad (3-42)$$

The process noise vector (with  $n_p$ ,  $n_q$  and  $n_r$  random and unknown angular acceleration inputs) is:

$$\underline{w}_A = [n_p \ n_q \ n_r \ 0 \ 0 \ 0]^T \quad (3-43)$$

The measurement noise vector for model A is:

$$\underline{v}_A = [n_p \ n_q \ n_r \ n_\phi \ n_\theta \ n_\psi]^T \quad (3-44)$$

The measurement vector  $\underline{z}_A$  in (3-41) contains the measured values of  $\underline{x}_A$ . Thus, the observation matrix  $H_A$  is an identity matrix.

Before elaborating on the optimal smoother algorithm implementation based on eq. (3-40) and (3-41), the kinematic model for the second step is now derived. We assume that the time histories,

$$\hat{p}(t), \hat{q}(t), \hat{r}(t); \hat{\phi}(t), \hat{\theta}(t), \hat{\psi}(t) \quad (3-45)$$

and the associated matrices,

$$\hat{H}_B^I(t) \quad , \quad \hat{H}_I^B(t) \quad , \quad \hat{\omega}(t) \quad (3-46)$$

are given, having completed the first step. The 6-component state vector for the next step is,

$$\underline{x}_B = [x_I \ y_I \ z_I \ u \ v \ w]^T \quad (3-47)$$

and the 6-component input vector is,

$$\underline{u}_B = [w_{x_I} \ w_{y_I} \ w_{z_I} \ (a_x - s\theta g) \ (a_y + c\theta s\phi g) \ (a_x + c\theta c\phi g)]^T \quad (3-48)$$

The input vector contains components of the true wind and accelerations,  $\underline{w}_I$  and  $\underline{a}_B$ . In this context, the actual values of these measured variables are interpreted as inputs and their measurement inaccuracies as process noise\*:

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\* Appendix A presents an improved wind model.

$$\underline{w}_B = [0 \ 0 \ 0 \ n_{a_x} \ n_{a_y} \ n_{a_z}]^T \quad (3-49)$$

Unlike the first step, in which the  $\underline{x}_A$  components have been smoothed optimally, this step reconstructs the  $\underline{x}_B$  components with eq. (3-2) and (3-11) constituting the state model B:

$$\begin{array}{l} \text{STATE} \\ \text{MODEL B} \end{array} \left\{ \begin{array}{l} \begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{z}_I \end{bmatrix} = \hat{H}_B^I(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} w_{x_I} \\ w_{y_I} \\ w_{z_I} \end{bmatrix} \\ \begin{bmatrix} \dot{u} \\ \dot{v} \\ \dot{w} \end{bmatrix} = \hat{\omega}(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} a_x - s\hat{\theta}g \\ a_y + c\hat{\theta}s\hat{\phi}g \\ a_z + c\hat{\theta}c\hat{\phi}g \end{bmatrix} + \begin{bmatrix} n_{a_x} \\ n_{a_y} \\ n_{a_z} \end{bmatrix} \end{array} \right. \quad (3-50)$$

Equations (3-14) to (3-17) plus VOR and DME measurement equations constitute the measurement model B:

$$\begin{array}{l} \text{MEASUREMENT} \\ \text{MODEL B} \end{array} \left\{ \begin{array}{l} |\underline{v}_{air}| = (u^2 + v^2 + w^2)^{1/2} + n_v \\ \alpha = \tan^{-1}(\frac{w}{u}) + n_\alpha \\ \beta = \tan^{-1}(\frac{v}{u}) + n_\beta \\ h = -z_I + n_h \\ r_{DME_{si}} = [(x_I - x_{si})^2 + (y_I - y_{si})^2 + (z_I - z_{si})^2]^{1/2} + n_{DME} \\ \theta_{VOR_{si}} = \tan^{-1}[(y_I - y_{si}) / (x_I - x_{si})] + n_{VOR} \end{array} \right. \quad (3-51)$$

where  $s_i$  symbolizes the distance  $r_{DME_{s_i}}$  or angle  $\theta_{VOR_{s_i}}$  being measured with respect to navigational station  $i$ . The measurement noise vector is:

$$\underline{v}_B = [n_v \ n_\alpha \ n_\beta \ n_h \ n_{DME_1} \ n_{DME_2} \ \dots \ n_{VOR_1} \ n_{VOR_2} \ \dots]^T \quad (3-52)$$

Estimates of measurement biases and scale factor errors may be obtained at the expense of significant increase in state vector dimension. Such an increase in dimension may affect not only the computing cost but also the computational accuracy.

Examination of eq. (3-40) to (3-51) shows that both models A and B are nonlinear. Thus the extended Kalman smoother algorithm has to be applied (Ref. 14). This algorithm is implemented as a combination of forward- and backward-running Kalman filters. The extended Kalman filter algorithm constitutes an adaptation of the linear Kalman filter theory to nonlinear situations. It propagates the nonlinear dynamic model between measurements and utilizes a locally linearized model for the measurement updates.

The following is the discrete formulation of the extended Kalman smoother algorithm, applied to the dynamic model of the system, which constitutes of the state model (eq. (3-38)) and measurement model (eq. (3-39)). The propagation of the estimated states  $\hat{\underline{x}}$  and of the state covariance matrix  $P$  between measurements, for forward filtering uses

$$\hat{\underline{x}}(t) = \underline{f}[\hat{\underline{x}}(t), \underline{u}(t)] \quad (3-53)$$

$$P_k(-) = \Phi_{k-1} P_{k-1}(+) \Phi_{k-1}^T + Q_{k-1} \quad (3-54)$$

where  $Q$  is the process noise covariance matrix and  $\Phi$  is the transition matrix obtained after local linearization of eq. (3-38) into:

$$\dot{\underline{x}} = F\underline{x} + G\underline{u} + L\underline{w} \quad (3-55)$$

In order not to create inaccuracies due to numerical differentiation, analytical derivation of the Jacobian matrices ( $F$ ,  $G$  and  $L$ ) has been carried out for both models A and B; this is documented in Appendix A. The Kalman gain matrix for forward filtering is,

$$K_k = P_k(-) H_k^T [H_k P_k(-) H_k^T + R_k]^{-1} \quad (3-56)$$

where  $R$  is the measurement noise covariance matrix and  $H$  is obtained by local linearization of eq. (3-39) as

$$\underline{z}_k = H_k \underline{x} + \underline{v}_k \quad (3-57)$$

State and covariance updates account for measurements as

$$\hat{\underline{x}}_k(+) = \hat{\underline{x}}(t) + K_k [\underline{z}_k - \underline{h}_k(\underline{x}(t))] \quad (3-58)$$

$$P_k(+) = [I - K_k H_k] P_k(-) \quad (3-59)$$

where  $\hat{\underline{x}}(t)$  is obtained by integration of eq. (3-53) from  $t_{k-1}$  to  $t_k$ .

The filter processing of the raw data renders the state estimates before the measurement update  $\hat{\underline{x}}_k(-) \equiv \hat{\underline{x}}(t)$  and after the measurement update  $\hat{\underline{x}}_k(+)$  and the associated covariance matrices  $P_k(-)$  and  $P_k(+)$ . The smoother algorithm uses this information as input and running backwards in time produces the improved estimates of the states  $\hat{\underline{x}}_{k/n}$  and of the covariance matrix  $P_{k/n}$ . The first step is the computation of the state matrix  $F_k$ :

$$F_k = f[\hat{\underline{x}}_k(+)] \quad (3-60)$$

The state matrix is used to calculate the state transition matrix  $\Phi_k$ . The state transition matrix and the input covariance matrices render matrix  $A_k$ :

$$A_k = P_k(+) \Phi_k^T P_{k+1}^{-1}(-) \quad (3-61)$$

Using the input state estimates  $\hat{\underline{x}}_k(-)$  and  $\hat{\underline{x}}_k(+)$  and the associated covariance matrices  $P_k(+)$  and  $P_k(-)$  along with  $A_k$ , the smoothed and reconstructed states  $\hat{\underline{x}}_{k/n}$  are obtained:

$$\hat{\underline{x}}_{k/n} = \hat{\underline{x}}_k(+) + A_k [\hat{\underline{x}}_{k+1/n} - \hat{\underline{x}}_{k+1}(-)] \quad (3-62)$$

$$P_{k/n} = P_k(+) + A_k [P_{k+1/n} - P_{k+1}(-)] A_k^T \quad (3-63)$$

This complete optimal estimation algorithm, which performs post-flight data smoothing and flight-path reconstruction has been coded in FORTRAN (Appendix B) and verified by application to a computer-generated SPIFR trajectory.



Examples of the optimal flight path reconstruction algorithm's application to the generic flight-test data records are given in Fig. 3-7 for a coordinated climbing turn flight segment of 60 seconds. Figure 3-7a) to f) present reconstructed measurements demonstrating both state variable reconstruction and improvement with respect to data corrupted by noise. The symbol convention used in these figures is: (+) for nominal, ( $\square$ ) for corrupted, ( $\nabla$ ) for filtered and ( $\Delta$ ) for smoothed time histories. Line segments are used to link results but they do not suggest a functional relationship.

Figures 3-7a) and b) represent the optimal smoothing of the angular states. As may have been expected, the "derivative" states (e.g., Fig. 3-7b) are noisier than the "integral" states (e.g., Fig. 3-7a). In a sense, this distinction is applicable to the airspeed versus aerodynamic angle measurements, which reflect the atmospheric turbulence effect. As follows from the translational submodel formulation, to reconstruct these measurements (e.g., Fig. 3-7c) and d)), the states  $u$ ,  $v$  and  $w$  are first estimated. The typical lag introduced by filtering is more apparent in some of the figures; it is then reduced by the smoother. The trajectory reconstruction is represented in Fig. 3-7e), f) and g). Note that optimal smoothing improves the filtered state estimates and also shrinks the position uncertainty ellipsoid.

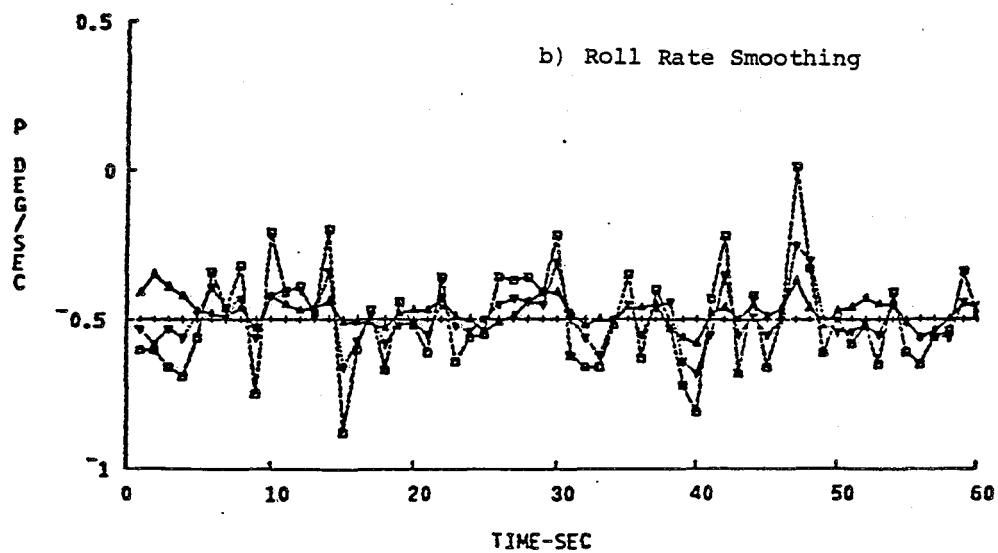
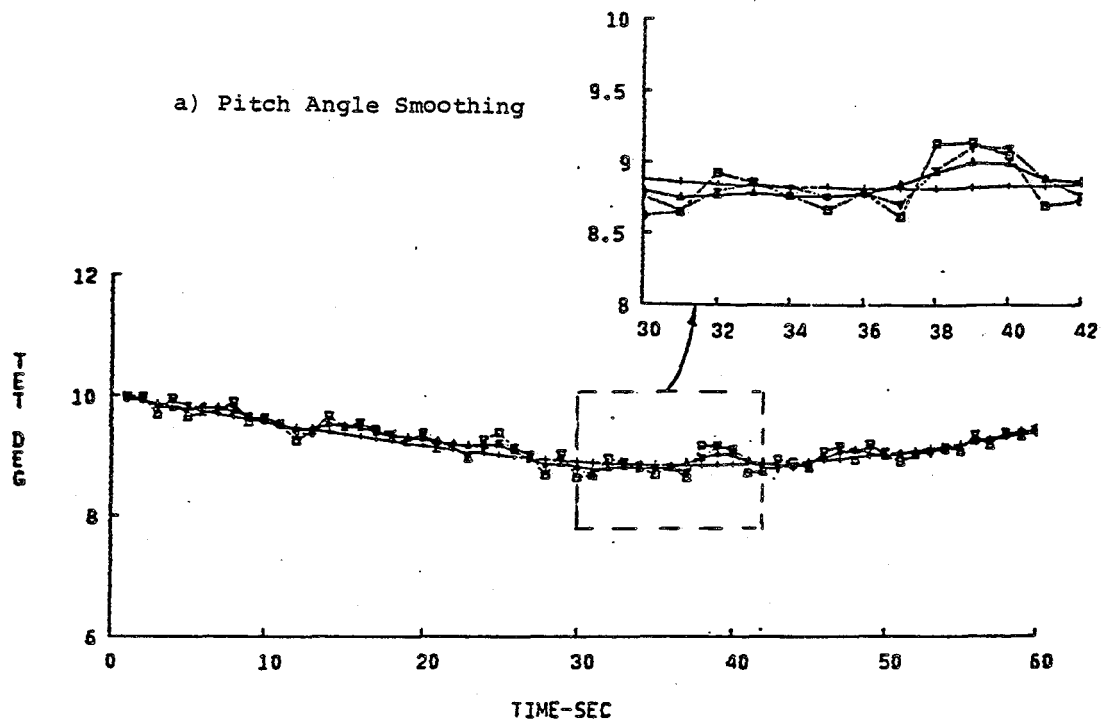


Figure 3-7: Examples of application of the optimal flight path reconstruction algorithm to the climbing turn pseudo-flight-test data.

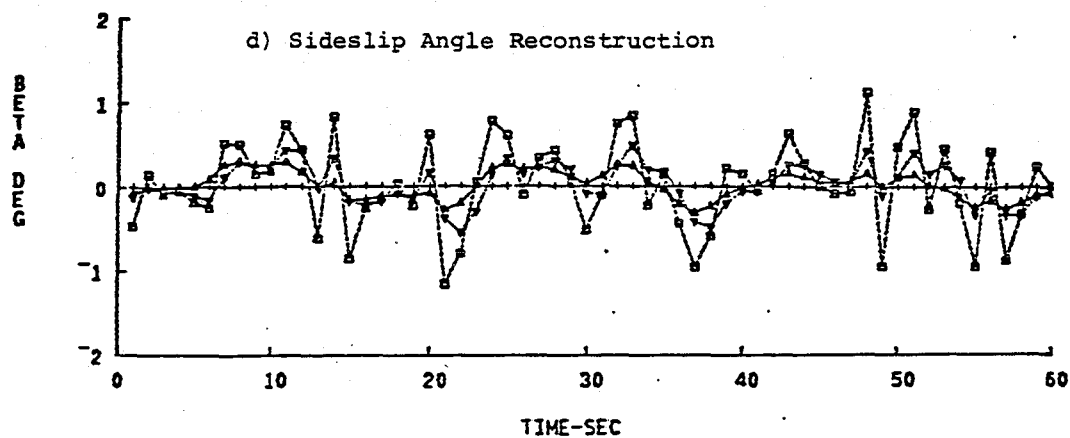
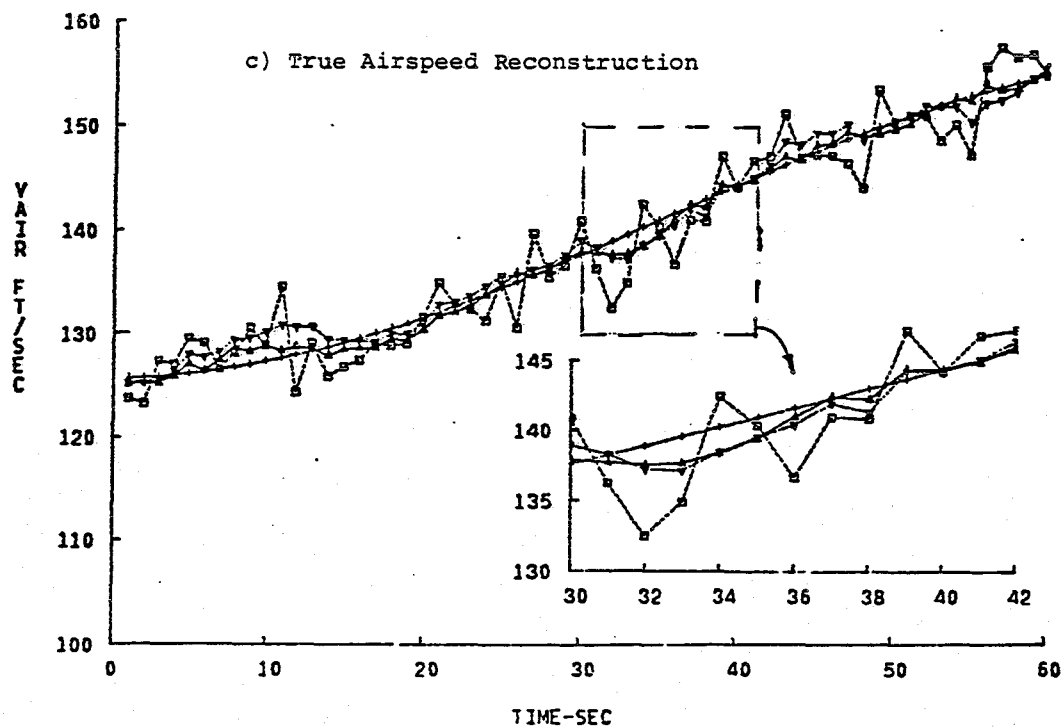


Figure 3-7: Examples of application of the optimal flight path reconstruction algorithm to the climbing turn pseudo-flight-test data.  
(cont.)

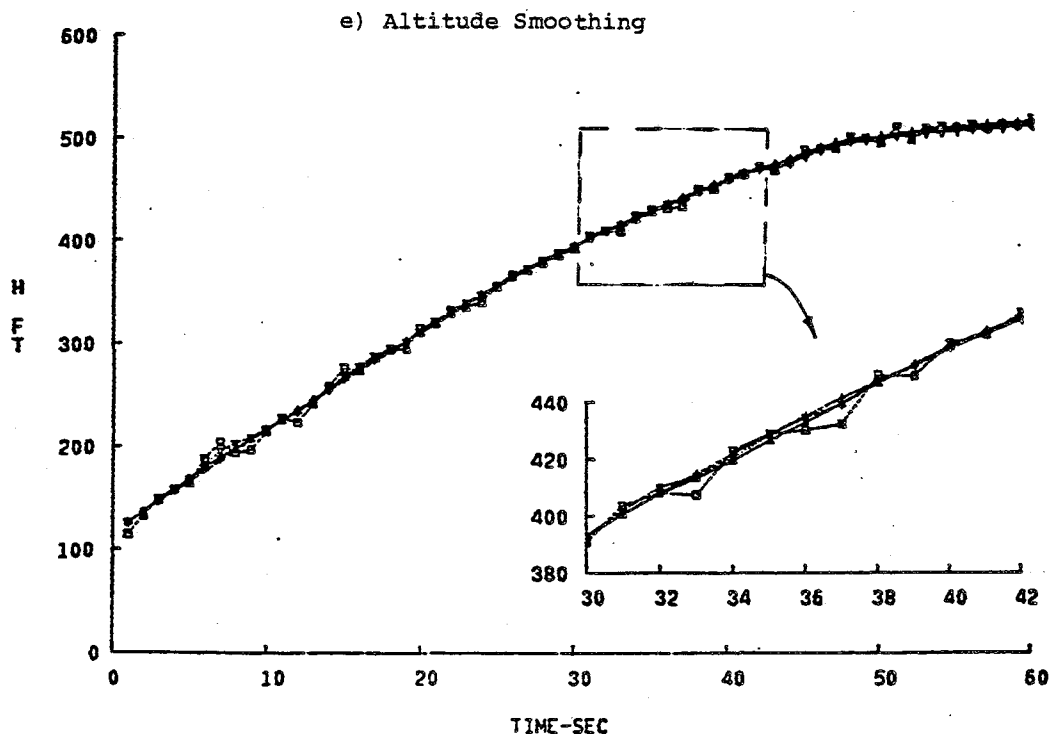


Figure 3-7: Examples of application of the optimal flight path reconstruction algorithm to the climbing turn pseudo-flight-test data.

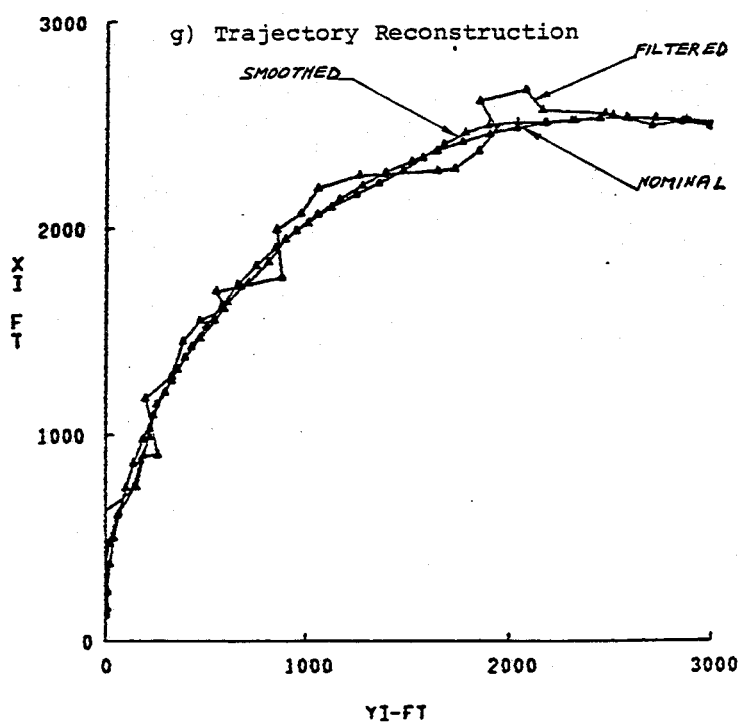
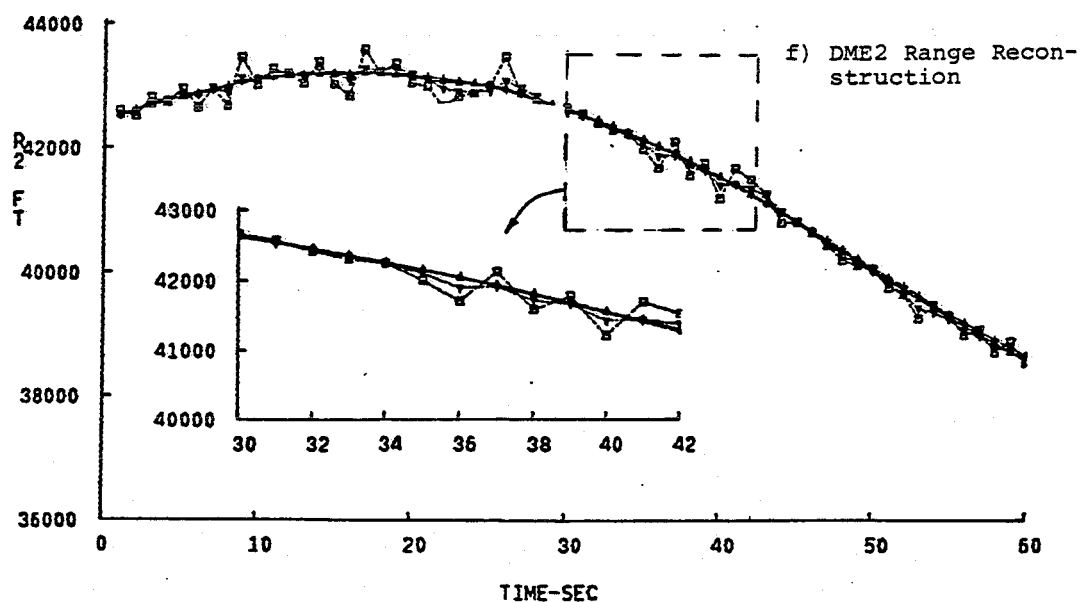


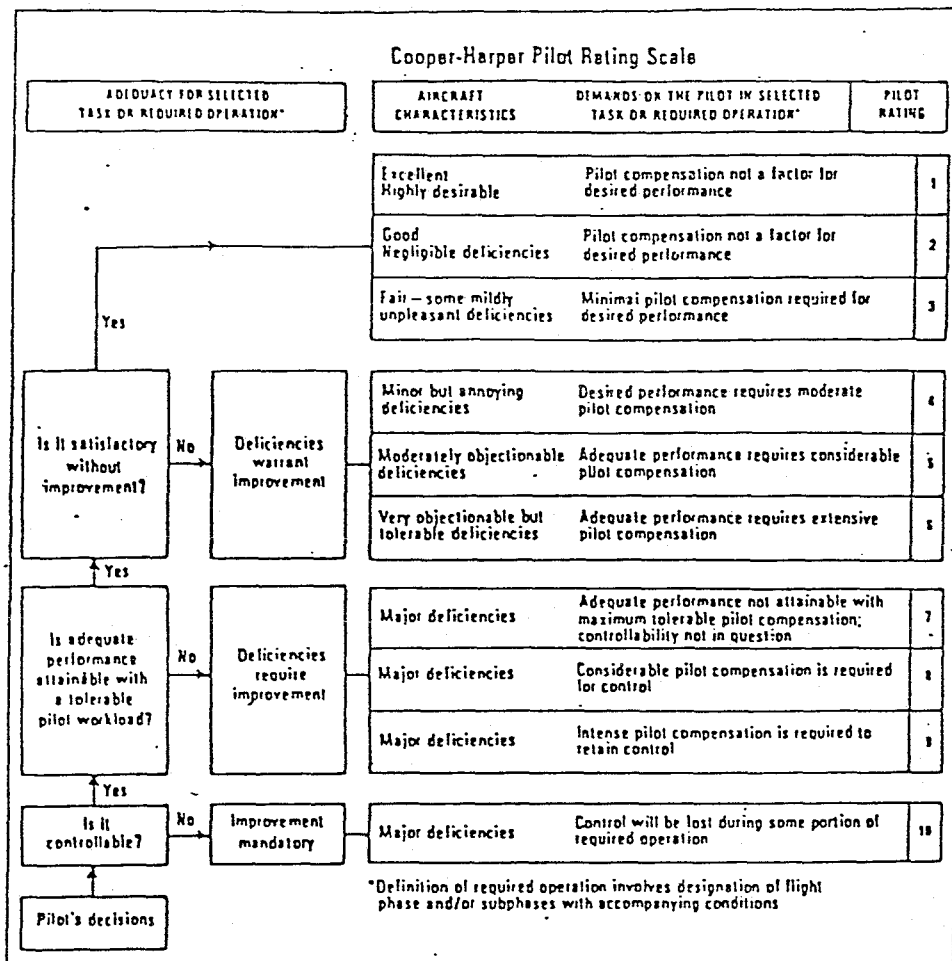
Figure 3-7: Examples of application of the optimal flight path reconstruction algorithm to the climbing turn pseudo-flight-test data.  
(cont.)

Flight test results are the important objectives of the SPIFR program. As the human operator is an integral part of the control and guidance loop, Pilot Opinion Ratings (POR) constitute important experimental results. Both the Cooper-Harper Rating (CHR), which is a performance rating (Ref. 15) and the workload rating (M.I.T. scale, Ref. 15) are significant. As we debrief the evaluation pilot with regard to both the complete mission and to its specific segments, knee-pad-size versions of both scales and of the grading sheet have been prepared (Fig. 4-1).

To test the complete SPIFR-mission-simulation concept, a series of preliminary flights has been carried out. Its main objectives were to verify the realism of simulation of SPIFR regime environment, the in-flight configuration matching capability and the data acquisition and reduction process.

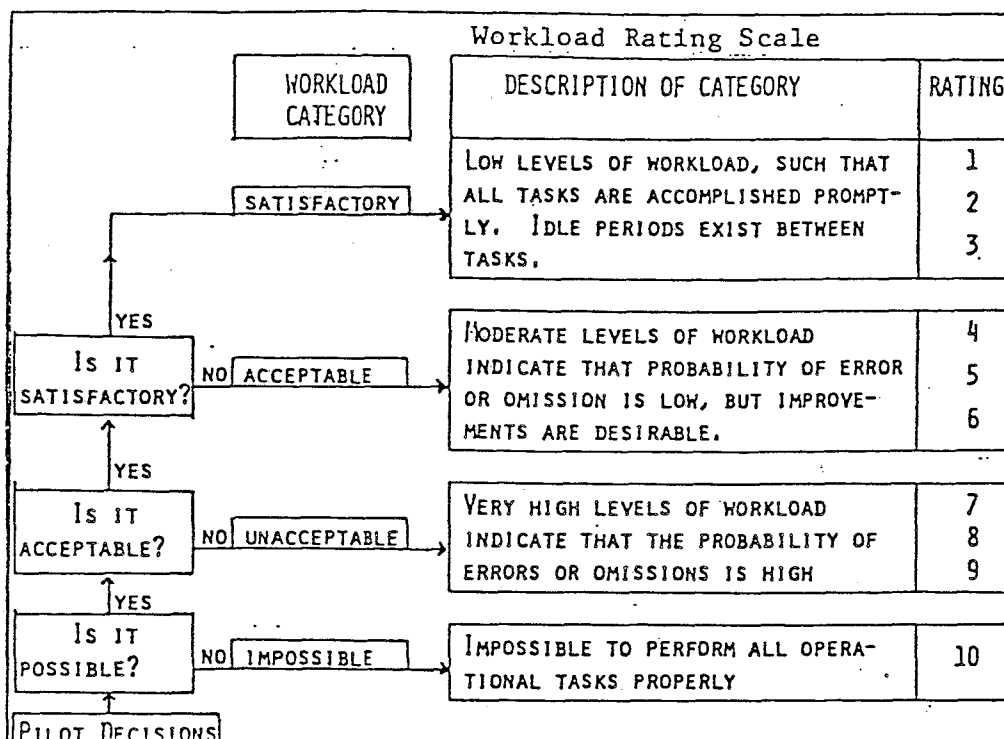
After extensive hangar checks of the aircraft system modifications, of the new navigation/communication package and of the onboard experimental setup, the proposed instrument tracks (Fig. 3-2 to 3-5) were flown - totalling to about 10 flight hours.

These preliminary flights have shown that the tasks appear to simulate SPIFR missions, which are realistic in both geometry and workload. Using the knee-pad-size POR scales and grading sheet the in-flight debriefing can be carried out without interfering with the mission. The in-flight configuration matching capability with regard to each



a) Performance POR Scale

Figure 4-1: Knee-pad Versions of the Performance and Workload PORs and of the Evaluation Sheet.



b) Workload POR Scale

Figure 4-1: Knee-pad Versions of the Performance and Workload PORs and of the Evaluation Sheet.



<u>EVALUATION SHEET</u>	
MISSION VARIANT #	
CONFIGURATION #	
PILOT	
DATE	
<u>SPEED RETRIMMING</u>	
CHR	
WORKLOAD	
COMMENTS	
<u>HOLDING PATTERN</u>	
CHR	
WORKLOAD	
COMMENTS	
<u>GLIDE SLOPE TRACKING</u>	
CHR	
WORKLOAD	
COMMENTS	
<u>OVERALL MISSION</u>	
CHR	
WORKLOAD	
COMMENTS	

c) Evaluation Sheet.

Figure 4-1: Knee-pad Versions of the  
(cont.) Performance and Workload  
PORs and of the Evaluation  
Sheet.

of the priority configurations has been confirmed. The data collection and reduction process has been verified by comparison of timings and directions of deflection of various controls reported by the safety pilot to those obtained by recorded data processing.

5.

#### CONCLUSION

This report summarizes the first phase of the SPIFR project, which constitutes an integrated theoretical and flight-test research effort, which addresses stability-and-control, avionics and human factor effects in single pilot IFR situations. The first phase activities were aimed at basic research system preparation and, consequently, at conducting the first flight test series of the SPIFR four-year program.

Most of the goals of the first phase of the SPIFR program have been achieved. The basic research system has been put together and successfully flight-tested, including the ARA aircraft modifications and the onboard digital data acquisition system. A modern navigation/communication system has been installed, and a new instrument panel has been designed to accomodate flexibility in introduction of additional instrumentation and workload devices. The data collection system has been built around the Z-80 microprocessor. The microprocessor performs the analog channels sampling, preliminary processing and transfer of the data records to the digital recorder. The software required for these on-board manipulations has been developed, debugged and flight-tested. In parallel, the post-flight data preprocessing software and procedure development has been completed and tried out with actual in-flight recorded data. Mission planning and experimental matrix design have been carried out accounting for navigational accuracy and the "learning curve effect" and for the amount-of-flight-hours-constraint. Applying theoretical algorithms the aerodynamic configurations for the

SPIFR program have been obtained and implemented on the ARA aircraft. A preliminary flight-test series has been conducted to check whether realistic SPIFR conditions are obtained and to verify the in-flight configurations matching. These flight tests have confirmed that the SPIFR mission simulation is realistic both in geometry and in workload.

During the second phase of the SPIFR project, the first flight series will be completed and the collected data will be analysed, including the subjective PORs. Finally, statistical regression analysis will be applied to render flying qualities criteria for Single Pilot Instrument Flight Rule operations.

The structure of the research program as summarized in this report will render quantitative criteria with regard to the effects of airframe dynamic response, workload level, and pilot experience on the SPIFR flight regime. Furthermore, the ARA is now ready to conduct a broad range of additional flight experiments associated with single-pilot instrument flight.

## APPENDIX A

### DERIVATION OF THE LINEARIZED VERSIONS OF THE SIMPLIFIED AND THE IMPROVED KINEMATIC MODELS

#### A.1 IMPROVED WIND MODEL

The kinematic state model B (eq.(3-50)) assumes that ideal, constant wind measurements  $\underline{w}_I$  are available along the flight path. Although we may disregard the high-frequency turbulence disturbances, it is difficult to obtain wind measurements along a flight path with an acceptable degree of reliability. A solution is to adjoin a wind model to state model B, estimating its parameters along with  $\underline{x}_B$ . A reasonable low-frequency wind model may constitute of a constant component and a linear variation with altitude,

$$\underline{w}_I(h) = \underline{w}_{I_0} + \frac{\partial \underline{w}_I}{\partial z_I} (z_I - z_{I_0}) \quad (A-1)$$

where  $\underline{w}_{I_0}$  is a constant wind vector at reference altitude  $-z_{I_0}$  and  $\frac{\partial \underline{w}_I}{\partial z_I}$  is a vector of slope of wind variation with altitude. Adjoining eq. (A-1) to eq. (3-50), we obtain:

$$\begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{z}_I \end{bmatrix} = \hat{H}_B^I(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} w_{x_{I_0}} + \frac{\partial w_{x_I}}{\partial z_I} (z_I - z_{I_0}) \\ w_{y_{I_0}} + \frac{\partial w_{y_I}}{\partial z_I} (z_I - z_{I_0}) \\ w_{z_{I_0}} + \frac{\partial w_{z_I}}{\partial z_I} (z_I - z_{I_0}) \end{bmatrix} \quad (A-2)$$

$$\begin{bmatrix} \dot{u} \\ \dot{v} \\ \dot{w} \end{bmatrix} = \hat{\omega}(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} a_x - s\hat{\theta}g \\ a_y + c\hat{\theta}s\hat{\phi}g \\ a_z + c\hat{\theta}c\hat{\phi}g \end{bmatrix} + \begin{bmatrix} n_{a_x} \\ n_{a_y} \\ n_{a_z} \end{bmatrix} + \hat{H}_I^B(t) * \frac{\partial w_I}{\partial z_I} * [\dot{z}_I] \quad (A-3)$$

Carrying through the mathematical steps necessary to transfer the state variable  $z_I$  derivative to the left-hand side, we obtain the state model B in the following form:

$$\begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{z}_I \end{bmatrix} = \hat{H}_B^I(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} w_{x_{I_0}} + \frac{\partial w_{x_I}}{\partial z_I} (z_I - z_{I_0}) \\ w_{y_{I_0}} + \frac{\partial w_{y_I}}{\partial z_I} (z_I - z_{I_0}) \\ w_{z_{I_0}} + \frac{\partial w_{z_I}}{\partial z_I} (z_I - z_{I_0}) \end{bmatrix} \quad (A-4)$$

$$\begin{bmatrix} \dot{u} \\ \dot{v} \\ \dot{w} \end{bmatrix} = \hat{\omega}(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} a_x - s\hat{\theta} g \\ a_y + c\hat{\theta}s\hat{\phi}g \\ a_z + c\hat{\theta}c\hat{\phi}g \end{bmatrix} + \begin{bmatrix} n_{a_x} \\ n_{a_y} \\ n_{a_z} \end{bmatrix} + H_{uvw} \hat{H}_I^B(t) \frac{\partial w_I}{\partial z_I} \quad (A-5)$$

$$\begin{bmatrix} \dot{w}_{x_{I_0}} \\ \dot{w}_{y_{I_0}} \\ \dot{w}_{z_{I_0}} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \quad (A-6)$$

$$\begin{bmatrix} \frac{\partial \dot{w}_{x_I}}{\partial z_I} \\ \frac{\partial \dot{w}_{y_I}}{\partial z_I} \\ \frac{\partial \dot{w}_{z_I}}{\partial z_I} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \quad (A-7)$$

$$H_{uvw} \triangleq \begin{bmatrix} \hat{H}_{B_{31}}^I & \hat{H}_{B_{32}}^I & \hat{H}_{B_{33}}^I \end{bmatrix} \begin{bmatrix} u \\ v \\ w \end{bmatrix} \quad (A-8)$$

The kinematic state model B of eq. (A-2) to (A-8) renders improved flight path reconstruction and an estimate of constant wind and of wind gradient along the flight path.

## A.2 LINEARIZATION OF THE SIMPLIFIED KINEMATIC MODEL

To apply the extended Kalman filter algorithm the non-linear kinematic model has to be linearized. The linearized version of the simplified kinematic model has been derived analytically and is presented in this section. The result for state model A [eq. (3-40)] is:

$$\begin{aligned}
 \begin{bmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \\ \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} &= \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 1 & \tan\theta \sin\phi & \tan\theta \cos\phi & q \tan\theta \cos\phi - r \tan\theta \sin\phi (q \sin\phi + r \cos\phi) / c^2 \theta & 0 \\ 0 & c\phi & -s\phi & -q \sin\phi - r \cos\phi & 0 \\ 0 & s\phi / c\theta & c\phi / c\theta & q \cos\phi / c\theta - r \sin\phi / c\theta (q \sin\phi + r \cos\phi) \frac{s\theta}{c^2 \theta} & 0 \end{bmatrix} \begin{bmatrix} p \\ q \\ r \\ \phi \\ \theta \\ \psi \end{bmatrix} + \begin{bmatrix} n_p \\ n_q \\ n_r \\ 0 \\ 0 \\ 0 \end{bmatrix} \quad (A-9) \\
 \dot{\underline{x}}_A & \quad \quad \quad \underline{F}_A \quad \quad \quad \underline{x}_A \quad \quad \quad \underline{w}_A
 \end{aligned}$$

Rearranging eq. (3-50) of state model B:

$$\begin{aligned}
 \begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{z}_I \\ \dot{u} \\ \dot{v} \\ \dot{w} \end{bmatrix} &= \begin{bmatrix} 0 \\ 6 \times 3 \end{bmatrix} \begin{bmatrix} \hat{H}_B^I(t) \\ \hat{\omega}(t) \end{bmatrix} \begin{bmatrix} x_I \\ y_I \\ z_I \\ u \\ v \\ w \end{bmatrix} + [I] \begin{bmatrix} w_{x_I} \\ w_{y_I} \\ w_{z_I} \\ a_x - \hat{s}\hat{\theta}g \\ a_y + \hat{c}\hat{\theta}\hat{s}\hat{\phi}g \\ a_z + \hat{c}\hat{\theta}\hat{c}\hat{\phi}g \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ n_{a_x} \\ n_{a_y} \\ n_{a_z} \end{bmatrix} \quad (A-10) \\
 \dot{\underline{x}}_B & \quad \quad \quad \underline{F}_B \quad \quad \quad \underline{x}_B \quad \quad \quad \underline{G}_B \quad \quad \quad \underline{u}_B \quad \quad \quad \underline{w}_B
 \end{aligned}$$



The linearized version of measurement model B [eq. (3-51)]:

$$\begin{bmatrix} |V_{air}| \\ \alpha \\ \beta \\ h \\ r_{DME_{s1}} \\ r_{DME_{s2}} \\ \theta_{VOR_{s1}} \\ \theta_{VOR_{s2}} \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 0 & 0 & \frac{u}{a_o^{1/2}} & \frac{v}{a_o^{1/2}} & \frac{w}{a_o^{1/2}} \\ 0 & 0 & 0 & \frac{-w}{a_o - v^2} & 0 & \frac{u}{a_o - v^2} \\ 0 & 0 & 0 & \frac{-v}{a_o - w^2} & \frac{u}{a_o - w^2} & 0 \\ 0 & 0 & -1 & 0 & 0 & 0 \\ \frac{x_I - x_{s1}}{a_{31}^{1/2}} & \frac{y_I - y_{s1}}{a_{31}^{1/2}} & \frac{z_I - z_{s1}}{a_{31}^{1/2}} & 0 & 0 & 0 \\ \frac{x_I - x_{s2}}{a_{32}^{1/2}} & \frac{y_I - y_{s2}}{a_{32}^{1/2}} & \frac{z_I - z_{s2}}{a_{32}^{1/2}} & 0 & 0 & 0 \\ \frac{-(y_I - y_{s1})}{a_{31} - (z_I - z_{s1})^2} & \frac{x_I - x_{s1}}{a_{31} - (z_I - z_{s1})^2} & 0 & 0 & 0 & 0 \\ \frac{-(y_I - y_{s2})}{a_{32} - (z_I - z_{s2})^2} & \frac{x_I - x_{s2}}{a_{32} - (z_I - z_{s2})^2} & 0 & 0 & 0 & 0 \end{bmatrix}}_{H_B} \underbrace{\begin{bmatrix} x_I \\ y_I \\ z_I \\ u \\ v \\ w \end{bmatrix}}_{\underline{x}_B} + \underbrace{\begin{bmatrix} n_v \\ n_\alpha \\ n_\beta \\ n_h \\ n_{DME_1} \\ n_{DME_2} \\ n_{VOR_1} \\ n_{VOR_2} \end{bmatrix}}_{\underline{v}_B} \quad (A-11)$$

$$\left. \begin{aligned} \text{with: } a_o &= u^2 + v^2 + w^2 \\ a_{3i} &= (x_I - x_{si})^2 + (y_I - y_{si})^2 + (z_I - z_{si})^2 \end{aligned} \right\} \quad (A-12)$$

### A.3 LINEARIZATION OF THE IMPROVED KINEMATIC MODEL.

The improvement to the kinematic model elaborated in the first section of this appendix refers to state model B. The linearized version of (A-3) is:

$$\begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{z}_I \\ \dot{u} \\ \dot{v} \\ \dot{w} \\ \dot{w}_{x_{I_0}} \\ \dot{w}_{y_{I_0}} \\ \dot{w}_{y_{I_0}} \\ \frac{\partial \dot{w}_{x_I}}{\partial z_I} \\ \frac{\partial \dot{w}_{y_I}}{\partial z_I} \\ \frac{\partial \dot{w}_{z_I}}{\partial z_I} \end{bmatrix} = \begin{bmatrix} F_{11} & F_{12} & F_{13} & F_{14} \\ & & & \\ F_{21} & F_{22} & F_{23} & F_{24} \\ & & & \\ F_{31} & F_{32} & F_{33} & F_{34} \\ & & & \\ F_{41} & F_{42} & F_{43} & F_{44} \end{bmatrix} \begin{bmatrix} x_I \\ y_I \\ z_I \\ u \\ v \\ w \\ w_{x_{I_0}} \\ w_{y_{I_0}} \\ w_{z_{I_0}} \\ \frac{\partial w_{x_I}}{\partial z_I} \\ \frac{\partial w_{y_I}}{\partial z_I} \\ \frac{\partial w_{z_I}}{\partial z_I} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ a_x - s\theta g \\ a_y + c\hat{\theta}s\hat{\phi}g \\ a_z + c\hat{\theta}c\hat{\phi}g \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ n_{a_x} \\ n_{a_y} \\ n_{a_z} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} \quad (A-13)$$

$\underline{\dot{x}}_B \qquad \qquad F_B \qquad \qquad \underline{x}_B$

where each  $F_{ij}$  stands for a 3x3 matrix:

$$F_{21} = F_{31} = F_{41} = F_{32} = F_{42} = F_{23} = F_{33} = F_{43} = F_{34} = F_{44} = [0] \quad (A-14)$$

$$F_{13} = [I] \quad (A-15)$$

$$F_{14} = (z_I - z_{I_0}) [I] \quad (A-16)$$

$$F_{11} = \begin{bmatrix} 0 & 0 & \frac{\partial w_{x_I}}{\partial z_I} \\ 0 & 0 & \frac{\partial w_{y_I}}{\partial z_I} \\ 0 & 0 & \frac{\partial w_{z_I}}{\partial z_I} \end{bmatrix} \quad (A-17)$$

$$F_{12} = \hat{H}_B^I(t) \quad (A-18)$$

$$F_{22} = \begin{bmatrix} \hat{H}_{B31}^I \left( \hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_1 & \hat{r} + \hat{H}_{B32}^I \left( \hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_1 & -\hat{q} + \hat{H}_{B33}^I \left( \hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_1 \\ -\hat{r} + \hat{H}_{B31}^I \left( \hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_2 & \hat{H}_{B32}^I \left( \hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_2 & \hat{p} + \hat{H}_{B33}^I \left( \hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_2 \\ \hat{q} + \hat{H}_{B31}^I \left( \hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_3 & -\hat{p} + \hat{H}_{B32}^I \left( \hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_3 & \hat{H}_{B33}^I \left( \hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_3 \end{bmatrix} \quad (A-19)$$

$$F_{24} = H_{uvw}^* \hat{H}_I^B(t) \quad (A-20)$$

APPENDIX B  
PROGRAM LISTINGS

B.1 ONBOARD ASSEMBLY PROGRAMMING

The microprocessor prepares the data in block units. Each block unit is a memory buffer of 1024 data words (each data word contains two bytes or 16 bits). For 38 information channels, for example, taken every second such a block can be filled with 26-sec worth of data (plus 36 dummy words:  $38 \times 26 + 36 = 1024$ ). A data block is written into the digital cartridge recordwise. Each record contains 128 data words, i.e., under normal conditions eight records complete a block transfer. Occasionally, to make sure that no data is missed, a record may be written repeatedly onto the cartridge. Thus, the first task for the preprocessing software (Appendix C) is to reconstruct the original data blocks, each constituting of eight records of  $\frac{8 \times 128 - 36}{38} = 26$  information-seconds.

B.2 GENERIC SPIFR FLIGHT PATH AND IN-FLIGHT MEASUREMENTS  
SIMULATION (FORTRAN)

This program creates a generic SPIFR mission trajectory, simulates the associated in-flight measurements and corrupts them with pseudo-random noise. Knowing the uncorrupted values of the measured variables, the algorithm for optimal smoothing and flight path reconstruction may be verified.

### B.3 OPTIMAL SMOOTHING AND FLIGHT PATH RECONSTRUCTION ALGORITHM (FORTRAN)

As demonstrated in the following listings, one of the key issues in optimal smoothing and flight path reconstruction is computer storage management -- in particular, between the forward and the backward passes over the measured data records. The smoothing algorithm, which consists of eq. (3-60) to (3-63), requires knowledge of the state-vector before and after each measurement update and of the corresponding covariance matrices. For state model A, e.g., the state vector has six components. This means that following the filtering pass 84 values have to be stored for each measurement instant. A SPIFR mission simulation is about 30 minutes long and after preprocessing the measurement update interval is standardized to be 1 sec for all variables. Thus, the temporary storage facility has to "remember" 84x30x60 values.

## T SPIFR8 LISTING

## ONBOARD ASSEMBLY (B.1)

```

1 ;
2 ;
3 ;
4 ;
5 ;
6 ;
7 ;
8 ;
9 ;
10 ;
11 ;
12 ;
13 ;
14 ;
15 ;
16 ;
17 ;
18      ORG      8000H
19  ADDAM  EQU    3000H      ;ADDRESS OF A TO D CONVERTER
20  JMP    EQU    0C3H
21  ;CO     EQU    03BH
22  INT75   EQU    OFFE3H
23  LITEPORT EQU    0C5H      ;LITE DISPLAY PORT IS PORT C J1 OF 116 BOARD
24  LITECTRL EQU    0C7H      ;CTRL PORT FOR J1 OF 116 BOARD
25  ;LITEPORT EQU    0E9H      ;LITE DISPLAY PORT IS PORT B J2 OF 8004
26  ;LITECTRL EQU    0EBH      ;CTRL PORT FOR J2 OF 8004
27  J18004  EQU    0E7H      ;CONTROL OF 8255 J-1
28  ALTPORT  EQU    0E4H      ;ALTIMETER PORT A J-1
29  PUSHPORT EQU    0E5H      ;PUSHBUTTON PORT B J-1
30      DI
31      CALL    INITPORTA ;8255 PORT A OF J2 ON 8004
32      CALL    INITUSART ;INITIALISE THE USART FOR PILOT TERMINAL
33      CALL    INITSENA ;SET UP SEMAPHORES ON ALL TEN BUFFERS
34      CALL    INITRE
35      CALL    FILLMEM   ;FILL MEMORY WITH INTEGERS 0-10239
36      CALL    INITWR    ;INITIALISE EMPTYING POINTERS
37      ;
38      ;DUMP TEN BUFFERS EACH 2048
39      ;TO TAPE, 256 BYTES AT A TIME
40      ;OVER AND OVER AGAIN.
41      ;THE BUFFERS ARE DESIGNATED BY
42      ; THE DIGITS 0 TO 9.
43      ;
44      ;DE POINTS TO THE LOCATION
45      ; TO BE EMPTIED.
46      ;
47      CALL    ALIGN     ;INITIALISE T9511
48      CALL    OK
49      LXI     D,BUFF0   ;DE PAIR POINT TO LOCATION TO BE EMPTIED
50      CALL    STINT     ;ENABLE THE INTERRUPTS
51  BB:
52      CALL    TSTEMPTY  ;WAIT UNTIL BUFFER FULL
53      CALL    WRITE     ;DUMP ANOTHER 256 BYTES TO TAPE
54      CALL    UEBUFS    ;UPDATE THE INDICES USED
55      ; TO KEEP TRACK OF EMPTYING THE TEN BUFFERS.
56      ; THERE ARE THREE OF THEM,
57      ; TWO POINTERS AND A COUNTER.
58      JMP     BB
59      ;
60      LDA     FLAG
61      CPI     0
62      JNZ     BB
63      MVI     A,10

```

228035	326188	64	STA	FLAG	
228038	3E24	65	MVI	A,'\$'	
22803A	CD4182	66	CALL	BO	
22803D	C31F80	67	JMP	BB	
22		68	;LAG:	DB	0
22		69	FILLLEN:		
228040	F5	70	PUSH	PSW	
228041	E5	71	PUSH	H	
228042	110090	72	LXI	D,BUFF0	;BASE ADDRESS FOR FILLING IS BUFF0
228045	210000	73	LXI	H,0	;COUNT STARTS WITH 0
228048	7D	74	FILLAG: MOV	A,L	;LOWER BYTE INTO ACC
228049	12	75	STAX	D	;STORE IT TO MEMORY
22804A	13	76	INX	D	;MOVE TO NEXT BYTE LOCATION
22804B	7C	77	MOV	A,H	;UPPER BYTE INTO ACC
22804C	12	78	STAX	D	;STORE IT TO MEMORY
22804D	13	79	INX	D	;POINT TO NEXT BYTE LOCATION
22804E	23	80	INX	H	;SIZE OF INTEGER UP BY 1
22804F	7C	81	MOV	A,H	;CHECK FOR AN UPPER BOUND
228050	FE28	82	CPI	28H	;
228052	C24880	83	JNZ	FILLAG	;REPEAT IF BELOW UPPER BOUND
228055	E1	84	POP	H	
228056	F1	85	POP	PSW	
228057	C9	86	RET		
22		87	UEBUFFS:		
228058	F5	88	PUSH	PSW	
228059	E5	89	PUSH	H	
22805A	C5	90	PUSH	B	
22805B	2A6688	91	LHLD	EREMAIN	
22805E	010001	92	LXI	B,256	;256 BYTES EMPTIED AT A TIME
228061	AF	93	XRA	A	;CARRY=0
228062	ED42	94	DSBC	B	
228064	226688	95	SHLD	EREMAIN	;EREMAIN=EREMAIN-256
22		96			;
22		97			;IS EREMAIN >= 256 ?
22		98			;
228067	AF	99	XRA	A	;CARRY=0
228068	ED42	100	DSBC	B	
22806A	F29D80	101	JP	ER00H	;IF S=0, HL >= BC
22		102			;
22		103			;CAN NOT EMPTY
22		104			; ANOTHER BLOCK OF 256
22		105			; FROM CURRENT BUFFER OF 2048
22		106			;
22806D	CD4887	107	CALL	SETEMPTY	;MARK CURRENT BUFFER EMPTY
22		108			;SET UP INDICES FOR DUMPING NEXT 2048 BLOCK
228070	210008	109	LXI	H,2048	;
228073	226688	110	SHLD	EREMAIN	;EREMAIN=2048
22		111			;
228076	3A6888	112	LDA	EMHICB	;SWITCH TO NEXT BUFFER
228079	3C	113	INR	A	;
22807A	326888	114	STA	EMHICB	;
22807D	FE0A	115	CPI	10	
22807F	C29280	116	JNZ	ESW	;
228082	76	117	HLT		
22		118			;
22		119			;WE ARE NOW BEYOND TENTH BUFFER
22		120			; NOTE EMHICB HAS RANGE 0 TO 9
22		121			; SWITCH TO BUFFER 0
22		122			;
228083	3E00	123	MVI	A,0	
228085	326888	124	STA	EMHICB	;EMHICB=0
22		125			;
22		126			;ECLRRBUF CONTAINS THE STARTING
22		127			; LOCATION OF THE CURRENT 2048 BLOCK
22		128			; BEING EMPTIED
22		129			;

LL8088	110090	130	LXI	D,BUFF0	;BUFF0 IS STARTING LOCATION OF
LL		131			; BLOCK 0 OR BUFFER 0
LL808B	ED537488	132	SDED	ECURRBUF	;NOTE THAT DE POINTS WHERE ECURRBUF POINTS
LL80AF	C39D80	133	JMP	EROOM	
LL		134	ESW:		
LL		135			
LL		136			; WE ARE GOING TO EMPTY A BUFFER
LL		137			; 2048 BYTES HIGHER IN CORE THAN THE
LL		138			; PREVIOUS BUFFER.
LL		139			
LL8092	2A7488	140	LHLD	ECURRBUF	
LL8095	010008	141	LXI	B,2048	
LL8098	09	142	DAD	B	
LL8099	227488	143	SHLD	ECURRBUF	
LL809C	EB	144	XCHG		;DE POINTING WHERE ECURRBUF POINTS.
LL		145	EROOM:		
LL809D	C1	146	POP	B	
LL809E	E1	147	POP	H	
LL809F	F1	148	POP	PSW	
LL80A0	C9	149	RET		
LL		150			
LL		151	WRITE:		
LL		152			;THE ONLY ERROR ALLOWED FOR NOW
LL		153			;IS TRYING TO WRITE BEYOND EOT
LL		154			;WRITE ON LEFT TAPE OR RIGHT TAPE
LL		155			;DEPENDING ON THE SETTING OF TSM
LL		156			;TSM='L' OR 'R'.
LL		157			;IF END OF TAPE OR HARD ERROR ON ONE TAPE,
LL		158			;SWITCH TO ANOTHER TAPE
LL		159			
LL80A1	F5	160	PUSH	PSW	
LL80A2	E5	161	PUSH	H	
LL80A3	C5	162	PUSH	B	
LL80A4	ED537888	163	SDED	TEMPDE	;SAVE DE PAIR IN CASE OF RETRY
LL		164	LXI	H,TEMPDE	
LL		165	CALL	WMP2	
LL80A8	3A6988	166	LDA	TSM	;WHICH TAPE DO WE USE?
LL80AB	FE4C	167	CPI	'L'	
LL80AD	C2C280	168	JNZ	WRITR	
LL		169	WRITL:		
LL80B0	CD3481	170	CALL	LCTUN	;IF YOU COME TO EOT SWITCH TO NEXT UNIT
LL		171			;((((((((MORE CODE HERE))))))))))))))))
LL		172			;((((((((ABOUT SWITCHING LOGIC))))))))))))))))
LL80B3	CABE80	173	JZ	RETML	
LL80B6	3E52	174	MVI	A,'R'	
LL80B8	326988	175	STA	TSM	
LL		176			;((((((((RETRANSMIT LAST RECORD ONTO RIGHT TAPE))))))))))))
LL80BB	C3C280	177	JMP	WRITR	; AND REWRITE RECORD ON RIGHT TAPE
LL80BE	C1	178	RETML:	POP	B
LL80BF	E1	179		POP	H
LL80C0	F1	180		POP	PSW
LL80C1	C9	181		RET	
LL		182	WRITR:		
LL80C2	CD0581	183	CALL	RETUN	;IF YOU COME TO EOT SWITCH TO NEXT UNIT
LL		184			;((((((((MORE CODE HERE))))))))))))))))
LL		185			;((((((((ABOUT SWITCHING LOGIC))))))))))))))))
LL80C5	CAD080	186	JZ	RETMR	
LL80C8	3E4C	187	MVI	A,'L'	
LL80CA	326988	188	STA	TSM	
LL		189			;((((((((RETRANSMIT LAST RECORD USING))))))))))))
LL80CD	C3B080	190	JMP	WRITL	; AND REWRITE RECORD ON LEFT TAPE
LL80D0	C1	191	RETMR:	POP	B
LL80D1	E1	192		POP	H
LL80D2	F1	193		POP	PSW
LL80D3	C9	194		RET	
LL		195	INITMR:		



228004	F5	196	PUSH	PSW	
228005	E5	197	PUSH	H	
228006	3E00	198	MVI	A,0	
228008	326888	199	STA	EMHICB	
22800B	210008	200	LXI	H,2048	
22800E	226688	201	SHLD	EREMAIN	
2280E1	3E4C	202	MVI	A,'L'	
2280E3	326988	203	STA	TSM	
2280E6	210090	204	LXI	H,BUFF0	
2280E9	227488	205	SHLD	ECURRBUF	
2280EC	110090	206	LXI	D,BUFF0	
2280EF	E1	207	POP	H	
2280F0	F1	208	POP	PSW	
2280F1	C9	209	RET		
22		210	DEH256:		
2280F2	E5	211	PUSH	H	
22		212			;
22		213			;DE (= DE - 256
22		214			;
2280F3	62	215	MOV	H,D	
2280F4	6B	216	MOV	L,E	;HL (= DE
2280F5	010001	217	LXI	B,256	
2280F8	AF	218	XRA	A	;CARRY=0
2280F9	ED42	219	DSBC	B	;HL - 256
2280FB	54	220	MOV	D,H	
2280FC	5D	221	MOV	E,L	;DE (= HL
2280FD	E1	222	POP	H	
2280FE	C9	223	RET		
22		224	LCTUF:		
22		225			;WRITE AN EOF MARK ON LCTU
2280FF	3E1B	226	MVI	A,ESC	
228101	CD4182	227	CALL	BO	
228104	3E26	228	MVI	A,'&	
228106	CD4182	229	CALL	BO	
228109	3E70	230	MVI	A,'p'	
22810B	CD4182	231	CALL	BO	
22810E	3E31	232	MVI	A,'1'	;ADDRESS OF LCTU
228110	CD4182	233	CALL	BO	
228113	3E75	234	MVI	A,'u'	
228115	CD4182	235	CALL	BO	
228118	3E35	236	MVI	A,'5'	;WRITE FILEMARK COMMAND IS ASCII CHAR 5
22811A	CD4182	237	CALL	BO	
22811D	3E43	238	MVI	A,'C'	
22811F	CD4182	239	CALL	BO	
228122	3E11	240	MVI	A,DC1	
228124	CD4182	241	CALL	BO	
228127	CD5782	242	CALL	BI	
22812A	326288	243	STA	SAVE	
22812B	CD5782	244	CALL	BI	
228130	326388	245	STA	SAVE+1	
228133	C9	246	RET		
22		247	LCTUM:		
228134	ED5B7888	248	LDSD	TEMPDE	
228138	3E1B	249	MVI	A,ESC	
22813A	CD4182	250	CALL	BO	
22813D	3E26	251	MVI	A,'&	
22813F	CD4182	252	CALL	BO	
228142	3E70	253	MVI	A,'p'	
228144	CD4182	254	CALL	BO	
228147	3E31	255	MVI	A,'1'	
228149	CD4182	256	CALL	BO	
22814C	3E64	257	MVI	A,'d'	
22814E	CD4182	258	CALL	BO	
228151	3E32	259	MVI	A,'2'	
228153	CD4182	260	CALL	BO	
228156	3E35	261	MVI	A,'5'	

228158	CD4182	262	CALL	BO	
22815B	3E36	263	MVI	A,'6'	
22815D	CD4182	264	CALL	BO	
228160	3E57	265	MVI	A,'W'	
228162	CD4182	266	CALL	BO	
228165	3E05	267	MVI	A,ENG	
228167	CD4182	268	CALL	BO	
22816A	CD5782	269	CALL	BI	
22816D	326488	270	STA	SAV	
228170	FE06	271	CPI	ACK	
228172	CA7881	272	JZ	NEXT	
228175	C33481	273	JMP	LCTUM	
22		274	NEXT:		DE POINTS TO LOCATION TO BE EMPTIED
228178	010001	275	LXI	B,256	
22817B	CD7482	276	CALL	SEND	
22817E	3E11	277	MVI	A,DC1	
228180	CD4182	278	CALL	BO	
228183	CD5782	279	CALL	BI	READ S OF F
228186	DA3481	280	JC	LCTUM	
228189	326288	281	STA	SAVE	
22818C	CD5782	282	CALL	BI	READ CR
22818F	DA3481	283	JC	LCTUM	
228192	326388	284	STA	SAVE+1	
228195	3A6288	285	LDA	SAVE	EITHER S OR F
228198	FES3	286	CPI	'S'	
22819A	C8	287	RZ		RETURN Z SET ON 'S', Z RESET ON 'F'
22819B	ED5B7888	288	LDED	TEMPDE	
22819F	C9	289	RET		
22		290	RTUF:		
22		291			WRITE AN EOF MARK ON LCTU
2281A0	3E1B	292	MVI	A,ESC	
2281A2	CD4182	293	CALL	BO	
2281A5	3E26	294	MVI	A,'8'	
2281A7	CD4182	295	CALL	BO	
2281AA	3E70	296	MVI	A,'p'	
2281AC	CD4182	297	CALL	BO	
2281AF	3E32	298	MVI	A,'2'	ADDRESS OF RTU
2281B1	CD4182	299	CALL	BO	
2281B4	3E75	300	MVI	A,'u'	
2281B6	CD4182	301	CALL	BO	
2281B9	3E35	302	MVI	A,'5'	WRITE FILEMARK COMMAND IS ASCII CHAR 5
2281BB	CD4182	303	CALL	BO	
2281BE	3E43	304	MVI	A,'C'	
2281C0	CD4182	305	CALL	BO	
2281C3	3E11	306	MVI	A,DC1	
2281C5	CD4182	307	CALL	BO	
2281C8	CD5782	308	CALL	BI	
2281CB	326288	309	STA	SAVE	
2281CE	CD5782	310	CALL	BI	
2281D1	326388	311	STA	SAVE+1	
2281D4	C9	312	RET		
22		313	RTUM:		
2281D5	ED5B7888	314	LDED	TEMPDE	
2281D9	3E1B	315	MVI	A,ESC	
2281DB	CD4182	316	CALL	BO	
2281DE	3E26	317	MVI	A,'8'	
2281E0	CD4182	318	CALL	BO	
2281E3	3E70	319	MVI	A,'p'	
2281E5	CD4182	320	CALL	BO	
2281E8	3E32	321	MVI	A,'2'	ADDRESS OF RTU
2281EA	CD4182	322	CALL	BO	
2281ED	3E44	323	MVI	A,'d'	
2281EF	CD4182	324	CALL	BO	
2281F2	3E32	325	MVI	A,'2'	
2281F4	CD4182	326	CALL	BO	
2281F7	3E35	327	MVI	A,'5'	

2281F9	CD4182	328	CALL	BO	
2281FC	3E36	329	MVI	A,'6'	
2281FE	CD4182	330	CALL	BO	
228201	3E57	331	MVI	A,'W'	
228203	CD4182	332	CALL	BO	
228206	3E05	333	MVI	A,END	
228208	CD4182	334	CALL	BO	
228208	CD5782	335	CALL	BI	
22820E	326488	336	STA	SAW	
228211	FE06	337	CPI	ACK	
228213	CA1982	338	JZ	NEXT	
228216	C3D581	339	JMP	RTUM	
22		340	NEXT:		
22		341			;DE POINTS TO LOCATION TO BE EMPTIED
228219	010001	342	LXI	B,256	
22821C	CD7482	343	CALL	SEND	
22821F	3E11	344	MVI	A,DC1	
228221	CD4182	345	CALL	BO	
228224	CD5782	346	CALL	BI	; READ S OR F
228227	DAD581	347	JC	RTUM	
22822A	326288	348	STA	SAVE	
22822D	CD5782	349	CALL	BI	; READ CR
228230	DAD581	350	JC	RTUM	
228233	326388	351	STA	SAVE+1	
228236	3A6288	352	LDA	SAVE	;EITHER S OR F
228239	FES3	353	CPI	'S'	;RETURN WITH Z SET ON S, Z RESET ON F
22823B	CA	354	RZ		
22823C	ED5B7888	355	LDED	TEMPDE	
228240	C9	356	RET		
22		357	;*****		
22		358	; CHARACTER OUTPUT ROUTINE		
22		359	; CD OUTPUTS ONE CHARACTER FROM ACC TO TERMINAL		
22		360	; VIA THE USART. ALL REGISTERS AND FLAGS ARE		
22		361	; PRESERVED. THE CHARACTER IT OUTPUTS IS IN THE ACC.		
22		362	;*****		
228241	F5	363	BO:	PUSH	PSW
228242	C5	364		PUSH	B
228243	4F	365		MOV	C,A ;SAVE A REG
22		366	BOO:		
228244	00	367		NOP	
228245	00	368		NOP	
228246	DBED	369		IN	SA251A ;GET USART STATUS
228248	E601	370		ANI	TXRDYA ;CHECK TRANSMIT READY FLAG
22824A	CA4482	371		JZ	BOO ;NOT READY
22824D	00	372		NOP	
22824E	00	373		NOP	
22824F	00	374		NOP	
228250	00	375		NOP	
228251	79	376		MOV	A,C ;READY TO TRANSMIT , RESTORE CHAR TO A REG
228252	D3EC	377		OUT	DA251A ;SEND IT
228254	C1	378		POP	B
228255	F1	379		POP	PSW
228256	C9	380		RET	
22		381	;*****		
22		382	; CHARACTER INPUT ROUTINE		
22		383	; BI INPUTS ONE CHARACTER FROM TERMINAL INTO ACC		
22		384	; VIA THE USART. THE FLAGS AND THE ACC ARE CHANGED.		
22		385	; THE CHARACTER IT READS IS RETURNED IN THE ACC.		
22		386	; IF NO TIMEOUT OCCURS, THE CARRY IS SET.		
22		387	; IF TIMEOUT OCCURS, THE CARRY IS RESET.		
22		388	; THE CHAR READ IS RETURNED IN THE ACC.		
22		389	;*****		
228257	00	390	BI:	NOP	
228258	C5	391		PUSH	B
228259	01FFFF	392		LXI	B,OFFFH
22		393	BI0:		

22A25C	08	394	DCX	B	
22A25D	78	395	MOV	A,B	
22A25E	B1	396	ORA	C	
22A25F	CA6F82	397	JZ	TIMEDOUT	
22A262	DBED	398	IN	S8251A	;GET USART STATUS
22A264	E602	399	ANI	R0RDYA	;CHECK RECIEVER READY
22A266	CA5C82	400	JZ	B10	;
22A269	DBEC	401	IN	D8251A	;GET CHAR
22A268	37	402	STC		
22A26C	3F	403	CNC		
22A26D	C1	404	POP	B	
22A26E	C9	405	RET		
22A26F	00	406	TIMEDOUT: NOP		
22A270	37	407	STC		
22A271	C1	408	POP	B	
22A272	C9	409	RET		
22A273	76	410	HLT		
22		411	SEND:		
22A274	1A	412	LDAX	D	
22A275	CD4182	413	CALL	BO	
22A278	13	414	INX	D	
22A279	08	415	DCX	B	
22A27A	78	416	MOV	A,B	
22A27B	B1	417	ORA	C	
22A27C	C27482	418	JNZ	SEND	
22A27F	C9	419	RET		
22		420	STATUS:		
22A280	F5	421	PUSH	PSW	
22A281	E5	422	PUSH	H	
22A282	21FC89	423	LXI	H,STAT	
22A285	3E18	424	MVI	A,ESC	;START ESCAPE SEQUENCE
22A287	CD4182	425	CALL	BO	
22A28A	3E5E	426	MVI	A,''	
22A28C	CD4182	427	CALL	BO	
22A28F	3E11	428	MVI	A,DC1	
22A291	CD4182	429	CALL	BO	
22A294	CD5782	430	CALL	BI	;EAT ESC
22A297	CD5782	431	CALL	BI	;EAT BACKSLASH
22A29A	CD5782	432	CALL	BI	;BYTE 0
22A29D	CD0B88	433	CALL	CO	
22A2A0	CD5782	434	CALL	BI	;BYTE 1
22A2A3	CD0B88	435	CALL	CO	
22A2A6	CD5782	436	CALL	BI	;BYTE 2
22A2A9	CD0B88	437	CALL	CO	
22A2AC	CD5782	438	CALL	BI	;BYTE 3
22A2AF	CD0B88	439	CALL	CO	
22A2B2	CD5782	440	CALL	BI	;BYTE 4
22A2B5	CD0B88	441	CALL	CO	
22A2B8	CD5782	442	CALL	BI	;BYTE 5
22A2BB	CD0B88	443	CALL	CO	
22A2BE	CD5782	444	CALL	BI	;BYTE 6
22A2C1	CD0B88	445	CALL	CO	
22A2C4	CD5782	446	CALL	BI	;GET CR
22A2C7	CD0B88	447	CALL	CO	
22A2CA	E1	448	POP	H	
22A2CB	F1	449	POP	PSW	
22A2CC	C9	450	RET		
22		451	LCRUST:		
22A2CD	F5	452	PUSH	PSW	
22A2CE	E5	453	PUSH	H	
22A2CF	3E18	454	MVI	A,ESC	
22A2D1	CD0B88	455	CALL	CO	
22A2D4	3E26	456	MVI	A,'&'	
22A2D6	CD0B88	457	CALL	CO	
22A2D9	3E70	458	MVI	A,'p'	
22A2DB	CD0B88	459	CALL	CO	

LL82DE	3E31	460	MVI	A,'1'	
LL82E0	CD0B88	461	CALL	CD	
LL82E3	3E5E	462	MVI	A,'''	
LL82E5	CD0B88	463	CALL	CD	
LL82E8	3E11	464	MVI	A,DC1	
LL82EA	CD0B88	465	CALL	CD	
LL82ED	CD5782	466	CALL	BI	;ESC READ
LL82F0	CD5782	467	CALL	BI	;BACKSLASH READ
LL82F3	CD5782	468	CALL	BI	;P READ
LL82F6	CD5782	469	CALL	BI	;DEVICE CODE DIGIT READ
LL82F9	CD5782	470	CALL	BI	;BYTE 0 READ
LL82FC	CD5782	471	CALL	BI	;BYTE 1 READ
LL82FF	CD5782	472	CALL	BI	;BYTE 2 READ
LL8302	CD5782	473	CALL	BI	;CR READ
LL8305	E1	474	POP	H	
LL8306	F1	475	POP	PSW	
LL8307	C9	476	RET		
LL		477			
LL		478			DELAY ONE MILLISECOND
LL		479			
LL		480	D1MS:		
LL8308	C5	481	PUSH	B	
LL8309	F5	482	PUSH	PSW	
LL830A	019800	483	LXI	B,152	
LL830B	0B	484	D1MS0:	DCX	B
LL830E	78	485	MOV	A,B	
LL830F	B1	486	ORA	C	
LL8310	C20D83	487	JNZ	D1MS0	
LL8313	F1	488	POP	PSW	
LL8314	C1	489	POP	B	
LL8315	C9	490	RET		
LL001B		491	ESC	EDU	1BH
LL000D		492	CR	EDU	0DH
LL00ED		493	S8Z51A	EDU	0EDH
LL00EC		494	D8Z51A	EDU	0ECH
LL0002		495	R8RDYA	EDU	0ZH
LL0001		496	T8RDYA	EDU	01H
LL000A		497	LF	EDU	0AH
LL0005		498	EN8	EDU	05H
LL0006		499	ACK	EDU	06H
LL0011		500	DC1 EDU	11H	
LL8316	F5	501	CNTR1:	PUSH	PSW
LL8317	3E74	502		MVI	A,074H
LL8319	D3DF	503		OUT	ODFH
LL831B	3E10	504		MVI	A,TLOW
LL831D	D3DD	505		OUT	ODDH
LL831F	3E27	506		MVI	A,THIGH
LL8321	D3DD	507		OUT	ODDH
LL8323	E3	508		XTHL	
LL8324	E3	509		XTHL	
LL8325	F1	510		POP	PSW
LL8326	C9	511		RET	
LL8327	F5	512	CNTR0:	PUSH	PSW
LL8328	3E36	513		MVI	A,036H
LL832A	D3DF	514		OUT	ODFH
LL832C	3E0A	515		MVI	A,0AH
LL832E	D3DC	516		OUT	ODCH
LL8330	3E00	517		MVI	A,00H
LL8332	D3DC	518		OUT	ODCH
LL8334	E3	519		XTHL	
LL8335	E3	520		XTHL	
LL8336	F1	521		POP	PSW
LL8337	C9	522		RET	
LL		523	STINT:		
LL8338	F5	524		PUSH	PSW
LL8339	E5	525		PUSH	H

22		526	;	
22		527	;	
22		528	;	PUT 'JMP BREAK' INST. AT LOCS INT75,INT75+1,INT75+2
22	383A	529		MVI A,00H
22	383C	530		STA INT75
22	383F	531		LXI H,BREAK
22	3842	532		SHLD INT75+1
22		533	;	
22		534	;	SETUP 8214 INTERRUPT CONTROLLER
22		535	;	
22	3845	536		MVI A,03H ;BIT 7=0 FOR MODE 0
22		537		;
22		538		;
22	3847	539		OUT 007H ;BIT 0 TO 3 DEFINE INTERRUPT PRIORIRY
22		540	;	;
22		541	;;	;
22		542	;	PUT Z80 IN INTERRUPT MODE 0
22	3849	543		INM
22	384B	544		POP H
22	384C	545		POP PSM
22		546	;	
22		547	;	TURN ON INTERRUPT SYSTEM
22		548	;	
22	384D	549		EI
22	384E	550		RET
22		551	;	
22		552	;	COME HERE ON TIMER INTERRUPT
22		553	;	
22	384F	554	BREAK:	NOP
22	3850	555		PUSH PSM
22	3851	556		PUSH H
22	3852	557		PUSH B
22	3853	558		PUSH D
22		559	;	
22	3854	560		LDA FLAG
22	3857	561		DCR A
22	3858	562		STA FLAG
22		563	;	
22	385B	564		MVI A,0FFH ;MAKE OUTPUT OF
22	385D	565		OUT 0E8H ; ZERO VOLTS
22	385F	566		LDDE ;RESTORE BUFFER POINTER TO DE PAIR
22	3863	567		CALL TSTFULL ;IS BUFFER EMPTY
22		568	;	
22		569	;	IF CNT=0.AND. CNT<=9 READ FAST CHANS AND STORE
22		570	;	
22	3866	571		CALL FAST ;COLLECT FAST DATA
22		572	;	
22		573	;	IF CNT = 4 READ SLOW CHANNELS
22		574	;	
22	3869	575		LDA CNT
22	386C	576		CPI 4
22	386E	577		JNZ NOT4
22	3871	578		CALL SLOW
22		579	NOT4:	
22		580	;	
22		581	;	
22		582	;	IF CNT=9 READ TIME AND SLOW CHANS
22		583	;	
22	3874	584		LDA CNT
22	3877	585		CPI 9
22	3879	586		JNZ NOT9
22		587	;	
22	387C	588		LXI H,2*26
22	387F	589		DAD D ;ADD 2*26 TO DE PAIR TO POINT BEYOND
22	3880	590		MOV E,L
22	3881	591		MOV D,H ;PUT HL IN DE

228382	CDCA86	592	CALL	DISPLAY	;IF THERE IS TWO DIGIT PAIR READY, DISPLAY MEMORY
228385	CDFA84	593	CALL	UPBLIPS	;THERE ARE TWO BUFFER POINTERS AND COUNTER
22		594			; TO UPDATE
228388	CD5785	595	CALL	UCLK	;TIC THE CLOCK
22838B	CD4B86	596	CALL	FLIP	;TOGGLE LITE 3
22838E	CD7A88	597	CALL	AVG	
228391	CD3D85	598	CALL	UINTS	
228394	CD4785	599	CALL	RINTS	
228397	ED535788	600	SOED	SAVED	
22839B	AF	601	XRA	A	
22839C	D3E8	602	OUT	OE8H	
22839E	CD9785	603	CALL	STATE	
2283A1	CD7886	604	CALL	INTWODIG	
2283A4	C3B983	605	JMP	MODISP	
22		606			
22		607			NOT9:
22		608			
2283A7	CD7A88	609	CALL	AVG	;AVERAGE FAST CHANNELS
2283AA	CD3D85	610	CALL	UINTS	;UPDATE INTERRUPT COUNT
22		611			
2283AD	CD4785	612	CALL	RINTS	;RESET INTERRUPT COUNT WHEN NECESSARY
2283B0	AF	613	XRA	A	;MAKE OUTPUT OF
2283B1	D3E8	614	OUT	OE8H	; FIVE VOLTS
22		615			
22		616			
2283B3	CD9785	617	CALL	STATE	; PLAY WITH PBS + LITES ON CONTROL PANEL
2283B6	CD7886	618	CALL	INTWODIG	;LOOK FOR FOR TWO DIGIT PAIR
22		619			MODISP:
2283B9	3E03	620	MVI	A,03H	
2283BB	D3D7	621	OUT	0D7H	
2283BD	D1	622	POP	D	
2283BE	C1	623	POP	B	
2283BF	E1	624	POP	H	
2283C0	F1	625	POP	PSW	
2283C1	FB	626	EI		
2283C2	C9	627	RET		
22		628			FAST:
2283C3	3E00	629	MVI	A,0	
2283C5	CD6185	630	CALL	ADCO	
2283C8	CDEB84	631	CALL	STORE	
22		632			
2283CB	3E00	633	MVI	A,0	;DELE COLUMN CHANNEL
2283CD	CD6185	634	CALL	ADCO	; READ ADC CHANNEL
2283D0	CDEB84	635	CALL	STORE	; PUT IN BUFFER RAM
22		636			
2283D3	3E05	637	MVI	A,5	;THETADOT CHANNEL
2283D5	CD6185	638	CALL	ADCO	; READ ADC CHANNEL
2283D8	CDEB84	639	CALL	STORE	; PUT IN BUFFER RAM
22		640			
2283DB	3E07	641	MVI	A,7	;HZ-NORMAL ACCEL CHANNEL
2283DD	CD6185	642	CALL	ADCO	; READ ADC CHANNEL
2283E0	CDEB84	643	CALL	STORE	; PUT IN RAM BUFFER
22		644			
2283E3	3E08	645	MVI	A,8	;DELA-ROLL WHEEL
2283E5	CD6185	646	CALL	ADCO	; READ ADC CHANNEL
2283E8	CDEB84	647	CALL	STORE	; PUT IN RAM BUFFER
22		648			
2283EB	3E09	649	MVI	A,9	;DELR-PEDALS CHANNEL
2283ED	CD6185	650	CALL	ADCO	; READ ADC CHANNEL
2283F0	CDEB84	651	CALL	STORE	; PUT IN RAM BUFFER
22		652			
2283F3	3E0B	653	MVI	A,11	;BETA-SIDESLIP CHANNEL
2283F5	CD6185	654	CALL	ADCO	; READ ADC CHANNEL
2283F8	CDEB84	655	CALL	STORE	; PUT IN RAM BUFFER
22		656			
2283FB	3E0D	657	MVI	A,13	;P-ROLL RATE CHANNEL

2283FD	CD6185	658		CALL	ADCO	; READ ADC CHANNEL
228400	CDEB84	659		CALL	STORE	; PUT IN RAM BUFFER
22		660	;			
228403	3E0E	661		MVI	A,14	;R-YAW RATE CHANNEL
228405	CD6185	662		CALL	ADCO	; READ ADC CHANNEL
228408	CDEB84	663		CALL	STORE	; PUT IN RAM BUFFER
22		664	;			
22840B	3E0F	665		MVI	A,15	;RY-LATERAL ACCEL CHANNEL
22840D	CD6185	666		CALL	ADCO	; READ ADC CHANNEL
228410	CDEB84	667		CALL	STORE	; PUT IN RAM BUFFER
22		668	;			
228413	3E15	669		MVI	A,21	;RX-LONGITUDINAL ACCEL CHANNEL
228415	CD6185	670		CALL	ADCO	; READ ADC CHANNEL
228418	CDEB84	671		CALL	STORE	; PUT IN RAM BUFFER
22		672	;			
22841B	3E19	673		MVI	A,25	;ALPHA-ANGLE OF ATTACK CHANNEL
22841D	CD6185	674		CALL	ADCO	; READ ADC CHANNEL
228420	CDEB84	675		CALL	STORE	; PUT IN RAM BUFFER
228423	C9	676		RET		
22		677	SLOW;			
22		678	;			
228424	CD7E85	679		CALL	DME	;DME DISTANCE
228427	CDEB84	680		CALL	STORE	; PUT IN BUFFER RAM
22		681	;			
22842A	3E01	682		MVI	A,1	;DELTA-THROTTLE HANDLE
22842C	CD6185	683		CALL	ADCO	; READ ADC CHANNEL
22842F	CDEB84	684		CALL	STORE	; PUT IN RAM BUFFER
22		685	;			
228432	3E02	686		MVI	A,2	;DELTA-FLAP LEVER CHANNEL
228434	CD6185	687		CALL	ADCO	; READ ADC CHANNEL
228437	CDEB84	688		CALL	STORE	; PUT IN RAM BUFFER
22		689	;			
22843A	3E03	690		MVI	A,3	;DELTA-ELEVATOR TRIM CHANNEL
22843C	CD6185	691		CALL	ADCO	; READ ADC CHANNEL
22843F	CDEB84	692		CALL	STORE	; PUT IN RAM BUFFER
22		693	;			
228442	3E04	694		MVI	A,4	;THETA-PITCH ANGLE CHANNEL
228444	CD6185	695		CALL	ADCO	; READ ADC CHANNEL
228447	CDEB84	696		CALL	STORE	; PUT IN RAM BUFFER
22		697	;			
22844A	3E06	698		MVI	A,6	;U-VELOCITY CHANNEL
22844C	CD6185	699		CALL	ADCO	; READ ADC CHANNEL
22844F	CDEB84	700		CALL	STORE	; PUT IN RAM BUFFER
22		701	;			
228452	3E0A	702		MVI	A,10	;PSI-HEADING ANGLE CHANNEL
228454	CD6185	703		CALL	ADCO	; READ ADC CHANNEL
228457	CDEB84	704		CALL	STORE	; PUT IN RAM BUFFER
22		705	;			
22845A	3E0C	706		MVI	A,12	;PHI-ROLL ANGLE CHANNEL
22845C	CD6185	707		CALL	ADCO	; READ ADC CHANNEL
22845F	CDEB84	708		CALL	STORE	; PUT IN RAM BUFFER
22		709	;			
228462	3E10	710		MVI	A,16	;DELTA-RUDDER TRIM CHANNEL
228464	CD6185	711		CALL	ADCO	; READ ADC CHANNEL
228467	CDEB84	712		CALL	STORE	; PUT IN RAM BUFFER
22		713	;			
22846A	3E11	714		MVI	A,17	;DELTA-AILERON TRIM CHANNEL
22846C	CD6185	715		CALL	ADCO	; READ ADC CHANNEL
22846F	CDEB84	716		CALL	STORE	; PUT IN RAM BUFFER
22		717	;			
228472	3E12	718		MVI	A,18	;DELTA-ELEVATOR POSITION CHANNEL
228474	CD6185	719		CALL	ADCO	; READ ADC CHANNEL
228477	CDEB84	720		CALL	STORE	; PUT IN RAM BUFFER
22		721	;			
22847A	3E13	722		MVI	A,19	;DELTA-THROTTLE POSITION CHANNEL
22847C	CD6185	723		CALL	ADCO	; READ ADC CHANNEL



22847F	CDEB84	724	CALL	STORE	; PUT IN RAM BUFFER
22		725			
228482	3E14	726	MVI	A,20	;DELF-FLAP POSIYION CHANNEL
228484	CD6185	727	CALL	ADCO	; READ ADC CHANNEL
228487	CDEB84	728	CALL	STORE	; PUT IN RAM BUFFER
22		729			
22848A	3E16	730	MVI	A,22	;DELA-AILERON POSITION CHANNEL
22848C	CD6185	731	CALL	ADCO	; READ ADC CHANNEL
22848F	CDEB84	732	CALL	STORE	; PUT IN RAM BUFFER
22		733			
228492	3E17	734	MVI	A,23	;DELR-RUDDER POSITION CHANNEL
228494	CD6185	735	CALL	ADCO	; READ ADC CHANNEL
228497	CDEB84	736	CALL	STORE	; PUT IN RAM BUFFER
22		737			
22849A	3E18	738	MVI	A,24	;N1LOC-N1 LOCALISER CHANNEL
22849C	CD6185	739	CALL	ADCO	; READ ADC CHANNEL
22849F	CDEB84	740	CALL	STORE	; PUT IN RAM BUFFER
22		741			
2284A2	3E1A	742	MVI	A,26	;ALPHA-PORT ALPHA CHANNEL
2284A4	CD6185	743	CALL	ADCO	; READ ADC CHANNEL
2284A7	CDEB84	744	CALL	STORE	; PUT IN RAM BUFFER
22		745			
2284AA	3E1B	746	MVI	A,27	;ALPHA-STARBOARD ALPHA CHANNEL
2284AC	CD6185	747	CALL	ADCO	; READ ADC CHANNEL
2284AF	CDEB84	748	CALL	STORE	; PUT IN RAM BUFFER
22		749			
2284B2	3E1C	750	MVI	A,28	;LOCMLS-MLS LOCALIZER CHANNEL
2284B4	CD6185	751	CALL	ADCO	; READ ADC CHANNEL
2284B7	CDEB84	752	CALL	STORE	; PUT IN RAM BUFFER
22		753			
2284BA	3E1D	754	MVI	A,29	;GSMLS-MLS GLIDE SLOPE CHANNEL
2284BC	CD6185	755	CALL	ADCO	; READ ADC CHANNEL
2284BF	CDEB84	756	CALL	STORE	; PUT IN RAM BUFFER
22		757			
2284C2	3E1E	758	MVI	A,30	;LOCN2-N2 LOCALIZER CHANNEL
2284C4	CD6185	759	CALL	ADCO	; READ ADC CHANNEL
2284C7	CDEB84	760	CALL	STORE	; PUT IN RAM BUFFER
22		761			
2284CA	3E1F	762	MVI	A,31	;IDELF-FLAP COMMAND CHANNEL
2284CC	CD6185	763	CALL	ADCO	; READ ADC CHANNEL
2284CF	CDEB84	764	CALL	STORE	; PUT IN RAM BUFFER
22		765			
2284D2	CD8385	766	CALL	DIGH	;H
2284D5	CDEB84	767	CALL	STORE	; PUT IN RAM BUFFER
22		768			
2284D8	CD8985	769	CALL	DIGLI	;LIGHTS
2284DB	CDEB84	770	CALL	STORE	; PUT IN RAM BUFFER
22		771			
2284DE	CD8D85	772	CALL	DIGMOD	;MODE SWITCHES
2284E1	CDEB84	773	CALL	STORE	; PUT IN RAM BUFFER
22		774			
2284E4	CD9385	775	CALL	DIGTIM	;TIME
2284E7	CDEB84	776	CALL	STORE	; PUT IN RAM BUFFER
2284EA	C9	777	RET		
22		778	STORE:		
22		779			
22		780			
22		781			
22		782			TAKE CONTENTS OF HL REGISTER
22		783			STORE AT DOUBLE BYTE POINTED
22		784			TO BY DE REGISTER.
2284EB	F5	785	PUSH	PSW	
2284EC	7D	786	MOV	A,L	
2284ED	12	787	STAX	D	
2284EE	13	788	INX	D	
2284EF	7C	789	MOV	A,H	

2284F0	12	790	STAX	D	
2284F1	13	791	INX	D	
2284F2	F1	792	POP	PSW	
2284F3	C9	793	RET		
22		794	;		
22		795	;		
22		796	UFBUFFS:		
22		797	;		
22		798	;		
22		799	;		
22		800	;		
22		801	;		THERE ARE TWO POINTERS
22		802	;		AND ONE COUNTER
22		803	;		TO BE UPDATED WHEN CURRENT
22		804	;		BUFFER IS FULL.
22		805	;		
22		806	;		FWHICHB IS FROM 0 TO 9
22		807	;		AND INDICATES THE CURRENT BUFFER
22		808	;		BEING FILLED
22		809	;		
22		810	;		SAVE POINTS TO THE BYTE OF
22		811	;		THE CURRENT BUFFER TO BE FILLED.
22		812	;		
22		813	;		REMAIN CONTAINS THE NUMBER
22		814	;		OF UNFILED BYTES IN CURRENT BUFFER
2284F4	F5	815	PUSH	PSW	
2284F5	E5	816	PUSH	H	
2284F6	C5	817	PUSH	B	
2284F7	2A5988	818	LHLD	REMAIN	;
2284FA	014C00	819	LXI	B, BYTPERSEC	; BYTPERSEC BYTES FILLED PER SECOND
2284FD	AF	820	XRA	A	; CARRY=0
2284FE	ED42	821	DSBC	B	
228500	225988	822	SHLD	REMAIN	; REMAIN=REMAIN-BYTPERSEC
22		823	;		
22		824	;		
22		825	;		IS REMAIN >= BYTPERSEC
228503	AF	826	XRA	A	; CARRY=0
228504	ED42	827	DSBC	B	
228506	F23985	828	JP	ROOM	; IF S=0, HL >= BC
22		829	;		
22		830	;		
22		831	;		CAN NOT FIT
22		832	;		ANOTHER BLOCK OF BYTPERSEC BYTES
22		833	;		IN CURRENT BUFFER
22		834	;		
228509	CD9487	835	CALL	SETFULL	; MARK CURRENT BUFFER FULL
22		836	;		
22850C	210008	837	LXI	H, 2048	
22850F	225988	838	SHLD	REMAIN	; REMAIN=2048
22		839	;		
228512	3A5B88	840	LDA	FWHICHB	; SWITCH TO NEXT BUFFER
228515	3C	841	INR	A	;
228516	325B88	842	STA	FWHICHB	;
228519	FE0A	843	CPI	10	
22851B	C22D85	844	JNZ	SW	
22		845	;		
22		846	;		
22851E	3E00	847	MVI	A, 0	
228520	325B88	848	STA	FWHICHB	
228523	110090	849	LXI	D, BUFF0	
228526	ED537688	850	SEED	CURRBUF	
22852A	C33985	851	JMP	ROOM	
22		852	;		
22852D	2A7688	853	SW:	LHLD	CURRBUF ; BASE ADDRESS OF CURRENT BUFFER
228530	010008	854		LXI	B, 2048
228533	09	855		DAD	B ; INCREMENT BY 2048

228534	227688	856		SHLD	CURRBUF	;UPDATED BASE ADDRESS SAVED
228537	54	857		MOV	D,H	;AND PUT INTO
228538	5D	858		MOV	E,L	; THE DE PAIR
22		859				
22		860	ROOM:			
228539	C1	861		POP	B	
22853A	E1	862		POP	H	
22853B	F1	863		POP	PSW	
22853C	C9	864		RET		
22		865	UINTS:			
22853D	F5	866		PUSH	PSW	
22853E	3A5E88	867		LDA	CNT	
228541	3C	868		INR	A	
228542	325E88	869		STA	CNT	
228545	F1	870		POP	PSW	
228546	C9	871		RET		
22		872	RINTS:			
228547	F5	873		PUSH	PSW	
228548	3A5E88	874		LDA	CNT	
22854B	FE0A	875		CPI	10	
22854D	C25585	876		JNZ	NOT10	
228550	3E00	877		MVI	A,0	
228552	325E88	878		STA	CNT	
22		879	NOT10:			
228555	F1	880		POP	PSW	
228556	C9	881		RET		
22		882	UCLK:			
228557	E5	883		PUSH	H	
228558	2A5C88	884		LHLD	TIM	
22855B	Z3	885		INX	H	
22855C	225C88	886		SHLD	TIM	
22855F	E1	887		POP	H	
228560	C9	888		RET		
22		889	ADCO:			
228561	320130	890		STA	ADDAM+01H	
228564	3E01	891		MVI	A,01	
228566	320030	892		STA	ADDAM+00H	
228569	3A0030	893	BUSY	LDA	ADDAM+00H	
22856C	07	894		RLC		
22856D	026985	895		JNC	BUSY	
228570	2A0430	896		LHLD	ADDAM+04H	
228573	C9	897		RET		
22		898	CDC0:			
228574	6F	899		MOV	L,A	
22		900				
228575	2600	901		MVI	H,0	
228577	C9	902		RET		
22		903	BDC0:			
228578	6F	904		MOV	L,A	
228579	3A5E88	905		LDA	CNT	
22857C	67	906		MOV	H,A	
22857D	C9	907		RET		
22		908	DNE:			
22857E	2E00	909		MVI	L,0	
228580	2600	910		MVI	H,0	
228582	C9	911		RET		
22		912	DIGH:			
22		913		MVI	L,34	
22		914		MVI	H,0	
228583	DBE4	915		IN	ALTPORT	;ALTIMETER READING
228585	6F	916		MOV	L,A	
228586	2600	917		MVI	H,0	
228588	C9	918		RET		
22		919	DIGLI:			
22		920		MVI	L,35	
22		921		MVI	H,0	

2A5288	922	LHLD	LIGHTS	
C9	923	RET		
	924	DIGMOD:		
DRES	925	IN	PUSHPORT	
6F	926	MOV	L,A	
2600	927	MVI	H,0	
	928	; MVI	L,36	
	929	; MVI	H,0	
C9	930	RET		
	931	DIGTIM:		
2A5C88	932	LHLD	TIM	
C9	933	RET		
	934	STATE:		
	935	; THISMACHINE HAS TWO STATES		
	936	; STATE 0	THE MACHINE STAYS IN THIS STATE FOR 30 SECS.	
	937	; AFTER 30 SECS. ELAPSE, IT TURNS ON THE PROPER LIGHT		
	938	; AND SHIFTS TO STATE 1.		
	939	; STATE 1	THE MACHINE STAYS IN STATE 1 UNTIL THE PROPER	
	940	; PUSHBUTTON IS DEPRESSED.(LIGHT X GOES WITH PB X, ETC)		
	941	; THE CORRESPONDING LIGHT IS TURNED OFF AND THE		
	942	; MACHINE SHIFTS TO STATE 0.		
	943	;		
F5	944	PUSH	PSW	
E5	945	PUSH	H	
C5	946	PUSH	B	
3A4E88	947	LDA	ST	
B7	948	DRA	A	;SET THE FLAGS
C2C185	949	JNZ	STATE1	
	950	STATE0:		
212C01	951	LXI	H,THSEDY	;LOAD THE NUMBER OF TIMER CLICKS NEEDED FOR 30 SEC
AF	952	XRA	A	;CLEAR CARRY
ED4B5088	953	LBCD	PTIM	
ED42	954	DSEC	B	
C2B785	955	JNZ	BPTIM	
CDDA85	956	CALL	TONE	
CD3D86	957	CALL	TONE	;STATE=1
C3D685	958	JMP	BACK	
	959	BPTIM:		
2A5088	960	LHLD	PTIM	
23	961	INX	H	
225088	962	SHLD	PTIM	
C3D685	963	JMP	BACK	
	964	STATE1:		
CD2586	965	CALL	PB	;RETURN PUSHBUTTON STATUS IN Z FLAG
C2D685	966	JNZ	BACK	
	967	PBON:		
CDFF85	968	CALL	TOFFL	;TURN OFF LITE
CD4586	969	CALL	TOFFS	;STATE=0
CD1C86	970	CALL	CPTIM	;PTIM = 0
CD5C86	971	CALL	SMPBLITE	;SWITCH TO NEXT PUSHBUTTON + LITE SET
C3D685	972	JMP	BACK	
	973	BACK:		
C1	974	POP	B	
E1	975	POP	H	
F1	976	POP	PSW	
C9	977	RET		
	978	TONE:		
F5	979	PUSH	PSW	
3A5688	980	LDA	BINARY	
FE00	981	CPI	0	
C2EF85	982	JNZ	ON2	
3A5288	983	LDA	LIGHTS	
E6FE	984	ANI	OFFH	
D3C5	985	OUT	LITEPORT	;BIT 0 PORT B 5 VOLTS
325288	986	STA	LIGHTS	
F1	987	POP	PSW	

2285EE	C9	988		RET	
22		989	ON2:		
2285EF	3A5288	990		LDA	LIGHTS
2285F2	E6FD	991		ANI	0FDH ;
2285F4	D3C5	992		OUT	LITEPORT ;BIT 1 PORT B 5 VOLTS
2285F6	325288	993		STA	LIGHTS
2285F9	F1	994		POP	PSW
2285FA	C9	995		RET	
22		996	TUFFL:		
2285FB	F5	997		PUSH	PSW
2285FC	3A5688	998		LDA	BINRY
2285FF	FE00	999		CPI	0
228601	C21086	1000		JNZ	OFF2
228604	3A5288	1001		LDA	LIGHTS
228607	F601	1002		ORI	01H ;
228609	D3C5	1003		OUT	LITEPORT ;BIT 0 PORT B 0 VOLTS
22860B	325288	1004		STA	LIGHTS
22860E	F1	1005		POP	PSW
22860F	C9	1006		RET	
22		1007	OFF2:		
228610	3A5288	1008		LDA	LIGHTS ;
228613	F602	1009		ORI	02H
228615	D3C5	1010		OUT	LITEPORT ;BIT 0 PORT B 0 VOLTS
228617	325288	1011		STA	LIGHTS
22861A	F1	1012		POP	PSW
22861B	C9	1013		RET	
22		1014	CPTIM:		
22861C	E5	1015		PUSH	H
22861D	210000	1016		LXI	H,0
228620	225088	1017		SHLD	PTIM ;CLEAR PTIM
228623	E1	1018		POP	H
228624	C9	1019		RET	
22		1020	PB:		
228625	3A5688	1021		LDA	BINRY
228628	FE00	1022		CPI	0
22862A	C23586	1023		JNZ	PB2
22862D	D8E5	1024		IN	PUSHPORT ;PUSHBUTTON STATUS
22862F	325488	1025		STA	MODES
228632	E601	1026		ANI	01H ;BIT 0 PORT B
228634	C9	1027		RET	;STATUS RETURNED IN Z FLAG
22		1028	PB2:		
228635	D8E5	1029		IN	PUSHPORT
228637	325488	1030		STA	MODES
22863A	E602	1031		ANI	02H ;BIT 1 PORT B
22863C	C9	1032		RET	
22		1033	TUNS:		
22863D	F5	1034		PUSH	PSW
22863E	3E01	1035		MVI	A,01H ;
228640	324E88	1036		STA	ST ;STATE=1
228643	F1	1037		POP	PSW
228644	C9	1038		RET	
22		1039	TOFFS:		
228645	F5	1040		PUSH	PSW
228646	3E00	1041		MVI	A,0
228648	324E88	1042		STA	ST
22864B	F1	1043		POP	PSW
22864C	C9	1044		RET	
22		1045	FLIP:		
22		1046	;		;TOGGLE LIGHT 3, TOGGLE LIGHT 4 TOGETHER
22864D	F5	1047		PUSH	PSW
22864E	3A5288	1048		LDA	LIGHTS
228651	EE04	1049		XRI	04H ;FLIP BIT 2
228653	EE08	1050		XRI	08H ;FLIP BIT 3
228655	325288	1051		STA	LIGHTS
228658	D3C5	1052		OUT	LITEPORT
22865A	F1	1053		POP	PSW

22865B	C9	1054	RET		
22		1055	SMPBLITE:		
22		1056	;	IF YOU ARE USING PBO AND LITE0,	
22		1057	;	USE PB1 AND LITE1.	
22		1058	;	IF YOU ARE USING PB1 AND LITE1,	
22		1059	;	USE PBO AND LITE0.	
22		1060	;		
22865C	F5	1061	PUSH	PSW	
22865D	3A5688	1062	LDA	BINRY	
228660	EE01	1063	XRI	01H	
228662	325688	1064	STA	BINRY	
228665	F1	1065	POP	PSW	
228666	C9	1066	RET		
22		1067	CTIM:		
228667	E5	1068	PUSH	H	
228668	210000	1069	LXI	H,0	;HL=0
228668	225C88	1070	SHLD	TIM	;SECOND COUNTER = 0
22866E	E1	1071	POP	H	
22866F	C9	1072	RET		
22		1073	SETCDIG:		
22		1074	;		
22		1075	;	SET DIGIT COUNTER CNTDIG	
22		1076	;		
228670	F5	1077	PUSH	PSW	
228671	3E00	1078	MVI	A,0	
228673	324D88	1079	STA	CNTDIG	;CNTDIG=0
228676	F1	1080	POP	PSW	
228677	C9	1081	RET		
22		1082	INTMODIG:		
228678	E5	1083	PUSH	H	
228679	C5	1084	PUSH	B	
22867A	D5	1085	PUSH	D	
22		1086			;CHECK TO SEE IF THERE IS
22		1087			;A TWO DIGIT INPUT READY
22		1088			;
22		1089			;IF THERE IS NOT,
22		1090			; RETURN WITH Z SET
22		1091			;
22		1092			;IF THERE IS,
22		1093			; RETURN WITH Z RESET
22		1094			;
22		1095			;
22867B	CDB186	1096	CALL	D1	;GET DIGIT IF WAITING
22867E	CAAD86	1097	JZ	INPUTR	; IF Z SET, NOTCHING WAITING
22		1098	;		
22		1099	;		
22		1100			;Z NOT SET, SO DIGIT IN ACC
228681	E60F	1101	ANI	0FH	;CONVERT ASCII DIGIT TO BINARY DIGIT
22		1102	CALL	HIMP	
22		1103	CALL	CRLF	
228683	57	1104	MOV	D,A	;SAVE DIGIT IN D
228684	3A4D88	1105	LDA	CNTDIG	;CNTDIG IS DIGIT COUNTER
228687	3C	1106	INR	A	
228688	324D88	1107	STA	CNTDIG	
22868B	FE02	1108	CPI	02H	;
22868D	CA9886	1109	JZ	INPUTE	;IF Z SET, COUNT IS 2
22		1110	;		
22		1111	;		
22		1112			;HAVE INPUT IN D, SAVE IN B
228690	7A	1113	MOV	A,D	;
228691	324B88	1114	STA	INPUTS	;SAVE FIRST INPUT DIGIT
228694	AF	1115	XRA	A	;Z IS SET
228695	C3AD86	1116	JMP	INPUTR	
22		1117	INPUTE:		
228698	3A4B88	1118	LDA	INPUTS	;MOVE FIRST INPUT DIGIT IN ACC
22869B	07	1119	RLC		

22869C	07	1120	RLC		
22869D	07	1121	RLC		
22869E	47	1122	MOV	B,A	; (B)=8*(INPUTS)
22869F	3A4B88	1123	LDA	INPUTS	;
2286A2	87	1124	ADD	A	; (A)=2*(INPUTS)
2286A3	80	1125	ADD	B	; (A)=2*(INPUTS)+8*(INPUTS)=10*(INPUTS)
2286A4	82	1126	ADD	D	; ADD IN SECOND INPUT DIGIT
2286A5	324C88	1127	STA	TWODIG	
2286A8	3E00	1128	MVI	A,0	
2286AA	324D88	1129	STA	CNTDIG	; CLEAR THE COUNTER
22		1130	INPUTR:		
2286AD	D1	1131	POP	D	
2286AE	C1	1132	POP	B	
2286AF	E1	1133	POP	H	
2286B0	C9	1134	RET		
22		1135	DI:		
22		1136	;		ACC AND FLAGS ARE CHANGED
22		1137	;		GET INPUT IF WAITING
22		1138	;		OTHERWISE RETURN WITH Z SET
22		1139	;		
22		1140	;		SEE IF INPUT IS ADECIMAL DIGIT,
22		1141	;		IF NOT RETURN WITH Z SET
22		1142	;		
22		1143	;		IF INPUT IS A DECIMAL DIGIT,
22		1144	;		ECHO IT AND RETURN IN ACC
22		1145	;		
22		1146	;		
2286B1	DBCD	1147	IN	S8251	
2286B3	E602	1148	ANI	RXR0Y	; IS THERE INPUT DATA YET
2286B5	C8	1149	RZ		; IF Z IS SET, RETURN
22		1150	;		
22		1151	;		READ THE CHAR
22		1152	;		
2286B6	DBCC	1153	IN	D8251	; GET CHAR
2286B8	E67F	1154	ANI	07FH	; CHOP OFF PARITY
22		1155	;		
22		1156	;		TEST FOR DIGIT FROM 0 TO 9
22		1157	;		
2286BA	FE30	1158	CPI	30H	; COMPARE WITH ASCII 0
2286BC	FAC886	1159	JM	DINODIG	; JUMP IF LESS THAN
2286BF	FE3A	1160	CPI	3AH	; COMPARE WITH ASCII COLON
2286C1	F2C886	1161	JP	DINODIG	; JUMP IF GREATER OR EQUAL
2286C4	CD0B88	1162	CALL	CD	; HAVE LEGAL DIGIT IN ACC, Z IS RESET
2286C7	C9	1163	RET		
22		1164	;		
22		1165	;		
22		1166	DINODIG:		
2286C8	AF	1167	XRA	A	; Z IS SET
2286C9	C9	1168	RET		
22		1169	DISPLAY:		
2286CA	F5	1170	PUSH	PSW	
2286CB	E5	1171	PUSH	H	
2286CC	C5	1172	PUSH	B	
22		1173			; DISPLAY MEMORY LOCATION
22		1174			; CORRESPONDING TO TWODIG ADDRESS
22		1175			;
2286CD	3A5E88	1176	LDA	CNT	; INTERRUPT COUNT LOADED IN ACC
2286D0	FE09	1177	CPI	9	; IS THIS THE NINTH INTERRUPT
2286D2	C2F386	1178	JNZ	DISPLAYR	; RETURN IF NOT NINE
22		1179			;
22		1180			;
2286D5	3A4C88	1181	LDA	TWODIG	; LOAD TWO DIGIT NUMBER
2286D8	FE00	1182	CPI	0	; IF IT IS ZERO, NOTHING TO DISPLAY YET
2286DA	CAF386	1183	JZ	DISPLAYR	; SO RETURN
22		1184			;
22		1185			;

LL86D0	87	1186	ADD	A	FORM BYTE OFFSET IN ACC
LL86DE	D602	1187	SUI	2	VALUE OF 1 IS AN OFFSET OF ZERO
LL		1188			
LL86E0	2600	1189	MVI	H,0	MOVE ACC OFFSET
LL86E2	6F	1190	MOV	L,A	HL HAS ACC OFFSET
LL86E3	ED4B5788	1191	LBCD	SAVEDE	BASE ADDRESS OF CURRENT STORAGE IN BC
LL86E7	09	1192	DAD	B	ADDED TO OFFSET TO FORM POINTER TO
LL		1193			MEMORY LOCATION YOU WANT TO SEE
LL		1194			
LL86E8	CD2A87	1195	CALL	CRLF	
LL86EB	CDFF86	1196	CALL	HDMP2	
LL		1197			
LL		1198			
LL		1199	CALL	CRLF	
LL		1200	LDA	TWODIG	
LL		1201	CALL	HDMP	
LL		1202	CALL	CRLF	
LL		1203	LXI	H,SAVEDE	
LL		1204	CALL	HDMP2	
LL		1205	CALL	CRLF	
LL86EE	3E00	1206	MVI	A,0	ZERO
LL86F0	324C88	1207	STA	TWODIG	TWODIG
LL		1208			
LL		1209			
LL		1210	DISPLAY:		
LL86F3	C1	1211	POP	B	
LL86F4	E1	1212	POP	H	
LL86F5	F1	1213	POP	PSW	
LL86F6	C9	1214	RET		
LL		1215	DUMP THE CONTENTS OF MEMORY IN HEX		
LL		1216	H HOLDS STARTING ADDRESS OF DUMP		
LL		1217	A REG IS USED IN HDMP		
LL86F7	F5	1218	HDMP2:	PUSH	PSW
LL86F8	E5	1219		PUSH	H
LL86F9	23	1220		INX	H
LL86FA	7E	1221		MOV	A,H
LL86FB	CD0987	1222		CALL	HDMP
LL86FE	2B	1223		DCX	H
LL86FF	7E	1224		MOV	A,H
LL8700	CD0987	1225		CALL	HDMP
LL8703	CD2A87	1226		CALL	CRLF
LL8706	E1	1227		POP	H
LL8707	F1	1228		POP	PSW
LL8708	C9	1229		RET	
LL		1230			
LL8709	F5	1231	HDMP:	PUSH	PSW
LL870A	F5	1232		PUSH	PSW
LL870B	E6F0	1233		ANI	0F0H
LL870D	0F	1234		RRC	
LL870E	0F	1235		RRC	
LL870F	0F	1236		RRC	
LL8710	0F	1237		RRC	
LL8711	CD2287	1238		CALL	BINHE
LL8714	CD0B88	1239		CALL	CO
LL8717	F1	1240		POP	PSW
LL8718	E60F	1241		ANI	0FH
LL871A	CD2287	1242		CALL	BINHE
LL871D	CD0B88	1243		CALL	CO
LL8720	F1	1244		POP	PSW
LL8721	C9	1245		RET	
LL8722	C630	1246	BINHE:	ADI	30H
LL8724	FE3A	1247		CPI	3AH
LL8726	D8	1248		RC	
LL8727	C607	1249		ADI	7H
LL8729	C9	1250		RET	
LL		1251			
					CRLF USES ONLY THE AREC



22872A	F5	1252	CRLF:	PUSH	PSW	
22872B	3E0D	1253		MVI	A,0DH	
22872D	CD0B88	1254		CALL	CD	
228730	3E0A	1255		MVI	A,0AH	
228732	CD0B88	1256		CALL	CD	
228735	F1	1257		POP	PSW	
228736	C9	1258		RET		
22		1259	;DATAOVRUN:			
22		1260	;	ARE WE FILLING FASTER THAN WE ARE EMPTYING		
22		1261	;	PUSH	PSW	
22		1262	;	PUSH	B	
22		1263	;	LDA	FWHICB	
22		1264	;	MOV	B,A	
22		1265	;	LDA	FWHICB	
22		1266	;	CMF	B	
22		1267	;	JNZ	D1	
22		1268	;			DATA OVERRUN
22		1269	;	MVI	A,'0'	
22		1270	;	CALL	BO	
22		1271	;	HLT		
22		1272	;	D1:		
22		1273	;	POP	B	
22		1274	;	POP	PSW	
22		1275	;	RET		
22		1276	;	VALIDMP:		
22		1277	;			LET THE FILLER CATCHUP WITH EMPTIER
22		1278	;	PUSH	PSW	
22		1279	;	PUSH	B	
22		1280	;	LDA	FILLONE	
22		1281	;	CPI	0	
22		1282	;	JNZ	V1	
22		1283	;			;ONE BUFFER HAS NOT YET BEEN FILLED
22		1284	;	V2:	LDA	FWHICB
22		1285	;	CPI	0	
22		1286	;	MVI	A,'W'	
22		1287	;	CALL	CD	
22		1288	;	JZ	V2	
22		1289	;			;ONE BUFFER HAS BEEN FILLED
22		1290	;	MVI	A,1	
22		1291	;	STA	FILLONE	
22		1292	;	V1:		
22		1293	;			;MAKE SURE FILLER STAYS AHEAD OF EMPTIER
22		1294	;	LDA	FWHICB	
22		1295	;	MOV	B,A	
22		1296	;	LDA	FWHICB	
22		1297	;	CMF	B	
22		1298	;	LDA	FWHICB	
22		1299	;	ADI	30H	
22		1300	;	CALL	CD	
22		1301	;	JZ	V1	
22		1302	;	POP	B	
22		1303	;	POP	PSW	
22		1304	;	RET		
22		1305	;	INITSEMA:		
22		1306	;			;MARK ALL BUFFERS EMPTY
228737	F5	1307		PUSH	PSW	
228738	C5	1308		PUSH	B	
228739	E5	1309		PUSH	H	
22873A	216A88	1310		LXI	H,SEMAPHORE	
22873D	060A	1311		MVI	B,10	
22873F	3645	1312	S1:	MVI	M,'E'	
228741	23	1313		INX	H	;ADDRESS NEXT SEMAPHORE
228742	05	1314		DCR	B	;ONE LESS SEMAPHORE TO INITIALISE
228743	C23F87	1315		JNZ	S1	;REPEAT UNTIL ALL SEMAPHORES ARE INITIALISED
228746	E1	1316		POP	H	
228747	C1	1317		POP	B	

008748	F1	1318	POP	PSW	
008749	C9	1319	RET		
00		1320	TSTFULL:		
00		1321			;WAIT UNTIL BUFFER EMPTY (INFINITE LOOP!)
00874A	F5	1322	PUSH	PSW	
00874B	C5	1323	PUSH	B	
00874C	E5	1324	PUSH	H	
00874D	216A88	1325	LXI	H,SEMAPHORE	
008750	3A5B88	1326	LDA	FMHICB	
008753	0600	1327	MVI	B,0	
008755	4F	1328	MOV	C,A	
008756	09	1329	DAD	B	; (HL):= SEMAPHORE+(FMHICB)
008757	7E	1330	MOV	A,H	; (A):= (SEMAPHORE+(FMHICB))
008758	FE46	1331	CPI	'F'	;SEE IF BUFFER FULL
00875A	CC6187	1332	CZ	OVRUN	;WAIT TIL EMPTY
00875D	E1	1333	POP	H	
00875E	C1	1334	POP	B	
00875F	F1	1335	POP	PSW	
008760	C9	1336	RET		
00		1337	OVRUN:		
008761	3E4F	1338	MVI	A,'O'	
008763	CD0B88	1339	CALL	CD	
008766	3E56	1340	MVI	A,'V'	
008768	CD0B88	1341	CALL	CD	
00876B	3A5B88	1342	LDA	FMHICB	
00876E	C641	1343	ADI	'A'	
008770	CD0B88	1344	CALL	CD	
008773	C30000	1345	JMP	0	
00		1346	TSTEMPTY:		
00		1347			;WAIT UNTIL BUFFER FULL
008776	F5	1348	PUSH	PSW	
008777	C5	1349	PUSH	B	
008778	E5	1350	PUSH	H	
008779	216A88	1351	LXI	H,SEMAPHORE	
00877C	3A6888	1352	LDA	EMHICB	
00877F	0600	1353	MVI	B,0	
008781	4F	1354	MOV	C,A	
008782	09	1355	DAD	B	
008783	7E	1356	EMPTY1: MOV	A,H	; (A):=(SEMAPHORE+(EMHICB))
008784	FE45	1357	CPI	'E'	;SEE IF BUFFER EMPTY
008786	F5	1358	PUSH	PSW	;SAVE Z FLAG
008787	3A6888	1359	LDA	EMHICB	
00878A	C630	1360	ADI	'0'	;CONVERT TO ASCII
00		1361	; CALL	CD	
00878C	F1	1362	POP	PSW	;RESTORE Z FLAG
00878D	CA8387	1363	JZ	EMPTY1	;WAIT UNTIL FULL
008790	E1	1364	POP	H	
008791	C1	1365	POP	B	
008792	F1	1366	POP	PSW	
008793	C9	1367	RET		
00		1368	SETFULL:		
00		1369			;MARK BUFFER FULL
008794	F5	1370	PUSH	PSW	
008795	C5	1371	PUSH	B	
008796	E5	1372	PUSH	H	
008797	216A88	1373	LXI	H,SEMAPHORE	
00879A	3A5B88	1374	LDA	FMHICB	
00879D	0600	1375	MVI	B,0	
00879F	4F	1376	MOV	C,A	; (BC):=(FMHICB)
0087A0	09	1377	DAD	B	; (HL):=SEMAPHORE+(FMHICB)
0087A1	3E46	1378	MVI	A,'F'	;MARK IT FULL
0087A3	77	1379	MOV	H,A	; (SEMAPHORE+(FMHICB)):= 'F'
0087A4	E1	1380	POP	H	
0087A5	C1	1381	POP	B	
0087A6	F1	1382	POP	PSW	
0087A7	C9	1383	RET		

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LL      1384  SETEMPTY:
LL      1385                                     ;MARK BUFFER EMPTY
LL87A8  F5    1386      PUSH    PSW
LL87A9  C5    1387      PUSH    B
LL87AA  E5    1388      PUSH    H
LL87AB  216A88 1389      LXI     H,SEMAPHORE
LL87AE  3A6888 1390      LDA     EWHICB
LL87B1  0600   1391      MVI     B,0
LL87B3  4F     1392      MOV     C,A      ;(BC):=(EWHICB)
LL87B4  09     1393      DAD     B      ;(HL):=SEMAPHORE+(EWHICB)
LL87B5  3E45   1394      MVI     A,'E'  ;MARK IT EMPTY
LL87B7  77     1395      MOV     M,A    ;(SEMAPHORE+(EWHICB)):'E'
LL87B8  E1     1396      POP     H
LL87B9  C1     1397      POP     B
LL87BA  F1     1398      POP     PSW
LL87BB  C9     1399      RET
LL      1400  INITRE:
LL87BC  CD7086 1401      CALL    SETCDIG ;ZERO DIGIT COUNTER, CNTDIG
LL87BF  CD2783 1402      CALL    CNTR0
LL87C2  CD1683 1403      CALL    CNTR1
LL87C5  3E0A   1404      MVI     A,10
LL87C7  326188 1405      STA     FLAG
LL87CA  3E80   1406      MVI     A,80H    ;FORMAT 8255 AS MODE 0,
LL87CC  D3EB   1407      OUT     OEBH    ; ALL THREE PORTS OUTPUT ON J-2 8004
LL87CE  110090 1408      LXI     D,BUFF0  ; SAVEDE POINTER =
LL87D1  ED535788 1409      SDED    SAVEDE ; SET TO BASE ADDRESS OF ALL TEN BUFFERS
LL87D5  3E00   1410      MVI     A,00H    ; POINTER THAT TELLS WHICH BUFFER
LL87D7  325B88 1411      STA     FWHICB ; IS BEING FILLED = 0
LL87DA  210008 1412      LXI     H,2048 ;COUNTER TO TELL HOW MUCH
LL87DD  225988 1413      SHLD    REMAIN ; OF A BUFFER IS UNFILLED.
LL87E0  110090 1414      LXI     D,BUFF0 ; POINTER TO BASE ADDRESS OF CURRENT
LL87E3  210000 1415      LXI     H,0    ;ZERO OUT
LL87E6  225E88 1416      SHLD    CNT    ; INTERRUPT COUNTER
LL87E9  ED537688 1417      SDED    CURRBUF ; BUFFER BEING FILLED
LL      1418      ; MVI     A,0
LL      1419      ; STA     FILLONE ;FILLONE=0, MEANS ALL BUFFERS ARE EMPTY
LL      1420      ; OF DATA.
LL87ED  3E80   1421      MVI     A,080H
LL87EF  D3C7   1422      OUT     LITECTRL ;FORMAT LIGHTS
LL87F1  3E9B   1423      MVI     A,09BH
LL87F3  D3E7   1424      OUT     J18004 ;FORMAT PUSHBUTTONS.
LL87F5  3EFF   1425      MVI     A,0FFH  ;TURN OFF LIGHTS
LL87F7  D3C5   1426      OUT     LITEPORT
LL87F9  325288 1427      STA     LIGHTS ; SAVE LIGHT STATUS
LL87FC  CD4586 1428      CALL    TOFFS ;STATE=0
LL87FF  CD1C86 1429      CALL    CPTIM ;PTIM=0
LL8802  CD6786 1430      CALL    CTIM  ;CLEAR SECOND COUNTER
LL8805  3E00   1431      MVI     A,0
LL8807  325688 1432      STA     BINARY ;BINARY=0, PBO AND LITE FIRST
LL880A  C9     1433      RET
LL      1434  ;*****
LL      1435      ; CHARACTER OUTPUT ROUTINE
LL      1436      ; CO OUTPUTS ONE CHARACTER FROM ACC TO TERMINAL
LL      1437      ; VIA THE USART. ALL REGISTERS AND FLAGS ARE
LL      1438      ; PRESERVED. THE CHARACTER IT OUTPUTS IS IN THE ACC.
LL      1439      ;*****
LL880B  F5     1440  CO:  PUSH    PSW
LL880C  C5     1441      PUSH    B
LL880D  4F     1442      MOV     C,A    ;SAVE A REG
LL880E  00     1443  COO: NOP      ;DELAY
LL880F  C0     1444      NOP
LL8810  1B0B   1445      IN      90251 ;GET USART STATUS
LL8812  E801   1446      ANI     TDRDY ;CHECK TRANSMIT READY FLAG
LL8814  C000   1447      JZ     CDR   ;IF EMPTY
LL8817  00     1448      NOP
LL      1449

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228819	00	1450	NOP		
22881A	00	1451	NOP		
22881B	79	1452	MOV	A,C	;READY TO TRANSMIT , RESTORE CHAR TO A REG
22881C	D3CC	1453	OUT	D8251	;SEND IT
22881E	C1	1454	POP	B	
22881F	F1	1455	POP	PSW	
228820	C9	1456	RET		
22		1457	INITUSART:		
228821	CD2B88	1458	CALL	RUSART	;MASTER RESET SEQUENCE
228824	CD3C88	1459	CALL	MUSART	;SET MODE IN USART
228827	CD4388	1460	CALL	CUSART	;SET COMMAND IN USART
22882A	C9	1461	RET		
22882B	3E80	1462	RUSART: MVI	A,80H	;RESET 8251
22882D	D3CD	1463	OUT	C8251	;
22882F	E3	1464	XTHL		
228830	E3	1465	XTHL		
228831	D3CD	1466	OUT	C8251	
228833	E3	1467	XTHL		
228834	E3	1468	XTHL		
228835	3E40	1469	MVI	A,40H	;
228837	D3CD	1470	OUT	C8251	;
228839	E3	1471	XTHL		
22883A	E3	1472	XTHL		
22883B	C9	1473	RET		
22883C	3E4E	1474	MUSART: MVI	A,USMODE	
22883E	D3CD	1475	OUT	C8251	
228840	E3	1476	XTHL		
228841	E3	1477	XTHL		
228842	C9	1478	RET		
228843	3E37	1479	CUSART: MVI	A,USCMD	;REST ERROR FLAGS
22		1480			; ENABLE TRANSMIT
22		1481			; ENABLE RECIEVE
22		1482			; READY DATA SET
22		1483			;
22		1484			;
228845	D3CD	1485	OUT C8251		;GIVE COMMAND
228847	E3	1486	XTHL		
228848	E3	1487	XTHL		
228849	C9	1488	RET		
22884A	C9	1489	RET		
22		1490			;
22004C		1491	BYTPERSEC EQU	2*38	; HOW MANY BYTES PER SEC OF DATA
22012C		1492	THSEBY: EQU	300	;NUMBER OF TIMER CLICKS NEEDED FOR 30 DELAY
22		1493			;300 FOR .1 SEC TIMER CLICKS
22		1494			;150 FOR .2 SEC TIMER CLICKS
220010		1495	TLOW EQU	010H	;
220027		1496	THIGH EQU	027H	;2710H=100000
22		1497	;TLOW EQU	020H	;
22		1498	;THIGH EQU	04EH	;4E20H=200000
22004E		1499	USMODE: EQU	04EH	;
220037		1500	USCMD: EQU	037H	;
22884B	00	1501	INPUTS: DB	0	
22884C	00	1502	TWODIG: DB	0	
22884D	00	1503	ONTDIG: DB	0	
2200CD		1504	S8251 EQU	OC0H	
2200CD		1505	C8251 EQU	S8251	
2200CC		1506	D8251 EQU	OCCH	
220002		1507	RORDY EQU	02H	
220001		1508	TXRDY EQU	01H	
22884E	0000	1509	ST: DW	0	
228850	0000	1510	PTIN: DW	0	
228852	0000	1511	LIGHTS: DW	0	
228854	0000	1512	MODES: DW	0	
228856	00	1513	BINRY: DB	0	
228857	0090	1514	SAVEDE: DW	BUFF0	
228859	0008	1515	REMAIN: DW	2048	

22885B	00	1516	FMICB: DB	0	;FILL WHICH BUFFER
22885C	0000	1517	TIN: DW	0	
22885E	0000	1518	CNT: DW	0	
228860	00	1519	FILLONE: DB	0	
228861	00	1520	FLAG: DB	0	
228862	0000	1521	SAVE: DW	0	
228864	0000	1522	SAV: DW	0	
228866	0000	1523	ERENAIN: DW	0	
228868	00	1524	EMICB: DB	0	;EMPTY WHICH BUFFER
228869	00	1525	TSU: DB	0	
22886A	45454545	1526	SEMAPHORE: DB	'EEEEEEEE'	;TEN BUFFER SEMAPHORES ALL 'E'
22	45454545				
228874	0000	1527	EDURBUF: DW	0	
228876	0090	1528	CURRBUF: DW	0	BUFF0
228878	0000	1529	TEMPDE: DW	0	
22		1530	AVG:		
22887A	F5	1531		PUSH	PSW
22887B	E5	1532		PUSH	H
22887C	C5	1533		PUSH	B
22887D	D5	1534		PUSH	D
22887E	DDE5	1535		PUSHX	
228880	FDE5	1536		PUSHY	
228882	3A5E88	1537	LDA	CNT	;
228885	FE00	1538	CPI	0	
228887	C29688	1539	JNZ	AVG1	
22		1540	; MWI	A,'1'	
22		1541	; CALL	CO	
22888A	CDE388	1542	CALL	PART1	
22888D	FDE1	1543	POPY		
22888F	DDE1	1544	POPX		
228891	D1	1545	POP	D	
228892	C1	1546	POP	B	
228893	E1	1547	POP	H	
228894	F1	1548	POP	PSW	
228895	C9	1549	RET		
228896	FE09	1550	AVG1: CPI	9	
228898	C2A788	1551	JNZ	AVG2	
22889B	CDEA88	1552	CALL	PART3	
22889E	FDE1	1553	POPY		
2288A0	DDE1	1554	POPX		
2288A2	D1	1555	POP	D	
2288A3	C1	1556	POP	B	
2288A4	E1	1557	POP	H	
2288A5	F1	1558	POP	PSW	
2288A6	C9	1559	RET		
2288A7	CDECB8	1560	AVG2: CALL	PART2	
2288AA	FDE1	1561	POPY		
2288AC	DDE1	1562	POPX		
2288AE	D1	1563	POP	D	
2288AF	C1	1564	POP	B	
2288B0	E1	1565	POP	H	
2288B1	F1	1566	POP	PSW	
2288B2	C9	1567	RET		
22		1568	PART1		
2288B3	21A68A	1569	LXI	H,A32	
2288B6	013000	1570	LXI	B,48	
2288B9	CDF489	1571	CALL	CLEAR	
22		1572	PART2:		
22		1573	; MWI	A,'2'	
22		1574	; CALL	CO	
22		1575	; CALL	CRLF	
2288BC	AF	1576	XRA	A	
2288BD	32888A	1577	STA	ITER	
22		1578	TP1:		
22		1579	; CALL	PORTAOFF	
2288C0	DB215788	1580	LXIX	PNTA16	

2288C4	FD21888A	1581	LXIY	ITER	
2288C8	CDBF89	1582	CALL	LD2BCDE	; (BCDE) := A16(ITER)
22		1583	CALL	WBCDE	; DUMP BCDE REGISTERS
22		1584			
2288CB	CD4D89	1585	CALL	DSTACK	; PUT (BCDE) ONTO 32 BIT STACK
2288CE	DD21A68A	1586	LXIX	A32	
2288D2	FD21888A	1587	LXIY	ITER	
2288D6	CD8B89	1588	CALL	LD4BCDE	; (BCDE) := A32(ITER)
22		1589	CALL	WBCDE	; DUMP BCDE REGISTERS
2288D9	CD4D89	1590	CALL	DSTACK	
2288DC	CD7189	1591	CALL	FIXADD	
2288DF	CD5F89	1592	CALL	UDSTACK	; (BCDE) := RESULT OF 32BIT INTEGER ADD
22		1593	CALL	WBCDE	; DUMP BCDE REGISTERS
2288E2	DD21A68A	1594	LXIX	A32	
2288E6	FD21888A	1595	LXIY	ITER	
2288EA	CDA389	1596	CALL	ST4BCDE	; (A32(ITER)) := (BCDE)
22		1597	LDA	ITER	
22		1598	CALL	HIMP	
22		1599	CALL	CRLF	
2288ED	3A888A	1600	LDA	ITER	; CHECK ITERATION COUNT
2288F0	3C	1601	INR	A	
2288F1	32888A	1602	STA	ITER	
2288F4	FEOC	1603	CPI	12	
2288F6	C2C088	1604	JNZ	TP1	
22		1605	CALL	PORTAON	
2288F9	C9	1606	RET		
22		1607	PART3:		
2288FA	AF	1608	XRA	A	
2288FB	32888A	1609	STA	ITER	
22		1610	TP2:		
2288FE	DD215788	1611	LXIX	PNTA16	
228902	FD21888A	1612	LXIY	ITER	
228906	CDBF89	1613	CALL	LD2BCDE	; (BCDE) := (A16(ITER))
228909	CD4D89	1614	CALL	DSTACK	; (BCDE) ONTO 32 BIT STACK OF T9511
22890C	DD21A68A	1615	LXIX	A32	
228910	FD21888A	1616	LXIY	ITER	
228914	CD8B89	1617	CALL	LD4BCDE	; (BCDE) := (A32(ITER))
228917	CD4D89	1618	CALL	DSTACK	; (BCDE) ONTO 32 BIT STACK OF T9511
22891A	CD7189	1619	CALL	FIXADD	; ADD 32 BIT INTEGERS TOGETHER
22891D	110A00	1620	LXI	D,10	
228920	010000	1621	LXI	B,0	
228923	CD4D89	1622	CALL	DSTACK	
228926	CD7E89	1623	CALL	FIXDIV	; DIVIDE BY TEN
228929	CD5F89	1624	CALL	UDSTACK	; (BCDE) HAS AVERAGE OF TEN VALUES
22892C	DD215788	1625	LXIX	PNTA16	
228930	FD21888A	1626	LXIY	ITER	
228934	CD8989	1627	CALL	ST2BCDE	; (BCDE) := (A16(ITER))
228937	3A888A	1628	LDA	ITER	; CHECK ITERATION COUNT
22893A	3C	1629	INR	A	
22893B	32888A	1630	STA	ITER	
22893E	FEOC	1631	CPI	12	
228940	C2FE88	1632	JNZ	TP2	
228943	C9	1633	RET		
22		1634	T95BUSY:		
228944	F5	1635		PUSH	PSW
228945	D805	1636	T95BUSY1:	IN	T9511CTRLPORT
228947	B7	1637		ORA	A
228948	FA4589	1638		JM	T95BUSY1
22894B	F1	1639		POP	PSW
22894C	C9	1640		RET	
22		1641	DSTACK:		
22894D	F5	1642		PUSH	PSW
22894E	CD4489	1643		CALL	T95BUSY
228951	7B	1644		MOV	A,E
228952	D3D4	1645		OUT	T9511DATAPORT
228954	7A	1646		MOV	A,D

; INPUT THE STATUS WORD  
; SET UP FLAGS  
; BIT 7 SET MEANS T9511 IS BUSY  
; ;  
; WAIT UNTIL T9511 NOT BUSY  
; LSB TO STACK  
; T9511DATAPORT  
; NEXT BYTE TO STACK

228955	D3D4	1647	OUT	T9511DATAPORT	
228957	79	1648	MOV	A,C	;NEXT SIG BYTE TO STACK OF T9511
228958	D3D4	1649	OUT	T9511DATAPORT	
22895A	78	1650	MOV	A,B	;MSB BYTE TO STACK OF T9511
22895B	D3D4	1651	OUT	T9511DATAPORT	
22895D	F1	1652	POP	PSW	
22895E	C9	1653	RET		
22		1654			
22895F	F5	1655	PUSH	PSW	
228960	CD4489	1656	CALL	T95BUSY	;WAIT UNTIL T9511 NOT BUSY
228963	D8D4	1657	IN	T9511DATAPORT	;MSB FROM STACK OF T9511
228965	47	1658	MOV	B,A	
228966	D8D4	1659	IN	T9511DATAPORT	;NEXT BYTE FROM STACK OF T9511
228968	4F	1660	MOV	C,A	
228969	D8D4	1661	IN	T9511DATAPORT	;NEXT BYTE FROM STACK OF T9511
22896B	57	1662	MOV	D,A	
22896C	D8D4	1663	IN	T9511DATAPORT	
22896E	5F	1664	MOV	E,A	
22896F	F1	1665	POP	PSW	
228970	C9	1666	RET		
22		1667			
228971	F5	1668	PUSH	PSW	
228972	CD4489	1669	CALL	T95BUSY	
228975	3E2C	1670	MVI	A,02CH	;32 BIT FIX POINT ADD
228977	D3D5	1671	OUT	OD5H	;
228979	CDFC89	1672	CALL	STAT	
22897C	F1	1673	POP	PSW	
22897D	C9	1674	RET		
22		1675			
22897E	F5	1676	PUSH	PSW	
22897F	CD4489	1677	CALL	T95BUSY	
228982	3E2F	1678	MVI	A,02FH	;32 BIT FIX POINT DIVIDE
228984	D3D5	1679	OUT	OD5H	;
228986	CDFC89	1680	CALL	STAT	
228989	F1	1681	POP	PSW	
22898A	C9	1682	RET		
22		1683			
22		1684			
22		1685			;THIS SUBROUTINE LOADS A 32 BIT ARRAY ELEMENT INTO
22		1686			;THE REGISTERS BCDE. REGISTER B HAS MOST SIGNIFICANT BYTE,
22		1687			;REGISTER E HAS THE LEAST SIGNIFICANT BYTE.
22		1688			;
22		1689			;THIS SUBROUTINE HAS A CALLING SEQUENCE
22		1690	;	LXIX	A32
22		1691	;	LXIY	ITER
22		1692	;	CALL	LD4BCDE
22898B	F5	1693	PUSH	PSW	
22898C	ES	1694	PUSH	H	
22		1695			
22898D	FD6E00	1696	MOVRY	L,0	
228990	FD6601	1697	MOVRY	H,1	;(HL):=CONTENTS(ITER)
22		1698			
228993	29	1699	DAD	H	
228994	29	1700	DAD	H	;(HL):=4*CONTENTS(ITER)
22		1701			
228995	DDE5	1702	PUSHX		
228997	C1	1703	POP	B	;(BC):=(IX)
22		1704			
228998	09	1705	DAD	B	;(HL):=A32(ITER)
22		1706			
22		1707			
228999	5E	1708	MOV	E,M	
22899A	23	1709	INX	H	
22899B	56	1710	MOV	D,M	
22899C	23	1711	INX	H	
22899D	4E	1712	MOV	C,M	

22899E	23	1713	INX	H	
22899F	46	1714	MOV	B,M	;(BCDE):=(4 BYTES OF A32(I))
22		1715			
2289A0	E1	1716	POP	H	
2289A1	F1	1717	POP	PSW	
2289A2	C9	1718	RET		
22		1719	ST4BCDE:		
22		1720	;		
22		1721	;THIS SUBROUTINE STORES THE REGISTERS BCDE INTO A 32 BIT ARRAY ELEMENT		
22		1722	; REGISTER B HAS MOST SIGNIFICANT BYTE,		
22		1723	;REGISTER E HAS THE LEAST SIGNIFICANT BYTE.		
22		1724	;		
22		1725	;THIS SUBROUTINE HAS A CALLING SEQUENCE		
22		1726	;	LXIX	A32
22		1727	;	LXIY	ITER
22		1728	;	CALL	ST4BCDE
2289A3	F5	1729		PUSH	PSW
2289A4	E5	1730		PUSH	H
2289A5	C5	1731		PUSH	B
2289A6	D5	1732		PUSH	D
22		1733			
2289A7	FD6E00	1734	MOVW	L,0	
2289A8	FD6601	1735	MOVW	H,1	;(HL):=CONTENTS(ITER)
22		1736			
2289AD	29	1737	DAD	H	
2289AE	29	1738	DAD	H	;(HL):=4*CONTENTS(ITER)
22		1739			
2289AF	D0E5	1740	PUSHX		
2289B1	C1	1741	POP	B	;(BC):=(IX)
22		1742			
2289B2	09	1743	DAD	B	;(HL):=A32(ITER)
22		1744			
2289B3	D1	1745	POP	D	
2289B4	73	1746	MOV	M,E	
2289B5	23	1747	INX	H	
2289B6	72	1748	MOV	M,D	
2289B7	23	1749	INX	H	
22		1750			
2289B8	C1	1751	POP	B	
2289B9	71	1752	MOV	M,C	
2289BA	23	1753	INX	H	
2289BB	70	1754	MOV	M,B	
22		1755			
2289BC	E1	1756	POP	H	
2289BD	F1	1757	POP	PSW	
2289BE	C9	1758	RET		
22		1759			
22		1760	LD2BCDE:		
22		1761	;		
22		1762	;THIS SUBROUTINE LOADS A 16 BIT ARRAY ELEMENT INTO THE REGISTERS BCDE.		
22		1763	;REGISTER BC HAS 16 BIT ZERO		
22		1764	;REGISTER DE HAS THE 16 BIT INTEGER.		
22		1765	;		
22		1766	;THIS SUBROUTINE HAS A CALLING SEQUENCE		
22		1767	;	LXIX	PNTA16
22		1768	;	LXIY	ITER
22		1769	;	CALL	LD2BCDE
2289BF	F5	1770		PUSH	PSW
2289C0	E5	1771		PUSH	H
22		1772			
2289C1	DD6E00	1773	MOVW	L,0	
2289C4	DD6601	1774	MOVW	H,1	;(HL):=ADDR(A16)
22		1775			
2289C7	EB	1776	XCHG		;(DE):=ADDR(A16)
22		1777			
2289C8	FD6E00	1778	MOVW	L,0	



LL89CB	FD6601	1779	MOVRY	H,1	; (HL):=CONTENTS(ITER)
LL		1780			
LL89CE	29	1781	DAD	H	; (HL):=2*CONTENTS(ITER)
LL		1782			
LL89CF	19	1783	DAD	D	; (HL):=ADDR(A16)+2*CONTENTS(ITER)
LL		1784			
LL		1785			
LL89D0	5E	1786	MOV	E,M	
LL89D1	23	1787	INX	H	
LL89D2	56	1788	MOV	D,M	; (DE) LOADED WITH 16 BIT INTEGER
LL		1789			; WHOSE ADDRESS IS IN (HL)
LL		1790			
LL89D3	010000	1791	LXI	B,0	; (BC) SET TO 0
LL		1792			
LL89D6	E1	1793	POP	H	
LL89D7	F1	1794	POP	PSW	
LL89D8	C9	1795	RET		
LL		1796			
LL		1797			
LL		1798			; THIS SUBROUTINE LOADS THE REGISTERS BCDE INTO A 16 BIT ARRAY ELEMENT.
LL		1799			; REGISTER BC HAS 16 BIT ZERO
LL		1800			; REGISTER DE HAS THE 16 BIT INTEGER.
LL		1801			
LL		1802			; THIS SUBROUTINE HAS A CALLING SEQUENCE
LL		1803			
LL		1804			
LL		1805			
LL89D9	F5	1806			
LL89DA	ES	1807			
LL89DB	CS	1808			
LL89DC	D5	1809			
LL		1810			
LL		1811			
LL89DD	DD6E00	1812	MOVX	L,0	
LL89DE	DD6601	1813	MOVX	H,1	; (HL):=ADDR(A16)
LL		1814			
LL89E3	EB	1815	XCHG		; (DE):=ADDR(A16)
LL		1816			
LL89E4	FD6E00	1817	MOVRY	L,0	
LL89E7	FD6601	1818	MOVRY	H,1	; (HL):=CONTENTS(ITER)
LL		1819			
LL89EA	29	1820	DAD	H	; (HL):=2*CONTENTS(ITER)
LL		1821			
LL89EB	19	1822	DAD	D	; (HL):=2*CONTENTS(ITER)+ADDR(A16)
LL		1823			
LL89EC	D1	1824	POP	D	; RESTORE DE PAIR AS IT WAS ON ENTERING
LL		1825			
LL		1826			
LL89ED	73	1827	MOV	M,E	
LL89EE	23	1828	INX	H	
LL89EF	72	1829	MOV	M,D	; (DE) STORED AT ADDRESS CONTAINED IN (HL)
LL		1830			
LL89F0	C1	1831	POP	B	; RESTORE BC
LL89F1	E1	1832	POP	H	
LL89F2	F1	1833	POP	PSW	
LL89F3	C9	1834	RET		
LL		1835			
LL		1836			
LL		1837			; THIS SUBROUTINE HAS A CALLING SEQUENCE
LL		1838			
LL		1839			
LL		1840			
LL		1841			
LL		1842			; THIS SUBROUTINE CLEARS AN ARRAY OF 32 BIT ELEMENTS.
LL		1843			; HL IS THE BASE ADDRESS
LL		1844			; BC IS HOW MANY BYTES TO ZERO

;;	1845	;			
;;	1846				
;;89F4	54	1847	MOV	D,H	
;;89F5	5D	1848	MOV	E,L	
;;89F6	13	1849	INX	D	; (DE) := (HL) + 1
;;		1850			
;;89F7	3600	1851	MVI	M,00H	; ZERO INITIAL LOCATION
;;89F9	EDB0	1852	LDIR		; NOW ZERO ALL 48 BYTES
;;		1853			
;;89FB	C9	1854	RET		
;;		1855	STAT:		
;;89FC	F5	1856	PUSH	PSW	
;;89FD	E5	1857	PUSH	H	
;;89FE	DBD5	1858	STAT2:	IN	OD5H
;;8A00	B7	1859	ORA	A	
;;8A01	FAFE89	1860	JR	STAT2	
;;8A04	E61E	1861	ANI	01EH	; ISOLATE BIT 4,3,2,1
;;8A06	CA0E8A	1862	JZ	STAT1	
;;8A09	3E54	1863	MVI	A,'T'	
;;8A0B	CD0B88	1864	CALL	CD	
;;		1865	STAT1:		
;;8A0E	E1	1866	POP	H	
;;8A0F	F1	1867	POP	PSW	
;;8A10	C9	1868	RET		
;;		1869	ALIGN:		
;;8A11	F5	1870	PUSH	PSW	
;;8A12	3E01	1871	MVI	A,01H	
;;8A14	D3D4	1872	OUT	OD4H	
;;8A16	3E00	1873	MVI	A,00H	
;;8A18	D3D4	1874	OUT	OD4H	
;;8A1A	3E1D	1875	MVI	A,01DH	
;;8A1C	B3D5	1876	OUT	OD5H	
;;8A1E	CD4489	1877	CALL	T95BUSY	
;;		1878	HH:		
;;8A21	DBD4	1879	IN	OD4H	
;;8A23	FE01	1880	CPI	01H	
;;8A25	CA218A	1881	JZ	HH	
;;8A28	F1	1882	POP	PSW	
;;8A29	C9	1883	RET		
;;		1884	OK:		
;;		1885	;	WRITE MESSAGE OK	
;;8A2A	D5	1886	PUSH	D	
;;8A2B	11F68A	1887	LXI	D,OKAY	
;;8A2E	CD448A	1888	CALL	MSG	
;;8A31	CD2A87	1889	CALL	CRLF	
;;8A34	D1	1890	POP	D	
;;8A35	C9	1891	RET		
;;		1892	DONE:		
;;		1893	;	WRITE MESSAGE DONE	
;;8A36	D5	1894	PUSH	D	
;;8A37	11FB8A	1895	LXI	D,DONEE	
;;8A3A	CD448A	1896	CALL	MSG	
;;8A3D	D1	1897	POP	D	
;;8A3E	C9	1898	RET		
;;8A3F	3E4F	1899	MVI	A,'O'	
;;8A41	CD0B88	1900	CALL	CD	
;;8A44	3E4B	1901	MVI	A,'K'	
;;8A46	CD0B88	1902	CALL	CD	
;;8A49	C9	1903	RET		
;;		1904	*****		
;;		1905	;		
;;		1906	;		
;;		1907	;	PRINT AMESSAGE ON CONSOLE.	
;;		1908	;	D-REGISTER POINTS TO BYTE CONTAINING LENGTH	
;;		1909	;	OF MESSAGE. MESSAGE IS IN THE BYTES FOLLOWING	
;;		1910	;	LENGTH BYTE.	

22		1911	;		
22		1912	;		
22		1913	;		
22		1914	;		CALLING SEQUENCE
22		1915	;	LXI	D,DONE
22		1916	;	CALL	MSG
22		1917	;	DONE:	DB LGTH,'DONE'
22		1918	;	LGTH	EDU \$-(DONE+1)
22		1919	;		
22		1920	;		
22		1921	;		
22		1922	;		
22		1923	MSG:	PUSH	PSW ;SAVE STATUS AND A REG
22	228A4A F5	1924		PUSH H	
22	228A4B E5	1925		PUSH D	
22	228A4C D5	1926		LDAX	D ;GET LENGTH OF MESSAGE
22	228A4D 1A	1927		MOV	H,A ;SAVE IT IN H
22	228A4E 67	1928		INX	D ;POINT TO FIRST BYTE OF MESSAGE
22	228A4F 13	1929			; TO OUTPUT
22	228A50 1A	1930	MSG:	LDAX	D ;BYTE OF MESSAGE INTO A
22	228A51 CD0B88	1931		CALL	CD ; OUTPUT CHAR
22	228A54 13	1932		INX	D ;POINT TO NEXT BYTE
22	228A55 25	1933		DCR	H ; NUMBER OF CHARS TO BE OUTPUT
22		1934			; DIMINISHED BY ONE
22	228A56 C2508A	1935		JNZ	MSG0 ;BRANCH IF THERE ARE
22	228A59 D1	1936		POP	D
22	228A5A E1	1937		POP	H
22	228A5B F1	1938		POP	PSW
22	228A5C C9	1939		RET	
22		1940	MSG0:		
22	228A5D F5	1941		PUSH	PSW
22	228A5E 78	1942		MOV	A,B
22	228A5F CD0987	1943		CALL	HDMP
22	228A62 79	1944		MOV	A,C
22	228A63 CD0987	1945		CALL	HDMP
22	228A66 7A	1946		MOV	A,D
22	228A67 CD0987	1947		CALL	HDMP
22	228A6A 7B	1948		MOV	A,E
22	228A6B CD0987	1949		CALL	HDMP
22	228A6E CD2A87	1950		CALL	CRLF
22	228A71 F1	1951		POP	PSW
22	228A72 C9	1952		RET	
22		1953	INITPORTA:		
22	228A73 F5	1954		PUSH	PSW
22	228A74 3E80	1955		MVI	A,080H
22	228A76 D3EB	1956		OUT	0E8H
22	228A78 F1	1957		POP	PSW
22	228A79 C9	1958		RET	
22		1959	PORTAON:		
22	228A7A F5	1960		PUSH	PSW
22	228A7B 3E00	1961		MVI	A,00H
22	228A7D D3EB	1962		OUT	0E8H
22	228A7F F1	1963		POP	PSW
22	228A80 C9	1964		RET	
22		1965	PORTAOFF:		
22	228A81 F5	1966		PUSH	PSW
22	228A82 3EFF	1967		MVI	A,0FFH
22	228A84 D3EB	1968		OUT	0E8H
22	228A86 F1	1969		POP	PSW
22	228A87 C9	1970		RET	
22	228A88 0000	1971	ITER:	DW	0
22	228A8A 0000	1972	I:	DW	0
22	228A8C A68A	1973	PNTA32:	DW	A32
22	228A87	1974	PNTA16:	EDU	SAVEDE
22	228A8E 0100	1975	A16:	DW	01H,02H,03H,04H,05H,06H,07H,08H,09H,0AH,0BH,0CH
22	228A90 0200				

LL8A92	0300				
LL8A94	0400				
LL8A96	0500				
LL8A98	0600				
LL8A9A	0700				
LL8A9C	0800				
LL8A9E	0900				
LL8AA0	0A00				
LL8AA2	0B00				
LL8AA4	0C00				
LL8AA6		1976	A32:	DS	4*20
LL0005		1977	T9511CTRLPORT	EDU	005H
LL0004		1978	T9511DATAPORT	EDU	004H
LL8AF6	04	1979	OKAY:	DB	4,'OK',CR,LF
LL8AF7	4F4B				
LL8AF9	0D				
LL8AFA	0A				
LL8AFB	06	1980	DONEE:	DB	6,'DONE',CR,LF
LL8AFC	444F4E45				
LL8B00	0D				
LL8B01	0A				
LL9000		1981		ORG	9000H
LL9000		1982	BUFF0:	DS	2048*10
LL		1983		END	
LL	0 ERRORS				
LL					
LL	T=0.53/3.15				
LL	09:23:38				
LL					

# GENERIC TRAJECTORY (B.2)

FILE: GTRAJ1    FORTRAN    A1    PRINCETON UNIVERSITY TIME-SHARING SYSTEM

	COMMON/COM/C(2000)	GT
	COMMON/DEGREE/DUMMY2(5)	GT
	COMMON/RK/DUMMY4(112)	GT
	COMMON/RUNOUT/DUMMY8(1)	GT
C		GT
235	CONTINUE	GT
	CALL MYINIT	GT
	CALL MYRUN	GT
	GOTO 235	GT
	END	GT
	SUBROUTINE MYINIT	GT
	CALL INPT	GT
	CALL INIT	GT
	CALL DYNAMI	GT
	RETURN	GT
	END	GT
	SUBROUTINE MYRUN	GT
	COMMON/COM/C(2000)	GT
	COMMON/RUNOUT/DAN	GT
	COMMON/SINAV/XST(7),YST(7),ZST(7),DIREQ(7),ISTDME,ISTVCR	GT
	1,R1(40),NOYES(40),SIGMA(40)	GT
	COMMON/DOUBLE/DSEED,DDS	GT
	DOUBLE PRECISION DSEED,DDS	GT
	EQUIVALENCE (C(203),TIME),(C(207),NSTEP)	GT
	EQUIVALENCE (C(211),TIMPR),(C(212),TIMPLT),(C(213),TIMTTY)	GT
	EQUIVALENCE (C(241),J1),(C(244),TIMSOF)	GT
C		GT
C	*****TEMPORARILY:	GT
	DO 259 I=1,40	GT
	259 R1(I)=0.	GT
C		GT
	DAN=0.	GT
C		GT
	CALL ERROR	GT
C		GT
242	CONTINUE	GT
	IF (TIME.LT.TIMSOF) GOTO 82	GT
	DAN=2.	GT
	CALL OUTPT	GT
	CALL FINT	GT
	GOTO 100	GT
C		GT
82	CONTINUE	GT
C		GT
C	***NOISE HAS TO BE DRAWN FROM RANDOM GEN FOR EACH CHANN EVERY DT AND	GT
C	***BE AVAILABLE FOR SUBROUTINE OUTPT AT WHATEVER REQUIRED RECORDING	GT
C	***INSTANTS.	GT
C	*****CALL GGNPM(DSEED,30,R1)	GT
	DSEED=DSEED+DDS	GT
C		GT
	CALL LOGIC	GT
C	***R.K. LOOP	GT
C		GT
	DO 246 J=1,4	GT
	J1=J	GT

	CALL ROTAT	GTR
	CALL DYNAM	GTR
C	IF (TIME.LE.0.) CALL OUTPT	GTR
	CALL RKG	GTR
246	CONTINUE	GTR
C		GTR
C		GTR
	NSIEP=NSTEP+1	GTR
	IF (TIME.LE.TIMPR.AND.TIME.LE.TIMPLT.AND.TIME.LE.TIMTTY) GOTO 242	GTR
	CALL OUTPT	GTR
	GOTO 242	GTR
100	CONTINUE	GTR
	RETURN	GTR
	END	GTR
	BLOCK        DATA	GTR
	COMMON/DEGREE/TETO,QO(50),PSIOJ,PHIOJ,WP0J(50),WR0J(50)	GTR
	COMMON/PROG/TACCX(50),TACCY(50),TACCZ(50),TPROG(50),	GTR
	1WPC(50),WRC(50),WQC(50),NTIME,TSWTCH(15),ISWTCH	GTR
	COMMON/COM/C(2000)	GTR
	COMMON/ALBET/XBETA,ZBETA,XALPHA,YALPHA	GTR
	COMMON/STNAV/XST(7),YST(7),ZST(7),DIREQ(7),ISTDME,ISTVOR	GTR
	1,R1(40),NOYES(40),SIGMA(40)	GTR
	COMMON/DOUBLE/DSEED,DDS	GTR
	DOUBLE PRECISION DSEED,DDS	GTR
C		GTR
	EQUIVALENCE (C(202),NRATE)	GTR
	EQUIVALENCE (C(214),DTPR),(C(215),DTPLT),(C(216),DTTTY)	GTR
	EQUIVALENCE (C(220),IPR),(C(244),TIMSCF)	GTR
	EQUIVALENCE (C(341),HO),(C(347),XEO),(C(348),YEO)	GTR
	EQUIVALENCE (C(277),USPEDO),(C(278),VSPEDO),(C(279),WSPEDO)	GTR
C		GTR
	DATA HO/116./,TIMSCF/60./,TETO/10./,PSIOJ/0./,PHIOJ/12.7/,	GTR
	1NTIME/15/,USPEDO/125./,VSPEDO/0./,WSPEDO/12./	GTR
	2,TPROG/0.,60.,61.,100.,101.,160.,161.,43*600./,	GTR
	6QO/2*.6,2*0.,2*.6,44*0./,	GTR
	7WP0J/2*-.5,2*0.,2*.5,44*0./,	GTR
	9WR0J/2*2.86,2*0.,2*-2.86,44*0./,	GTR
	BTACCX/2*.179,2*.096,2*.179,2*-.206,42*.2/,	GTR
	CTACCY/40*0.,10*0./,	GTR
	DTACCZ/2*-1.003,2*-.994,2*-1.003,2*-.985,42*-1./	GTR
	DATA NRATE/20/,DTPR/400./,DTPLT/400./,DTTTY/1./,	GTR
	1IPR/1/	GTR
	2,XBETA/0./,ZBETA/0./,XALPHA/0./,YALPHA/0./	GTR
	3,XST/7*120000./	GTR
	4,YST/7*120000./	GTR
	5,ZST/7*0./	GTR
	6,DIREQ/7*32./	GTR
	7,ISTDME/1/,ISTVOR/1/	GTR
	DATA DSEED/1.D0/,DDS/1.D0/,NOYES/40*0/,SIGMA/40*0./	GTR
	DATA ISWTCH/1/,TSWTCH/15*600./	GTR
	1,XEO/0./,YEO/0./	GTR
	END	GTR
	SUBROUTINE INPT	GTR
	INTEGER FILE(6),GO	GTR

```

LOGICAL SOF
DIMENSION NAME(8), LNAME(4)

C
COMMON/COM/C(2000)
COMMON/DEGREE/TETO,QO(50),PSIOJ,PHIOJ,WPOJ(50),WROJ(50)
COMMON/PROG/TACCX(50),TACCY(50),TACCZ(50),TPROG(50),
1WPC(50),WRC(50),WQC(50),NTIME,TSWTCH(15),ISWTCH
COMMON/ALBET/XBETA,ZBETA,XALPHA,YALPHA
COMMON/STNAV/XST(7),YST(7),ZST(7),DIREQ(7),ISTDME,ISTVOR
1,R1(40),NOYES(40),SIGMA(40)
COMMON/DOUBLE/DSEED,DDS
DOUBLE PRECISION DSEED,DDS

C
EQUIVALENCE (C(202),NRATE)
EQUIVALENCE (C(214),DTPR),(C(215),DTPLT),(C(216),DTTTY)
EQUIVALENCE (C(220),IPR),(C(243),IF2),(C(244),TIMSOF)
EQUIVALENCE (C(341),HO),(C(347),XEO),(C(348),YEO)
EQUIVALENCE (C(277),USPEDO),(C(278),VSPEDO),(C(279),WSPEDO)

C
NAMelist/INP/FILE
NAMelist/INCN/HO,TETO,QO,TIMSOF,PSIOJ,PHIOJ,WPOJ,WROJ,
1TACCX,TACCY,TACCZ,NTIME,TPROG,USPEDO,VSPEDO,WSPEDO
2,XBETA,ZBETA,XALPHA,YALPHA
3,XST,YST,ZST,DIREQ,ISTDME,ISTVOR
4,TSWTCH,XEO,YEO
NAMelist/PARM/NRATE,DTTTY,DTPR,DTPLT,IPR,DSEED,DDS,NOYES,SIGMA

C
DATA NAME/4HINCN,4HPARM,4H      ,4H      ,4H      ,4H      ,4H      ,4H      /
235 CONTINUE
PRINT 502
502 FORMAT(1H,'TO CONTINUE ENTER F,TO STOP ENTER T')
READ 503,SCF
503 FORMAT(L1)
IF(SOF)STOP
PRINT 500
500 FORMAT(1H,'ENTER DESIRED FILES IN NAMelist INP',/)
READ(5,INP)
IF1=FILE(1)
IF2=FILE(2)
IF3=FILE(3)
IF4=FILE(4)
IF5=FILE(5)
IF6=FILE(6)
DO 220 I=1,2
LNAME(I)=NAME(I)
220 CONTINUE

C
IF(IF1.EQ.5)PRINT 501,LNAME
501 FORMAT(1H,'ENTER NAMELISTS ',A4,A4,'IN THIS ORDER',/)
IF(IF3.NE.0)READ(IF1,INCN)
IF(IF4.NE.0)READ(IF1,PARM)

C
PRINT 504
504 FORMAT(1H,'TO RUN ENTER 1,TO MODIFY INPUT DATA ENTER 0')
READ 505,GO

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505 FORMAT (I1)
      IF (GO.NE.1) GOTO 235
      RETURN
      END
      SUBROUTINE INIT
      DIMENSION IPL(100),IPD(100)
      COMMON/COM/C(2000)
      COMMON/DEGREE/TETO,QO(50),PSIOJ,PHIOJ,WPOJ(50),WROJ(50)
      COMMON/PROG/TACCX(50),TACCY(50),TACCZ(50),TPROG(50),WPC(50),
1WRC(50),WQC(50),NTIME,TSWCH(15),ISWCH
      COMMON/RK/ARK(4),BRK(4),CRK(4),QRK(100)

C      EQUIVALENCE (C(201),N)
      EQUIVALENCE (C(202),NRATE), (C(203),TIME), (C(204),TIMED)
      EQUIVALENCE (C(205),DT), (C(207),NSTEP)
      EQUIVALENCE (C(211),TIMPR), (C(212),TIMPLT), (C(213),TIMTTY)
      EQUIVALENCE (C(214),DTPR), (C(215),DTPLT), (C(216),DITTY)
      EQUIVALENCE (C(217),LINE), (C(218),NPRINT), (C(219),NPLOT)
      EQUIVALENCE (C(222),NSQ2)
      EQUIVALENCE (C(242),CRAD), (C(370),GRAV1), (C(319),THETO)
      EQUIVALENCE (C(318),PHIO), (C(320),PSIO)

C      GRAV1=32.17

C      ARK(1)=.5
      ARK(2)=1.-1./SQRT(2.)
      ARK(3)=1.+1./SQRT(2.)
      ARK(4)=1./6.
      BRK(1)=2.
      BRK(2)=1.
      BRK(3)=1.
      BRK(4)=2.
      CRK(1)=ARK(1)
      CRK(2)=ARK(2)
      CRK(3)=ARK(3)
      CRK(4)=ARK(1)
      DO 229 I=1,100
229  QRK(I)=0.

C      NSQ2=1

C      PI=4.*ATAN(1.)
      CRAD=180./PI
      THETO=TETO/CRAD
      PSIO=PSIOJ/CRAD
      PHIO=PHIOJ/CRAD
      DO 248 I=1,NTIME
      WPC(I)=WPOJ(I)/CRAD
      WQC(I)=QO(I)/CRAD
248  WRC(I)=WROJ(I)/CRAD

C      IPL(1)=203
      IPD(1)=204
      N=1
      C(1)=IPL(1)

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	C(101)=IPD(1)	GT
	TIME=0.	GT
	TIMED=1.	GT
	NSTEP=0	GT
	NRAT=NRATE	GT
	DT=1./FLOAT(NRAT)	GT
C		GT
	NPRINT=0	GT
	NPIOT=0	GT
	LINE=60	GT
	TIMPR=DTPR-.5*DT	GT
	TIMPLT=DTPLT-.5*DT	GT
	TIMTTY=DTTTY-.5*DT	GT
	IF(DTTTY.GT.50.)            TIMTTY=1000.	GT
C		GT
	RETURN	GT
	END	GT
	SUBROUTINE ERROR	GT
	PRINT 507	GT
507	FORMAT(1H ,'RUNNING NOW',/)	GT
	RETURN	GT
	END	GT
	SUBROUTINE DYNAMI	GT
	DIMENSION IPL(100),IPD(100)	GT
	COMMON/COM/C(2000)	GT
	EQUIVALENCE (C(201),N)	GT
	EQUIVALENCE (C(205),DT)	GT
	EQUIVALENCE (C(311),TET), (C(319),THETO), (C(312),PHI)	GT
	EQUIVALENCE (C(318),PHIO), (C(310),PSI), (C(320),PSIO)	GT
	EQUIVALENCE (C(334),XE), (C(335),YE), (C(336),ZE)	GT
	EQUIVALENCE (C(341),HO), (C(343),HM), (C(347),XE0), (C(348),YE0)	GT
	EQUIVALENCE (C(271),USPEED), (C(277),USPED0), (C(272),VSPEED)	GT
	EQUIVALENCE (C(278),VSPED0), (C(273),WSPEED), (C(279),WSPED0)	GT
C		GT
	N=N+1	GT
	IPL(N)=310	GT
	IPD(N)=314	GT
	N=N+1	GT
	IPL(N)=311	GT
	IPD(N)=315	GT
	N=N+1	GT
	IPL(N)=312	GT
	IPD(N)=316	GT
	N=N+1	GT
	IPL(N)=271	GT
	IPD(N)=274	GT
	N=N+1	GT
	IPL(N)=272	GT
	IPD(N)=275	GT
	N=N+1	GT
	IPL(N)=273	GT
	IPD(N)=276	GT
	N=N+1	GT
	IPL(N)=334	GT
	IPD(N)=337	GT

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      N=N+1
      IPL(N)=335
      IPD(N)=338
      N=N+1
      IPL(N)=336
      IPD(N)=339
C
      TET=THETO
      PSI=PSIO
      PHI=PHIO
      XE=XEO
      YE=YEO
      ZE=-HO
      HM=HO
C
      USPEED=USPELO
      VSPEED=VSPELO
      WSPPEED=WSPELO
C
      DO 111 I=2,N
      C(I)=IPL(I)
111 C(100+I)=IPL(I)
C
      RETURN
      END
      SUPEROUTINE LOGIC
      COMMON/COM/C(2000)
      COMMON/PROG/TACCX(50),TACCY(50),TACCZ(50),TPROG(50),
1 WPC(50),WRC(50),WQC(50),NTIME,TSWTCH(15),ISWTCH
      EQUIVALENCE (C(302),WQ),(C(303),WR),(C(301),WP)
      EQUIVALENCE (C(531),ACCX),(C(532),ACCY),(C(533),ACCZ)
      EQUIVALENCE (C(203),TIME),(C(311),TET)
      EQUIVALENCE (C(312),PHI),(C(272),VSPEED),(C(205),DT)
      IF(TIME.LT.TSWTCH(ISWTCH))GOTO 11
      IF(ISWTCH.EQ.1)GOTO 12
      IF(ISWTCH.EQ.2)GOTO 13
      PHI=0.
      TET=-.1745
      ISWTCH=ISWTCH+1
      GOTO 11
13 PHI=12.7*.01745
      TET=.1745
      ISWTCH=ISWTCH+1
      GOTO 11
12 PHI=0.
      TET=.096
      ISWTCH=ISWTCH+1
11 CONTINUE
C***FOR THIS N.L. MODEL TRANSITION BETWEEN COMPUTATIONALLY PREDICTED
C***STEADY STATES WILL ANYWAY BE ARTIFICIAL. THUS, THE TSWTCH-OPTION
C***IS DEFERRED AND ONLY THE FIRST SQUINT-SEGMENT IS USED IN EACH RUN.
C***RESULTS OF ALL RUNS APPEND TO EACH OTHER ON FILE 10('DISP MOD'-
C***OPTION OF FILEDEF-BEFORE THE CONSECUTIVE RUNS OF THE JOB).
C***THE CREATED FILE HAS ALL DATA-VARIABLES OF A GIVEN INSTANT AS A
C***RECORD.IT'S COMPATIBLE WITH APL-LINPLOT(BLANKS BETWEEN VALUES),

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C***AND A SEPARATE PROGRAM CONVERTS IT TO A TIME-VECTOR-RECORD FILE.
      WQ=SQUINT (TIME,TPROG,WQC,NTIME,1)
      WP=SQUINT (TIME,TPROG,WPC,NTIME,1)
      WR=SQUINT (TIME,TPROG,WRC,NTIME,1)
      ACCX=SQUINT (TIME,TPROG,TACCX,NTIME,1)
      ACCY=SQUINT (TIME,TPROG,TACCY,NTIME,1)
      ACCZ=SQUINT (TIME,TPROG,TACCZ,NTIME,1)
      RETURN
      END
      SUBROUTINE DYNAM
      COMMON/COM/C(2000)

C
      EQUIVALENCE (C(302),WQ), (C(311),TET), (C(315),DTET)
      EQUIVALENCE (C(321),VX), (C(323),VZ)
      EQUIVALENCE (C(334),XE), (C(336),ZE), (C(337),XED), (C(339),ZED)
      EQUIVALENCE (C(351),CEB11)
      EQUIVALENCE (C(353),CEB13), (C(357),CEB31), (C(359),CEB33)
      EQUIVALENCE (C(310),PSI), (C(312),PHI), (C(314),DPSI), (C(316),DPHI)
      EQUIVALENCE (C(301),WP), (C(303),WR)
      EQUIVALENCE (C(322),VY), (C(335),YE), (C(338),YED)
      EQUIVALENCE (C(439),CSF), (C(440),SNF), (C(441),CST), (C(442),SNT)
      EQUIVALENCE (C(352),CEB12), (C(354),CEB21), (C(355),CEB22)
      EQUIVALENCE (C(356),CEB23), (C(358),CEB32)
      EQUIVALENCE (C(531),ACCX), (C(532),ACCY), (C(533),ACCZ)
      EQUIVALENCE (C(271),USPEED), (C(272),VSPEED), (C(273),WSPEED)
      EQUIVALENCE (C(274),DUSPED), (C(275),DVSPED), (C(276),DWSPED)
      EQUIVALENCE (C(370),GRAV1)

C
      DPSI=(WR*CSF+WQ*SNF)/CST
      DTET=WQ*CSF-WR*SNF
      DPHI=WP+DPSI*SNT
      CALL DBTOI (USPEED,VSPEED,WSPEED,CEB11,CEB12,CEB13
1,CEB21,CEB22,CEB23,CEB31,CEB32,CEB33,VX,VY,VZ)
      XED=VX
      ZED=VZ
      YED=VY
      DUSPED=-WQ*WSPEED+WR*VSPEED-GRAV1*SNT +ACCX*GRAV1
C*****DVSPED=-WR*USPEED+WP*WSPEED+GRAV1*CST*SNF+ACCY*GRAV1-ASSUME COORD.
      DVSPED=0.
      DWSPED=+WQ*USPEED-WP*VSPEED+GRAV1*CST*CSF+ACCZ*GRAV1

C
C
      RETURN
      END
      SUBROUTINE FINISH
      COMMON/COM/C(2000)
      COMMON/REC/A3(2000,20)

C
      EQUIVALENCE (C(203),TIME), (C(217),LINE), (C(218),NPRINT)
      EQUIVALENCE (C(219),NPLOT), (C(220),IFR), (C(243),IF2), (C(242),CRAD)
      EQUIVALENCE (C(212),TIMPLT)

C
      ENTRY FINT
      WRITE (IF2,516)
516 FORMAT (1H , 'TIME IS OVER', ///)

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C

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      IF (NPLOT.LT.2) GOTO 518
      DO 121 I=1,NPLOT
121  WRITE (10,531) (A3(I,J),J=1,16)
531  FORMAT (1H,16 (F9.2,X))
      ENDFILE 10
      WRITE (IF2,517) NPLOT
517  FORMAT (1H,I15)
518  CONTINUE
      RETURN
      END
      SUBROUTINE CUPPT
      COMMON/COM/C(2000)
      COMMON/RUNCUT/DAN
      COMMON/REC/A3(2000,20)
      DIMENSION RDME(7),VOR(7)
      COMMON/ALBET/XBETA,ZBETA,XALPHA,YALPHA
      COMMON/STNAV/XST(7),YST(7),ZST(7),DIREQ(7),ISTDME,ISTVOR
1, R1(40),NOYES(40),SIGMA(40)
      EQUIVALENCE (C(336),ZE)
      EQUIVALENCE (C(203),TIME), (C(211),TIMPR), (C(212),TIMPLT)
      EQUIVALENCE (C(213),TIMTTY), (C(214),DTPR), (C(215),DIPLT)
      EQUIVALENCE (C(216),DTTY), (C(217),LINE), (C(218),NPRINT)
      EQUIVALENCE (C(219),NPLOT), (C(242),CRAD), (C(243),IF2)
      EQUIVALENCE (C(302),WQ), (C(321),VX), (C(323),VZ), (C(334),XE)
      EQUIVALENCE (C(343),HM), (C(311),TET)
      EQUIVALENCE (C(310),PSI), (C(312),PHI)
      EQUIVALENCE (C(301),WP), (C(303),WR), (C(322),VY), (C(335),YE)
      EQUIVALENCE (C(531),ACCX), (C(532),ACCY), (C(533),ACCZ)
      EQUIVALENCE (C(271),USPEED), (C(272),VSPEED), (C(273),WSPEED)

```

C  
C

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      WPJ=CRAD*WP+NOYES(1)*SIGMA(1)*R1(1)
      WQJ=CRAD*WQ+NOYES(2)*SIGMA(2)*R1(2)
      WRJ=CRAD*WR+NOYES(3)*SIGMA(3)*R1(3)
      PSIJ=CRAD*PSI+NOYES(4)*SIGMA(4)*R1(4)
      THETJ=CRAD*TET+NOYES(5)*SIGMA(5)*R1(5)
      PHIJ=CRAD*PHI+NOYES(6)*SIGMA(6)*R1(6)
      VAIR=SQRT(USPEED**2+VSPEED**2+WSPEED**2)+NOYES(7)*SIGMA(7)*R1(7)
      VRP=VSPEED+WR*XBETA-WP*ZBETA
      USPD=USPEED
      BETA=ATAN2(VRP,USPD)
      BETAJ=CRAD*BETA+NOYES(8)*SIGMA(8)*R1(8)
      WQR=WSPEED-WQ*XALPHA-WP*YALPHA
      ALPHA=ATAN2(WQR,USPD)
      ALPHAJ=CRAD*ALPHA+NOYES(9)*SIGMA(9)*R1(9)
      HM=-ZE+NOYES(10)*SIGMA(10)*R1(10)
      DO 301 I=1,ISTDME
301  RDME(I)=SQRT((XE-XST(I))**2+(YE-YST(I))**2+(ZE-ZST(I))**2)+
1NOYES(10+I)*SIGMA(10+I)*R1(10+I)
      DO 302 I=1,ISTVOR
      YVOR=YE-YST(I)
      XVOR=XE-XST(I)
      REQ=DIREQ(I)/CRAD
      RUNITX=COS(REQ)

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```

RUNITY=SIN(REQ)
VCOS=ABS((XVCR*RUNITY+YVOR*RUNITY)/SQRT(XVOR**2+YVOR**2))
RVOR1=ARCOS(VCOS)
RVOR=CRAD*RVOR1+NOYES(10+ISTDME+I)*SIGMA(10+ISTDME+I)*
1R1(10+ISTDME+I)
302 VOR(I)=SATF(RVOR,10.)
VXY=SQRT(VX*VX+VY*VY)
VZN=-VZ
GAMV=ATAN2(VZN,VXY)
GAMVJ=CRAD*GAMV
GAMH=ATAN2(VY,VX)
GAMHJ=CRAD*GAMH
ACCX=ACCX+NOYES(10+ISTDME+ISTVOR+1)*SIGMA(10+ISTDME+ISTVOR+1)*
1R1(10+ISTDME+ISTVOR+1)
ACCY=ACCY+NOYES(10+ISTDME+ISTVOR+2)*SIGMA(10+ISTDME+ISTVOR+2)*
1R1(10+ISTDME+ISTVOR+2)
ACCZ=ACCZ+NOYES(10+ISTDME+ISTVOR+3)*SIGMA(10+ISTDME+ISTVOR+3)*
1R1(10+ISTDME+ISTVOR+3)
C***NOW,IF TRIGGERED-CONTAMINATION BY NOISE;IF NOT-BYPASSED.
C
C***OUTPUT OPTIONS:
C*** 1.SHORT(TERMINAL) PRINTOUT;
C*** 2.LONG PRINTOUT OF FIRST BUNCH,SECOND OR BOTH;
C*** 3.CREATION OF 1SEC-INTERVAL-FILE OF DATA(SAME AS FLIGHT FILE)-
C*** -TO BE PRINTED,PLOTTED OR FURTHER PROCESSED.
C
IF (TIME.GT.0..AND.DAN.LT.1.) GOTO 879
PRINT 508
WRITE(IF2,511) TIME,VAIR,GAMVJ,GAMHJ,HM,XE,YE,PSIJ,THETJ,
1PHIJ,VOR(1),RDME(1),ALPHAJ,BETAJ
879 CONTINUE
IF (TIME.LE.TIMPR) GOTO 241
IF (LINE.NE.60) GOTO 259
WRITE(IF2,508)
508 FORMAT(1H1,' TIME VAIR GAMVJ GAMEJ HM XE
1YE PSIJ THETJ PHIJ VOR(1) RDME(1) ALPHAJ BETAJ')
NPRINT=NPRINT+1
LINE=1
259 CONTINUE
WRITE(IF2,511) TIME,VAIR,GAMVJ,GAMHJ,HM,XE,YE,PSIJ,THETJ,PHIJ,
1VOR(1),RDME(1),ALPHAJ,BETAJ
511 FORMAT(1H ,5F7.1,2F10.1,4F7.1,F11.1,2F7.1)
NPRINT=NPRINT+1
TIMPR=TIMPR+CTPR
LINE=LINE+1
241 IF (TIME.LE.TIMPLT.OR.NPLOT.GE.2000) GOTO 247
NPLOT=NPLOT+1
A3(NPLOT,1)=TIME
A3(NPLOT,2)=WPJ
A3(NPLOT,3)=WQJ
A3(NPLOT,4)=WRJ
A3(NPLOT,5)=ACCX
A3(NPLOT,6)=ACCY
A3(NPLOT,7)=ACCZ
A3(NPLOT,8)=HM

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      A3(NPLOT,9)=VAIR
      A3(NPLOT,10)=PSIJ
      A3(NPLOT,11)=THETJ
      A3(NPLOT,12)=PHIJ
      A3(NPLOT,13)=VOR(1)
      A3(NPLOT,14)=RDME(1)
      A3(NPLOT,15)=ALPHAJ
      A3(NPLOT,16)=BETAJ
      TIMPLT=TIMPLT+DTPLT
247   IF (TIME.LE.TIMTTY)GOTO 240
      IF (TIME.LT.(1.5*DTTTY))PRINT 510
510  FORMAT(1H1,' TIME          VAIR          GAMVJ          GAMHJ          XE          YE
      1   HM')
      PRINT 513,TIME,VAIR,GAMVJ,GAMHJ,XE,YE,HM
513  FORMAT(1H ,7F10.1)
      TIMTTY=TIMTTY+DTTTY
240  CONTINUE
C
      RETURN
      END
      FUNCTION SATF(X11,XM11)
      SATF=SIGN(AMIN1(ABS(X11),XM11),X11)
      RETURN
      END
      SUBROUTINE RCTAT
      COMMON/COM/C(2000)
      EQUIVALENCE (C(311),TET),(C(351),CEB11),(C(353),CEB13)
      EQUIVALENCE (C(357),CEB31),(C(359),CEB33)
      EQUIVALENCE (C(441),CST),(C(442),SNT)
      EQUIVALENCE (C(310),PSI),(C(312),PHI),(C(352),CEE12)
      EQUIVALENCE (C(354),CEB21),(C(355),CEB22),(C(356),CEB23)
      EQUIVALENCE (C(358),CEB32),(C(443),CSF),(C(444),SNP)
      EQUIVALENCE (C(439),CSF),(C(440),SNF)
C
      SNT=SIN(TET)
      CST=COS(TET)
      SNP=SIN(PSI)
      CSF=COS(PSI)
      SNF=SIN(PHI)
      CSF=COS(PHI)
C
      CEE11=CST*CSF
      CEB13=-SNT
      CEE31=+SNT*CSF*CSF+SNF*SNP
      CEB33=CST*CSF
      CEB12=CST*SNP
      CEB21=SNF*SNT*CSF-CSF*SNP
      CEB22=SNF*SNT*SNP+CSF*CSF
      CEB23=SNF*CST
      CEE32=CSF*SNT*SNP-SNF*CSF
      RETURN
      END
      SUBROUTINE DITOB(XI,YI,ZI,A11,A12,A13,A21,A22,A23,A31,A32,A33,
      1XO,YO,ZO)
      XO=A11*XI+A13*ZI+A12*YI

```

```

      ZO=A31*XI+A33*ZI+A32*YI
      YO=A21*XI+A22*YI+A23*ZI
      RETURN
      ENTRY DBTCI (XI,YI,ZI,A11,A12,A13,A21,A22,A23,A31,A32,A33,
1XO,YO,ZO)
      XO=A11*XI+A31*ZI+A21*YI
      ZO=A13*XI+A33*ZI+A23*YI
      YO=A12*XI+A22*YI+A32*ZI
      RETURN
      END
      SUBROUTINE RKG
      DIMENSION IPL(100),IPD(100)
      COMMON/COM/C(2000)
      COMMON/RK/ARK(4),BRK(4),CRK(4),QRK(100)
C
      EQUIVALENCE (C(201),N)
      EQUIVALENCE (C(205),H),(C(241),J)
C
      DO 100 I=1,N
      IL=C(I)
      ID=C(100+I)
      X1=C(ID)*H
      X2=(X1-BRK(J)*QRK(I))*ARK(J)
      C(IL)=C(IL)+X2
100  QRK(I)=QRK(I)+3.*X2-CRK(J)*X1
C
      RETURN
      END
      FUNCTION SQUINT(X,TABX,TABY,NTAB,N)
      DIMENSION TABX(NTAB),TABY(NTAB)
      IF (NTAB.NE.1) GOTO 1
      SQUINT=TABY(NTAB)
      RETURN
1  IF (X-TABX(N)) 2,3,4
2  N=N-1
   IF (N) 9,9,1
3  SQUINT=TABY(N)
   FACTOR=0.
   RETURN
4  IF ((N+1).GT.NTAB) GOTO 10
   IF (X-TABX(N+1)) 5,6,7
6  N=N+1
   GOTO 3
7  N=N+1
   GOTO 4
5  FACTOR=(X-TABX(N))/(TABX(N+1)-TABX(N))
   SQUINT=(TABY(N+1)-TABY(N))*FACTOR+TABY(N)
   RETURN
9  PRINT 1000,X,TABX(1)
   Y=SQRT(-1.)
   STOP
1000 FORMAT(1H,10('$'),'SQUINT UNDERFLOW - INPUT =',E15.8,' LESS THAGT
1N FIRST ARG. TABLE    ENTRY( ',E15.8,' ) ')
10  PRINT 2000,X,TABX(NTAB)
   Y=SQRT(-1.)

```

FILE: GTRAJ1 FCRTRAN A1 PRINCETON UNIVERSITY TIME-SHARING SYSTEM

```
      STCP
2000  FORMAT(1H ,10('$'), 'SQUINT OVERFLOW -INPUT =',E15.8 ,'  GREATER
      1  THAN  LAST  ARG. TABLE      ENTRY (' ,E15.8 ,' ) ' )
      END
```

GTR  
GTE  
GTR  
GTE



OPTIMAL FLIGHT PATH RECONSTRUCTION (B.3)

FILE: OPTFILT FORTRAN A

PRINCETON UNIVERSITY TIME-SHARING

```

C*
C*OPTIMAL FILTERING PROGRAM
C*
      IMPLICIT REAL*8(A-H,O-$)
      REAL*4 PREDCT(6)
      DIMENSION SUM(6),H112(11,6),H111(6,6)
      COMMON/DAT0/S2LIAC,S2XYZR,TIMSOF,X00(11),S2WIND,S2WNDZ,S2WNDY
1,S2V,S2ALF,S2BET,S2H,S2DME,S2VOR,S2BDME,S2ZR,PERCNT,OMEGA,AGLOBE
4,OUTL1,OUTL2,S2QA,S2QB
2,EPS2,TLAM0,SMEW0,XST,YST,ZST,DIREQ,KDME(20),NDME1(20),NDME2(20)
3,KDME2(20),NXP,NRATE,NSTEP,IDGT,ISTDME,ISTVOR,SOF
      LOGICAL GO,SOF
      NAMEDLIST/INP/FILE
      INTEGER FILE(2)
      NAMEDLIST/OK/GO
      NAMEDLIST/DAT/SOF,NXP,S2LIAC,S2XYZR,NRATE,TIMSOF,X00,NSTEP,IDGT
1,S2V,S2ALF,S2BET,S2H,S2DME,S2VOR,PERCNT,OMEGA,AGLOBE
4,OUTL1,OUTL2,S2QA,S2QB
2,EPS2,ISTDME,ISTVOR,XST,YST,ZST,DIREQ,KDME,NDME1,NDME2,S2WIND
3,TLAM0,SMEW0,S2WNDZ,S2BDME,S2ZR,S2WNDY,KDME2
      DIMENSION P(11,11),PO(11,11),HB(6,11),X0(11),XOUT(11)
1,RES(6),RK(6,6),HBT(11,6),PHT(11,6),HPHT(6,6),HPHTR(6,6)
2,HPHTRI(6,6),WKAREA(110),CKALM(11,6),DELY(11,1),RES1(6,1)
3,XPLUS(11),AIDEN(11,11),CH(11,11),UNMKH(11,11),PPLUS(11,11)
4,CKALMT(6,11),UNMKHT(11,11),STABK1(11,11),STABK2(11,11)
5,STABK3(6,11),STABK4(11,11)
      DIMENSION XST(7),YST(7),ZST(7),DIREQ(7)
1,XST7(7),YST7(7),ZST7(7),DIREQ7(7)

C***
      DEFINE FILE 12(60,2112,L,KSTPA)
C***
      1 CONTINUE
      PRINT 1002
1002 FORMAT(1H,'TYPE &INP FILE= &END')
      READ(5,INP)
      INF1=FILE(1)
      INF2=FILE(2)
      PRINT 2000,FILE
2000 FORMAT(2I10)
      PRINT 1004
1004 FORMAT(1H,'TYPE &DAT DATA= &END')
      READ(INF1,DAT)
      IF(SOF)GOTO 92
      PRINT 1003
1003 FORMAT(1H,'IF EVERYTHING O.K. TYPE &OK GO=.TRUE.&END')
      GO=.TRUE.
      READ(5,OK)
      IF(GO)GOTO 10
      GOTO 1
10 CONTINUE
C***
      DO 331 I=1,6
331 SUM(I)=0.0D0
C***
      PI=4.0D0*DATAN(1.0D0)

```

```
CRAD=180.0D0/PI
DO 17 I=1,NXP
17 X0(I)=X00(I)
KSTEP=0
KSTEP1=0
DO 101 I=1,NXP
DO 102 J=1,NXP
AIDEN(I,J)=0.0D0
102 P0(I,J)=0.0D0
101 CONTINUE
C*****
DO 109 I=1,NXP
109 AIDEN(I,I)=1.0D0
DO 104 I=1,6
DO 105 J=1,6
105 RK(I,J)=0.0D0
104 CONTINUE
RK(1,1)=S2V
RK(2,2)=S2ALF
RK(3,3)=S2BET
RK(4,4)=S2H
RK(5,5)=S2DME
RK(6,6)=S2DME
C***
DO 461 I=1,7
XST7(I)=XST(I)
YST7(I)=YST(I)
ZST7(I)=ZST(I)
461 DIREQ7(I)=DIREQ(I)
ISTV07=ISTVOR
ISTDM7=ISTDME
NRAT7=NRATE
TIMS7=TIMSOF
NXP7=NXP
S2LI7=S2LIAC
C***
IDME2=1
IDME=1
301 CONTINUE
KSTEP=KSTEP+1
KSTEP1=KSTEP1+1
C*
IFLAG=1
C***
IF(KDME(IDME).GT.KSTEP)GOTO 807
C*
DO 817 I=1,NXP7
DO 817 J=1,NXP7
817 IF(I.NE.J) P0(I,J)=0.0D0
IFLAG=5
C*
XST7(1)=XST(NDME1(IDME))
YST7(1)=YST(NDME1(IDME))
ZST7(1)=ZST(NDME1(IDME))
IDME=IDME+1
```

```

807 CONTINUE
C*
  IF(KDME2(IDME2).GT.KSTEP)GOTO 827
  DO 828 I=1,NXP7
  DO 828 J=1,NXP7
828 IF(I.NE.J)P0(I,J)=0.0D0
  IFLAG=5
  XST7(2)=XST(NDME2(IDME2))
  YST7(2)=YST(NDME2(IDME2))
  ZST7(2)=ZST(NDME2(IDME2))
  IDME2=IDME2+1
827 CONTINUE
C*
C*CALLING THE PROPAGATION-BETWEEN-MEASUREMENTS SUBROUTINE
C***
  CALL PROP27(TIM7,PERCNT,OMEGA,AGLOBE,EPS2,S2WNDY,TLAM0
  1,SMEW0,S2WIND,S2WNDZ,X0,P0,XST7,YST7,ZST7,DIREQ7,S2ZR,S2BDME
  3,OUTL1,OUTL2,S2QA,S2QB
  2,S2LI7,S2XYZR,XOUT,P,HB,RES,IFLAG,NRAT7,NXP7,ISTDM7,ISTVO7,KSTEP)
  DO 201 I=1,6
  DO 202 J=1,NXP
202 HBT(J,I)=HB(I,J)
201 CONTINUE
  CALL VMULFF(P,HBT,NXP,NXP,6,NXP,NXP,PHT,NXP,IER1)
  CALL VMULFF(HB,PHT,6,NXP,6,6,NXP,HPHT,6,IER2)
  DO 211 I=1,6
  DO 212 J=1,6
212 HPHTR(I,J)=HPHT(I,J)+RK(I,J)
211 CONTINUE
C***
  DO 341 I=1,6
341 SUM(I)=SUM(I)+HPHTR(I,I)
C***
  CALL LINV1F(HPHTR,6,6,HPHTRI,IDGT,WKAREA,IER3)
  CALL VMULFF(PHT,HPHTRI,NXP,6,6,NXP,6,CKALM,NXP,IER4)
  DO 221 I=1,6
221 RES1(I,1)=RES(I)
  CALL VMULFF(CKALM,RES1,NXP,6,1,NXP,6,DELX,NXP,IER5)
  DO 231 I=1,NXP
231 XPLUS(I)=XOUT(I)+DELX(I,1)
  CALL VMULFF(CKALM,HB,NXP,6,NXP,NXP,6,CH,NXP,IER6)
  DO 241 I=1,NXP
  DO 242 J=1,NXP
242 UNMKH(I,J)=AIDEN(I,J)-CH(I,J)
241 CONTINUE
C-OLD CALL VMULFF(UNMKH,P,NXP,NXP,NXP,NXP,NXP,PPLUS,NXP,IER7)
  DO 281 I=1,NXP
  DO 281 J=1,NXP
281 UNMKHT(J,I)=UNMKH(I,J)
  DO 283 I=1,NXP
  DO 283 J=1,6
283 CKALMT(J,I)=CKALM(I,J)
  CALL VMULFF(P,UNMKHT,NXP,NXP,NXP,NXP,NXP,STABK1,NXP,IER7)
  CALL VMULFF(UNMKH,STABK1,NXP,NXP,NXP,NXP,NXP,STABK2,NXP,IER8)
  CALL VMULFF(RK,CKALMT,6,6,NXP,6,6,STABK3,6,IER9)

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```

      CALL VMULFF(CKALM,STABK3,NXP,6,NXP,NXP,6,STABK4,NXP,IER10)
      DO 282 I=1,NXP
      DO 282 J=1,NXP
282  PPLUS(I,J)=STABK2(I,J)+STABK4(I,J)
C***
C***
      IF(KSTEP1.LT.5) GOTO 253
      KSTEP1=0
      DO 251 I=1,NXP
      DO 252 J=1,NXP
      IF(I.LE.J) GOTO 252
      PPLUS(I,J)=.5D0*(PPLUS(I,J)+PPLUS(J,I))
      PPLUS(J,I)=PPLUS(I,J)
252  CONTINUE
251  CONTINUE
253  CONTINUE
C*****
      DO 741 I=1,NXP
741  X0(I)=XPLUS(I)
      DO 742 I=1,NXP
      DO 742 J=1,NXP
742  P0(I,J)=PPLUS(I,J)
C***
      KSTEPA=KSTEP
C***
      WRITE(12,KSTEPA) (XPLUS(I),I=1,NXP)
      1, (XOUT(I),I=1,NXP), ((PPLUS(I,J),I=1,NXP),J=1,NXP)
      2, ((P(I,J),I=1,NXP),J=1,NXP)
C***
      IF(KSTEP.EQ.NSTEP) GOTO 311
C***
      GOTO 301
C***
311  CONTINUE
C***
      IF(NSTEP.GT.60) GOTO 1
      DO 342 I=1,6
342  PREDCT(I)=DSQRT(SUM(I)/59)
      PREDCT(2)=57.3*PREDCT(2)
      PREDCT(3)=57.3*PREDCT(3)
      PRINT 343, (PREDCT(I),I=1,6)
343  FORMAT(' ',F12.0,2F12.1,3F12.0)
C***
      GOTO 1
92  CONTINUE
      STOP
      END
      BLOCK DATA
      IMPLICIT REAL*8 (A-H,O-$)
      COMMON/DAT0/S2LIAC,S2XYZR,TIMSOF,X00(11),S2WIND,S2WNDZ,S2WNDY
      1,S2V,S2ALF,S2BET,S2H,S2DME,S2VOR,S2BDME,S2ZR,PERCNT,OMEGA,AGLOBE
      4,OUTL1,OUTL2,S2QA,S2QB
      2,EPS2,TLAM0,SMEW0,XST,YST,ZST,DIREQ,KDME(20),NDME1(20),NDME2(20)
      3,KDME2(20),NXP,NRATE,NSTEP,IDGT,ISTDME,ISTVOR,SOF
      DIMENSION XST(7),YST(7),ZST(7),DIREQ(7)

```

```
LOGICAL SOP
DATA SOP/.FALSE./,NXP/11/,S2LIAC/.4D0/,NRATE/20/,TIMSOF/1.0D0/
1,X00/0.0D0,0.0D0,-116.0D0,125.0D0,0.0D0,12.0D0,5*0.0D0/
2,S2V/6.25D0/,S2ALF/.000076D0/,S2WIND/.10D0/,S2WNDZ/.000001D0/
3,S2BET/.000076D0/,S2H/25.0D0/,S2DME/40000.0D0/,S2VOR/.000004D0/
4,NSTEP/60/,IDGT/3/,S2XYZR/25.0D0/,S2ZR/.10D0/
6,ISTDME/2/,ISTVOR/2/,S2BDME/.000025D0/,S2WNDY/.10D0/
7,XST/.703D0, .6985D0,5*.706D0/
8,YST/-1.297D0,-1.2985D0,5*-1.294D0/
9,ZST/7*0.0D0/
A,DIREQ/32.0D0,32.0D0,0.0D0,0.0D0,0.0D0,0.0D0,0.0D0/
B,KDME/1,19*2500/,NDME1/1,2,3,1,4,15*2/,NDME2/2,3,1,4,16*3/
C,OMEGA/.0000728D0/,AGLOBE/20940000.0D0/,EPS2/.0067D0/
D,TLAM0/.700D0/,SMEW0/-1.300D0/
DATA PERCNT/.000001D0/
1,KDME2/1,19*2600/
2,OUTL1/20000.0D0/,OUTL2/20000.0D0/,S2QA/.81D0/,S2QB/.81D0/
END
```

C\*

C\*\*\*STATE AND COVARIANCE MATRIX PROPAGATION BETWEEN MEASUREMENTS.

C\*

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SUBROUTINE PROP27(TIM SOP, PERC1, OMEG1, AGLOB1, EPS1, S2W0Y
1, TLAM00, SMEW00, S2W0, S2WZ, X0, P0, XST, YST, ZST, DIREQ, S2ZR1, S2BDM
3, OUTL1T, OUTL2T, S2QAT, S2QBT
2, S2LIAC, S2XYZR, XOUT, P, HB, RES, IFLAG7, NRATE, NXP, ISTDME, ISTVOR, KSTEP)
IMPLICIT REAL*8 (A-H, O-S)
EQUIVALENCE (IC(202), NRATE1), (C(311), TIMSF)
DIMENSION P0(11,11), X0(11), P01(11,11), P1(11,11), HB1(8,11), X01(11)
EQUIVALENCE (C(467), S2LIA), (C(373), S2XYZ)
EQUIVALENCE (IC(251), NXP1), (C(551), X01(1)), (C(593), P01(1,1))
EQUIVALENCE (C(993), HB1(1,1)), (C(793), P1(1,1))
DIMENSION HB(6,11), XOUT(11), P(11,11), RES(6), Z(11), ZCAL(8)
EQUIVALENCE (C(469), XE), (C(471), YE), (C(473), ZE)
EQUIVALENCE (C(481), USPEED), (C(483), VSPEED), (C(485), WSPEED)
EQUIVALENCE (C(571), Z(1)), (C(1235), ZCAL(1))
DIMENSION XST(7), YST(7), ZST(7), DIREQ(7), XST1(7), YST1(7), ZST1(7)
1, DIREQ1(7)
EQUIVALENCE (C(1257), XST1(1)), (C(1271), YST1(1))
EQUIVALENCE (C(1299), DIREQ1(1)), (C(1285), ZST1(1))
EQUIVALENCE (IC(252), ISTDME1), (IC(253), ISTVOR1)
EQUIVALENCE (IC(259), KSTEP1)
EQUIVALENCE (C(505), OMEGA), (C(507), AGLOBE), (C(509), EPS2)
EQUIVALENCE (C(511), TLAM0), (C(513), SMEW0)
EQUIVALENCE (C(470), S2WNDZ)

```

C\*\*\*

```

EQUIVALENCE (C(482), WX), (C(484), WY), (C(486), WZ)
EQUIVALENCE (C(468), S2WIND)
COMMON/COM/C(2000)
COMMON/INCOM/IC(500)

```

C\*\*\*

```

EQUIVALENCE (C(312), PERCNT), (C(381), S2ZR), (C(382), S2BDME)
1, (C(494), BDME1), (C(498), BDME2), (C(474), S2WNDY)
2, (IC(261), IFLAG), (C(502), OUTL1), (C(504), OUTL2)
3, (C(506), S2QA), (C(508), S2QB)
OUTL1=OUTL1T
OUTL2=OUTL2T
S2QA=S2QAT
S2QB=S2QBT
IFLAG=IFLAG7
S2WNDY=S2W0Y
S2ZR=S2ZR1
S2BDME=S2BDM
PERCNT=PERC1

```

C\*\*\*

```

OMEGA=OMEG1
AGLOBE=AGLOB1
EPS2=EPS1
TLAM0=TLAM00
SMEW0=SMEW00
KSTEP1=KSTEP
NRATE1=NRATE
TIMSF=TIMSOP
S2LIA=S2LIAC

```

```

S2XYZ=S2XYZR
S2WIND=S2W0
S2WNDZ=S2WZ
NXP1=NXP
DO 61 I=1,NXP1
61 X01(I)=X0(I)
DO 62 I=1,NXP1
DO 62 J=1,NXP1
P01(I,J)=P0(I,J)
62 CONTINUE
DO 64 I=1,7
XST1(I)=XST(I)
YST1(I)=YST(I)
ZST1(I)=ZST(I)
64 DIREQ1(I)=DIREQ(I)
ISTDM1=ISTDME
ISTV01=ISTVOR

```

C

```

CALL MYINIT
CALL MYRUN

```

C\*\*\*

```

DO 101 I=1,NXP1
DO 102 J=1,NXP1
IF(I.LT.J)GOTO 101
102 P1(J,I)=P1(I,J)
101 CONTINUE
XOUT(1)=XE
XOUT(2)=YE
XOUT(3)=ZE
XOUT(4)=USPEED
XOUT(5)=VSPEED
XOUT(6)=WSPEED
XOUT(7)=WX
XOUT(8)=WY
XOUT(9)=WZ

```

C\*

```

XOUT(10)=BDME1
XOUT(11)=BDME2

```

C\*\*\*K-TH VECTOR Z TRANSFERRED FROM INIT AND VECTOR ZCAL--FROM OUTPT

```

DO 111 I=1,6
111 RES(I)=Z(I+3)-ZCAL(I)

```

C\*

```

RES(5)=RES(5)-BDME1
RES(6)=RES(6)-BDME2

```

C\*\*\*

```

DO 52 I=1,NXP1
DO 52 J=1,NXP1
52 P(I,J)=P1(I,J)
DO 63 I=1,6
DO 63 J=1,NXP1
63 HB(I,J)=HB1(I,J)

```

C

```

RETURN
END
SUBROUTINE MYINIT

```

```

C      IMPLICIT REAL*8 (A-H,O-$)
C      CALL INIT
C      CALL DYNAMI
C      RETURN
C      END
C      SUBROUTINE MYRUN
C      IMPLICIT REAL*8 (A-H,O-$)
C      COMMON/COM/C (2000)
C      COMMON/INCOM/IC (500)
C      EQUIVALENCE (C (305),TIME), (IC (207),NSTEP)
C      EQUIVALENCE (IC (241),J1), (C (311),TIMSF)
C
C 242 CONTINUE
C      IF (TIME.LT.TIMSF) GOTO 82
C      CALL OUTPT
C      GOTO 100
C
C 82 CONTINUE
C
C ***R.K. LOOP
C
C      DO 246 J=1,4
C      J1=J
C      CALL DYNAM
C
C      CALL RKG
C 246 CONTINUE
C
C
C      NSTEP=NSTEP+1
C      GOTO 242
C 100 CONTINUE
C      RETURN
C      END
C      SUBROUTINE INIT
C      IMPLICIT REAL*8 (A-H,O-$)
C      REAL*4 Z1 (11),XA1 (6)
C      DIMENSION IPL (100),IPD (100)
C      COMMON/COM/C (2000)
C      COMMON/INCOM/IC (500)
C      COMMON/RK/ARK (4),BRK (4),CRK (4),QRK (100)
C
C      EQUIVALENCE (IC (251),NXP1), (C (467),S2LIA), (C (373),S2XYZ)
C      COMMON/FQ/PB (11,11),QB (11,11)
C      EQUIVALENCE (C (993),HB1 (1,1)), (C (571),Z (1))
C      DIMENSION HB1 (8,11),XA (6),Z (11)
C      EQUIVALENCE (IC (259),KSTEP1)
C
C      EQUIVALENCE (IC (201),N)
C      EQUIVALENCE (IC (202),NRATE1), (C (305),TIME), (C (307),TIMED)
C      EQUIVALENCE (C (303),DT), (IC (207),NSTEP)
C      EQUIVALENCE (C (309),CRAD), (C (301),GRAV1)
C      EQUIVALENCE (C (493),ACCX), (C (495),ACCY), (C (497),ACCZ)
C      EQUIVALENCE (C (313),WP), (C (315),WQ), (C (317),WR)
C      EQUIVALENCE (C (329),PHI), (C (327),TET), (C (325),PSI)

```



```

EQUIVALENCE (C(351),CEB11), (C(353),CEB12), (C(355),CEB13)
EQUIVALENCE (C(357),CEB21), (C(359),CEB22), (C(361),CEB23)
EQUIVALENCE (C(363),CEB31), (C(365),CEB32), (C(367),CEB33)
EQUIVALENCE (IC(1),IPL(1)), (IC(101),IPD(1))
EQUIVALENCE (C(468),S2WIND), (C(470),S2WINDZ)
1, (C(381),S2ZR), (C(382),S2BDME), (C(474),S2WNDY)
2, (IC(261),IFLAG), (C(502),OUTL1), (C(504),OUTL2)
3, (C(506),S2QA), (C(508),S2QB)

```

```

C
GRAV1=32.17D0

```

```

C
ARK(1)=.5D0
ARK(2)=1.0D0-1.0D0/DSQRT(2.0D0)
ARK(3)=1.0D0+1.0D0/DSQRT(2.0D0)
ARK(4)=1.0D0/6.0D0
BRK(1)=2.0D0
BRK(2)=1.0D0
BRK(3)=1.0D0
BRK(4)=2.0D0
CRK(1)=ARK(1)
CRK(2)=ARK(2)
CRK(3)=ARK(3)
CRK(4)=ARK(1)
DO 229 I=1,100
229 QRK(I)=0.0D0

```

```

C
PI=4.0D0*DATAN(1.0D0)
CRAD=180.0D0/PI

```

```

C
IPL(1)=305
IPD(1)=307
N=1
TIME=0.0D0
TIMED=1.0D0
NSTEP=0
NRAT=NRATE1
DT=1.0D0/DFLOAT(NRAT)

```

```

C***

```

```

C
DO 306 I=1,NXP1
DO 307 J=1,NXP1
307 FB(I,J)=0.0D0
306 CONTINUE
DO 308 I=1,8
DO 309 J=1,NXP1
309 HB1(I,J)=0.0D0
308 CONTINUE
HB1(4,3)=-1.0D0

```

```

C*
HB1(5,10)=1.0D0
HB1(6,11)=1.0D0
DO 311 I=1,NXP1
DO 312 J=1,NXP1
312 QB(I,J)=0.0D0
311 CONTINUE

```

```
QB(4,4)=S2LIA
QB(5,5)=S2QA
QB(6,6)=S2QB
DO 314 I=1,2
314 QB(I,I)=S2XYZ
QB(3,3)=S2ZR
QB(7,7)=S2WIND
QB(8,8)=S2WNDY
QB(9,9)=S2WNDZ
C*
QB(10,10)=S2BDME
QB(11,11)=S2BDME
C***
C***READ IN SMOOTHED VECTOR X OF MODEL A AND VECTOR Z AT K-TH TIME
C***POINT.Z COSTITUTES OF INPUT(ACCEL MEASUREMENTS) AND MEASUREMENT
C***MATRICES.FIRST NEEDED IN DYNAM AND SECOND--IN MAIN.
C
IF(KSTEP1.EQ.2) GOTO 319
READ(10) (XA1(I),I=1,6)
319 CONTINUE
READ(9) (Z1(I),I=1,11)
Z(5)=Z1(5)/CRAD
Z(6)=Z1(6)/CRAD
Z(10)=Z1(10)/CRAD
Z(11)=Z1(11)/CRAD
Z(4)=Z1(4)
Z(7)=Z1(7)
Z(8)=Z1(8)
Z(9)=Z1(9)
C***
WP=XA1(1)
WQ=XA1(2)
WR=XA1(3)
PHI=XA1(4)
TET=XA1(5)
PSI=XA1(6)
CALL ROTAT
ACCX=Z1(1)
ACCY=Z1(2)
ACCZ=Z1(3)
C*
C* IFLAG=5 FOR FIRST STEP
IF(IFLAG.NE.5) GOTO 837
OOR1=Z(8)
ONR1=Z(8)
OOR2=Z(9)
ONR2=Z(9)
GOTO 838
837 CONTINUE
IF(DABS(Z(8)-ONR1).LT.OUTL1) GOTO 839
Z(8)=ONR1+(ONR1-OOR1)
839 CONTINUE
OOR1=ONR1
ONR1=Z(8)
IF(DABS(Z(9)-ONR2).LT.OUTL2) GOTO 840
```

Z(9)=ONR2+(ONR2-00R2)

840 CONTINUE

00R2=ONR2

ONR2=Z(9)

838 CONTINUE

C\*

RETURN

END

SUBROUTINE DYNAMI

IMPLICIT REAL\*8 (A-H,O-S)

DIMENSION IPL(100),IPD(100)

COMMON/COM/C(2000)

COMMON/INCOM/IC(500)

C\*\*\*

DIMENSION X01(11),P01(11,11),P1(11,11)

EQUIVALENCE (C(337),CSF),(C(339),SNF),(C(341),CST),(C(343),SNT)

1,(C(505),OMEGA),(C(507),AGLOBE),(C(509),EPS2)

2,(C(511),TLAM0)

3,(C(351),CEB11),(C(352),CEB12),(C(353),CEB13)

4,(C(354),CEB21),(C(355),CEB22),(C(356),CEB23)

5,(C(357),CEB31),(C(358),CEB32),(C(359),CEB33)

6,(C(494),BDME1),(C(498),BDME2),(C(312),PERCNT),(C(311),TIMSF)

7,(C(313),WP),(C(315),WQ),(C(317),WR)

COMMON/PQ/FB(11,11),QB(11,11)

DIMENSION B60(11,11),FKDT(11,11),SUME(11,11),SUME1(11,11)

1,THAT(11,11),THATT(11,11),PTMATT(11,11),TMPTMT(11,11)

EQUIVALENCE (IC(251),NXP1),(C(551),X01(1)),(C(593),P01(1,1))

EQUIVALENCE (C(793),P1(1,1))

C\*\*\*

EQUIVALENCE (IC(201),N)

EQUIVALENCE (C(303),DT)

EQUIVALENCE (C(327),TET),(C(325),PSI),(C(329),PHI)

EQUIVALENCE (C(469),XE),(C(471),YE),(C(473),ZE)

EQUIVALENCE (C(481),USPEED),(C(485),WSPEED),(C(483),VSPRED)

EQUIVALENCE (IC(1),IPL(1)),(IC(101),IPD(1))

EQUIVALENCE (C(482),WX),(C(484),WY),(C(486),WZ)

C

N=N+1

IPL(N)=469

IPD(N)=475

N=N+1

IPL(N)=471

IPD(N)=477

N=N+1

IPL(N)=473

IPD(N)=479

N=N+1

IPL(N)=481

IPD(N)=487

N=N+1

IPL(N)=483

IPD(N)=489

N=N+1

IPL(N)=485

IPD(N)=491

```

N=N+1
  IPL (N) =482
  IPD (N) =488
N=N+1
  IPL (N) =484
  IPD (N) =490
N=N+1
  IPL (N) =486
  IPD (N) =492

```

```

N=N+1
  IPL (N) =494
  IPD (N) =496
N=N+1
  IPL (N) =498
  IPD (N) =500

```

$XE = X01 \quad (1)$   
 $YE = X01 \quad (2)$   
 $ZE = X01 \quad (3)$

```
USPEED=X01(4)
VSPEED=X01(5)
WSPEED=X01(6)
```

WX=X01 (7)  
WY=X01 (8)  
WZ=X01 (9)

BDME1=X01 (10)  
BDME2=X01 (11)

```

DO 201 I=1, NXP1
201 P1(I, 1)=P01(I, 1)
DO 202 I=2, NXP1
202 P1(I, 2)=P01(I, 2)
DO 203 I=3, NXP1
203 P1(I, 3)=P01(I, 3)
DO 204 I=4, NXP1
204 P1(I, 4)=P01(I, 4)
DO 205 I=5, NXP1
205 P1(I, 5)=P01(I, 5)
DO 206 I=6, NXP1
206 P1(I, 6)=P01(I, 6)
DO 207 I=7, NXP1
207 P1(I, 7)=P01(I, 7)
DO 208 I=8, NXP1
208 P1(I, 8)=P01(I, 8)
DO 209 I=9, NXP1
209 P1(I, 9)=P01(I, 9)
DO 210 I=10, NXP1
210 P1(I, 10)=P01(I, 10)
P1(11, 11)=P01(11, 11)

```

C\*\*\*

[illegible]

```

DO 101 I=1,NXP1
DO 102 J=1,NXP1
IF (I.LT.J) GOTO 101
102 P1(J,I)=P1(I,J)
101 CONTINUE

```

C\*\*\*

```

TLAM=TLAM0+XE/AGLOBE
COST=DCOS(TLAM)
SINT=DSIN(TLAM)
TANT=SINT/COST
SIN2T=2*SINT*COST
COS2T=COST*COST-SINT*SINT
C1111=1.0D0-ZE/AGLOBE-.5D0*EPS2*COS2T
C112=1/C1111

```

C

C

```

C141=C112*(ZE/AGLOBE+.5*EPS2*COS2T)
C111=(CEB11*USPEED+CEB21*VSPEED+CEB31*WSPEED+WX)/AGLOBE
C211=(CEB12*USPEED+CEB22*VSPEED+CEB32*WSPEED+WY)/AGLOBE
C241=-C112*YE*TANT/AGLOBE
C341=C112*EPS2*SIN2T
C56=OMEGA*(CEB11*COST-CEB13*SINT)
C64=OMEGA*(CEB21*COST-CEB23*SINT)
C45=OMEGA*(CEB31*COST-CEB33*SINT)

```

C\*\*\*

```

C413=OMEGA*(CEB11*SINT+CEB13*COST)
C412=OMEGA*(CEB21*SINT+CEB23*COST)
C411=OMEGA*(CEB31*SINT+CEB33*COST)
CENT1=-OMEGA**2*AGLOBE*C1111*.5*SIN2T
CENT2=-OMEGA**2*AGLOBE*C1111*COST**2
C47=2*(+WR*CEB21-WQ*CEB31)+OMEGA*CEB12*SINT
C48=2*(+WR*CEB22-WQ*CEB32)-C413
C49=2*(+WR*CEB23-WQ*CEB33)-OMEGA*CEB12*COST
C57=2*(-WR*CEB11+WP*CEB31)+OMEGA*CEB22*SINT
C58=2*(-WR*CEB12+WP*CEB32)-C412
C59=2*(-WR*CEB13+WP*CEB33)-OMEGA*CEB22*COST
C67=2*(+WQ*CEB11-WP*CEB21)+OMEGA*CEB32*SINT
C68=2*(+WQ*CEB12-WP*CEB22)-C411
C69=2*(+WQ*CEB13-WP*CEB23)-OMEGA*CEB32*COST

```

C

C\*\*\*

```

C1122=C112*C112
C2112=C211*C1122
C13=C111*C1122
C11=-EPS2*SIN2T*C13
C31=C111*C112*EPS2*(2*COS2T-C112*EPS2*SIN2T*SIN2T)
C33=C13*EPS2*SIN2T
C21=-EPS2*SIN2T*C2112+C13*(-C1111+.5D0*EPS2*SIN2T*SIN2T)*YE/
1 AGLOBE/COST/COST
C22=-C111*C112*TANT
C23=C2112-C13*TANT*YE/AGLOBE
C14=C141*CEB11
C15=C141*CEB21
C16=C141*CEB31
C24=C241*CEB11+C141*CEB12

```

```

C25=C241*CEB21+C141*CEB22
C26=C241*CEB31+C141*CEB32
C34=C341*CEB11
C35=C341*CEB21
C36=C341*CEB31
C17=C141
C27=C241
C28=C141
C37=C341
C411=OMEGA*(CEB31*SINT+CEB33*COST)
C412=OMEGA*(CEB21*SINT+CEB23*COST)
C413=OMEGA*(CEB11*SINT+CEB13*COST)
C433=OMEGA*COST
C43=C433*C413
C53=C433*C412
C63=C433*C411
COST1=COST*OMEGA/AGLOBE
SINT1=SINT*OMEGA/AGLOBE
C4111=(C1111*COS2T+.5D0*EPS2*SIN2T*SIN2T)*OMEGA*OMEGA
C4112=(C1111*SIN2T- EPS2*SIN2T*COST*COST)*OMEGA*OMEGA
C41=(WSPEED*C412-VSPEED*C411)/AGLOBE
1-CEB11*C4111+CEB13*C4112+COST1*(WX*CEB12-WY*CEB11)+SINT1*(
2 WY*CEB13+WZ*CEB12)
C51=(USPEED*C411-WSPEED*C413)/AGLOBE
1-CEB21*C4111+CEB23*C4112+COST1*(WX*CEB22-WY*CEB21)+SINT1*(
2 WY*CEB23+WZ*CEB22)
C61=(VSPEED*C413-USPEED*C412)/AGLOBE
1-CEB31*C4111+CEB33*C4112+COST1*(WX*CEB32-WY*CEB31)+SINT1*(
2 WY*CEB33+WZ*CEB32)
C65=-C56
C46=-C64
C54=-C45
FB(1,1)=C11
FB(2,1)=C21
FB(3,1)=C31
FB(4,1)=C41
FB(5,1)=C51
FB(6,1)=C61
FB(2,2)=C22
FB(1,3)=C13
FB(2,3)=C23
FB(3,3)=C33
FB(4,3)=C43
FB(5,3)=C53
FB(6,3)=C63
FB(1,4)=CEB11+C14
FB(2,4)=CEB12+C24
FB(3,4)=+CEB13+C34
FB(1,5)=CEB21+C15
FB(2,5)=CEB22+C25
FB(3,5)=+CEB23+C35
FB(1,6)=CEB31+C16
FB(2,6)=CEB32+C26
FB(3,6)=+CEB33+C36
FB(5,4)=-WR+C54

```

```

FB(6,4)=WQ+C64
FB(4,5)=WR+C45
FB(6,5)=-WP+C65
FB(4,6)=-WQ+C46
FB(5,6)=WP+C56
FB(1,7)=1.0D0+C17
FB(2,8)=1.0D0+C141
FB(3,9)=1.0D0
FB(2,7)=C27
FB(3,7)=C37
FB(4,7)=C47
FB(4,8)=C48
FB(4,9)=C49
FB(5,7)=C57
FB(5,8)=C58
FB(5,9)=C59
FB(6,7)=C67
FB(6,8)=C68
FB(6,9)=C69

```

C\*\*\*\*

C

```

CALL CSTM(FB,PERCNT,TIMSP,TMAT,B60,FKDT,SUME,SUME1,NXP1,NTERMS)
DO 600 I=1,NXP1
DO 600 J=1,NXP1
600 TMATT(J,I)=TMAT(I,J)
DO 610 I=1,NXP1
DO 610 J=1,NXP1
610 TMPTMT(I,J)=P1(I,J)+QB(I,J)
CALL VMULFF(TMPTMT,TMATT,NXP1,NXP1,NXP1,NXP1,NXP1,PTMATT,NXP1,I1)
CALL VMULFF(TMAT,PTMATT,NXP1,NXP1,NXP1,NXP1,NXP1,P1,NXP1,I2)

```

C

```

RETURN
END
SUBROUTINE DYNAM
IMPLICIT REAL*8(A-H,O-$)
COMMON/COM/C(2000)
COMMON/INCOM/IC(500)

```

C\*\*\*

```

EQUIVALENCE(IC(251),NXP1)
COMMON/FQ/FB(11,11),QB(11,11)
EQUIVALENCE(C(494),BDME1),(C(496),DBDME1)
1,(C(498),BDME2),(C(500),DBDME2)
EQUIVALENCE(C(793),P1(1,1))
EQUIVALENCE(C(401),DP11),(C(402),DP21),(C(403),DP31)
EQUIVALENCE(C(404),DP41),(C(405),DP51),(C(406),DP61)
EQUIVALENCE(C(407),DP71),(C(408),DP81),(C(409),DP91)
EQUIVALENCE(C(410),DP22),(C(411),DP32),(C(412),DP42)
EQUIVALENCE(C(413),DP52),(C(414),DP62),(C(415),DP72)
EQUIVALENCE(C(416),DP82),(C(417),DP92)
EQUIVALENCE(C(418),DP33),(C(419),DP43),(C(420),DP53)
EQUIVALENCE(C(421),DP63),(C(422),DP73),(C(423),DP83)
EQUIVALENCE(C(424),DP93)
EQUIVALENCE(C(425),DP44),(C(426),DP54),(C(427),DP64)
EQUIVALENCE(C(428),DP74),(C(429),DP84),(C(430),DP94)
EQUIVALENCE(C(431),DP55),(C(432),DP65),(C(433),DP75)

```

```

EQUIVALENCE (C(434),DP85), (C(435),DP95), (C(436),DP66)
EQUIVALENCE (C(437),DP76), (C(438),DP86), (C(439),DP96)
EQUIVALENCE (C(440),DP77), (C(441),DP87), (C(442),DP97)
EQUIVALENCE (C(443),DP88), (C(444),DP98), (C(445),DP99)
EQUIVALENCE (C(319),WPD), (C(321),WQD), (C(323),WRD)
DIMENSION DPM(11,11),FP(11,11),P1(11,11)

```

C\*\*\*

```

EQUIVALENCE (C(482),WX), (C(484),WY), (C(486),WZ)
EQUIVALENCE (C(488),DWX), (C(490),DWY), (C(492),DWZ)

```

C

```

EQUIVALENCE (C(315),WQ), (C(327),TET), (C(333),DTET)
EQUIVALENCE (C(499),VX), (C(503),VZ)
EQUIVALENCE (C(469),XE), (C(473),ZE), (C(475),XED), (C(479),ZED)
EQUIVALENCE (C(351),CEB11)
EQUIVALENCE (C(355),CEB13), (C(363),CEB31), (C(367),CEB33)
EQUIVALENCE (C(325),PSI), (C(329),PHI), (C(331),DPSI), (C(335),DPHI)
EQUIVALENCE (C(313),WP), (C(317),WR)
EQUIVALENCE (C(501),VY), (C(471),YE), (C(477),YED)
EQUIVALENCE (C(337),CSF), (C(339),SNF), (C(341),CST), (C(343),SNT)
EQUIVALENCE (C(353),CEB12), (C(357),CEB21), (C(359),CEB22)
EQUIVALENCE (C(361),CEB23), (C(365),CEB32)
EQUIVALENCE (C(493),ACCX), (C(495),ACCY), (C(497),ACCZ)
EQUIVALENCE (C(481),USPEED), (C(483),VSPEED), (C(485),WSPEED)
EQUIVALENCE (C(487),DUSPED), (C(489),DVSPED), (C(491),DWSPED)
EQUIVALENCE (C(301),GRAV1)
EQUIVALENCE (C(511),TLAM0)
EQUIVALENCE (C(505),OMEGA), (C(507),AGLOBE), (C(509),EPS2)

```

C\*\*\*

C

```

CALL DBTOI(USPEED,VSPEED,WSPEED,CEB11,CEB12,CEB13
1,CEB21,CEB22,CEB23,CEB31,CEB32,CEB33,VX,VY,VZ)

```

C\*\*\*

```

DO 101 I=1,NXP1
DO 102 J=1,NXP1
IF(I.LT.J)GOTO 101
102 P1(J,I)=P1(I,J)
101 CONTINUE
TLAM=TLAM0+XE/AGLOBE
COST=DCOS(TLAM)
SINT=DSIN(TLAM)
TANT=SINT/COST
SIN2T=2*SINT*COST
COS2T=COST*COST-SINT*SINT
C1111=1.0D0-ZE/AGLOBE-.5D0*EPS2*COS2T
C112=1/C1111

```

C

C

```

C141=C112*(ZE/AGLOBE+.5*EPS2*COS2T)
C111=(CEB11*USPEED+CEB21*VSPEED+CEB31*WSPEED+WX)/AGLOBE
C211=(CEB12*USPEED+CEB22*VSPEED+CEB32*WSPEED+WY)/AGLOBE
C241=-C112*YE*TANT/AGLOBE
C341=C112*EPS2*SIN2T
C56=OMEGA*(CEB11*COST-CEB13*SINT)
C64=OMEGA*(CEB21*COST-CEB23*SINT)
C45=OMEGA*(CEB31*COST-CEB33*SINT)

```



```

XED=VX+WX+C141*C111*AGLOBE
ZED=+VZ+WZ+C341*C111*AGLOBE
YED=VY+WY+C141*C211*AGLOBE+C241*C111*AGLOBE

```

C\*\*\*

```

C413=OMEGA*(CEB11*SINT+CEB13*COST)
C412=OMEGA*(CEB21*SINT+CEB23*COST)
C411=OMEGA*(CEB31*SINT+CEB33*COST)
CENT1=-OMEGA**2*AGLOBE*C1111*.5*SIN2T
CENT2=-OMEGA**2*AGLOBE*C1111*COST**2
C47=2*(+WR*CEB21-WQ*CEB31)+OMEGA*CEB12*SINT
C48=2*(+WR*CEB22-WQ*CEB32)-C413
C49=2*(+WR*CEB23-WQ*CEB33)-OMEGA*CEB12*COST
C57=2*(-WR*CEB11+WP*CEB31)+OMEGA*CEB22*SINT
C58=2*(-WR*CEB12+WP*CEB32)-C412
C59=2*(-WR*CEB13+WP*CEB33)-OMEGA*CEB22*COST
C67=2*(+WQ*CEB11-WP*CEB21)+OMEGA*CEB32*SINT
C68=2*(+WQ*CEB12-WP*CEB22)-C411
C69=2*(+WQ*CEB13-WP*CEB23)-OMEGA*CEB32*COST

```

C

C\*\*\*

```

DUSPED=-WQ*WSPEED+WR*VSPEED+ACCX*GRAV1
1+C45*VSPEED-C64*WSPEED
2+C47*WX+C48*WY+C49*WZ+CENT1*CEB11+CENT2*CEB13

```

C\*

C\*

```

DVSPED=-WR*USPEED+WP*WSPEED+ACCY*GRAV1
1-C45*USPEED+C56*WSPEED
2+C57*WX+C58*WY+C59*WZ+CENT1*CEB21+CENT2*CEB23
DWSPED=+WQ*USPEED-WP*VSPEED+ACCZ*GRAV1
1+C64*USPEED-C56*VSPEED
2+C67*WX+C68*WY+C69*WZ+CENT1*CEB31+CENT2*CEB33

```

C

```

DWX=0.0D0
DWY=0.0D0
DWZ=0.0D0

```

C\*

```

DBDME1=0.0D0
DBDME2=0.0D0

```

C\*\*\*

C

```

RETURN
END
SUBROUTINE OUTPT
IMPLICIT REAL*8(A-H,O-$)
COMMON/COM/C(2000)
COMMON/INCOM/IC(500)
DIMENSION RDME(7),VOR(7)

```

C\*\*\*

```

DIMENSION XST1(7),YST1(7),ZST1(7),DIREQ1(7)
EQUIVALENCE (C(1257),XST1(1)),(C(1271),YST1(1)),(C(1285),ZST1(1))
EQUIVALENCE (C(1299),DIREQ1(1)),(IC(252),ISTDM1),(IC(253),ISTVO1)
EQUIVALENCE (C(993),HB1(1,1))
EQUIVALENCE (C(1235),ZCAL(1))
DIMENSION ZCAL(8),HB1(8,11)

```

C

```

EQUIVALENCE (C(309),CRAD)
EQUIVALENCE (C(473),ZE)
EQUIVALENCE (C(305),TIME)
EQUIVALENCE (C(315),WQ),(C(499),VX),(C(503),VZ),(C(469),XE)
EQUIVALENCE (C(327),TET)
EQUIVALENCE (C(325),PSI),(C(329),PHI)
EQUIVALENCE (C(313),WP),(C(317),WR),(C(501),VY),(C(471),YE)
EQUIVALENCE (C(493),ACCX),(C(495),ACCY),(C(497),ACCZ)
EQUIVALENCE (C(481),USPEED),(C(483),VSPEED),(C(485),WSPEED)
EQUIVALENCE (C(507),AGLOBE),(C(509),EPS2)
EQUIVALENCE (C(511),TLAM0),(C(513),SMEW0)
DIMENSION XDME(7),YDME(7),ZDME(7)

C***
TLAM=TLAM0+XE/AGLOBE
COST=DCOS(TLAM)
SINT=DSIN(TLAM)
TANT=SINT/COST
SMEW=SMEW0+YE/AGLOBE/COST
SIN2T=2*SINT*COST
COS2T=COST*COST-SINT*SINT
C1111=1.0D0-.5D0*EPS2*COS2T-ZE/AGLOBE
AC1111=AGLOBE*C1111
COSS=DCOS(SMEW)
SINS=DSIN(SMEW)
RX1=EPS2*SIN2T*COST*COSS-C1111*SINT*COSS-C1111*TANT*SINS*YE/AGLOBE
RX2=EPS2*SIN2T*COST*SINS-C1111*SINT*SINS+C1111*TANT*COSS*YE/AGLOBE
RX3=EPS2*SIN2T*SINT+C1111*COST

C
C***VECTORS X OF MODEL A AND Z(K-TH TIME POINT) OF MODEL B(WITHOUT
C***ACCEL) TRANSFERRED FROM INIT
C
VAIR2=USPEED**2+VSPEED**2+WSPEED**2
VAIR=DSQRT(VAIR2)
VRP=VSPEED
USPD=USPEED
BETA=DATAN2(VRP,USPD)
WQR=WSPEED
ALPHA=DATAN2(WQR,USPD)
DO 301 I=1,ISTDM1
XDME(I)=AC1111*COST*COSS-DCOS(XST1(I))*DCOS(YST1(I))*
1 (-ZST1(I)+AGLOBE*(1.0D0-.5D0*EPS2*DCOS(2*XST1(I))))
YDME(I)=AC1111*COST*SINS-DCOS(XST1(I))*DSIN(YST1(I))*
1 (-ZST1(I)+AGLOBE*(1.0D0-.5D0*EPS2*DCOS(2*XST1(I))))
ZDME(I)=AC1111*SINT-DSIN(XST1(I))*
1 (-ZST1(I)+AGLOBE*(1.0D0-.5D0*EPS2*DCOS(2*XST1(I))))
C***XST,YST ARE LATITUDE AND LONGITUDE
301 RDME(I)=DSQRT(XDME(I)**2+YDME(I)**2+ZDME(I)**2)
C
C*301 RDME(I)=DSQRT((XE-XST1(I))**2+(YE-YST1(I))**2+(ZE-ZST1(I))**2)
C
DO 302 I=1,ISTVO1
302 VOR(I)=1.
C***
ZCAL(1)=VAIR
ZCAL(2)=ALPHA

```

```

ZCAL(3)=BETA
ZCAL(4)=-ZE
ZCAL(5)=RDME(1)
ZCAL(6)=RDME(2)
ZCAL(7)=VOR(1)
ZCAL(8)=VOR(2)

```

C

```

HB1(5,1)=(RX1*XDME(1)+RX2*YDME(1)+RX3*ZDME(1))/RDME(1)
HB1(6,1)=(RX1*XDME(2)+RX2*YDME(2)+RX3*ZDME(2))/RDME(2)
HB1(5,2)=(-C1111*SINS*XDME(1)+C1111*COSS*YDME(1))/RDME(1)
HB1(6,2)=(-C1111*SINS*XDME(2)+C1111*COSS*YDME(2))/RDME(2)
HB1(5,3)=(-COST*COSS*XDME(1)-COST*SINS*YDME(1)-SINT*ZDME(1))
1/RDME(1)
HB1(6,3)=(-COST*COSS*XDME(2)-COST*SINS*YDME(2)-SINT*ZDME(2))
1/RDME(2)
HB1(7,1)=-(YE-YST1(1))/(RDME(1)**2-(ZE-ZST1(1))**2)
HB1(8,1)=-(YE-YST1(2))/(RDME(2)**2-(ZE-ZST1(2))**2)
HB1(7,2)=(XE-XST1(1))/(RDME(1)**2-(ZE-ZST1(1))**2)
HB1(8,2)=(XE-XST1(2))/(RDME(2)**2-(ZE-ZST1(2))**2)
HB1(1,4)=USPEED/VAIR
HB1(2,4)=-WSPEED/(VAIR2-VSPEED**2)
HB1(3,4)=-VSPEED/(VAIR2-WSPEED**2)
HB1(1,5)=VSPEED/VAIR
HB1(3,5)=USPEED/(VAIR2-WSPEED**2)
HB1(1,6)=WSPEED/VAIR
HB1(2,6)=USPEED/(VAIR2-VSPEED**2)

```

C

```

RETURN
END
FUNCTION SATF(X11,XM11)
IMPLICIT REAL*8(A-H,O-$)
SATF=DSIGN(DMIN1(DABS(X11),XM11),X11)
RETURN
END
SUBROUTINE ROTAT
IMPLICIT REAL*8(A-H,O-$)
COMMON/COM/C(2000)
EQUIVALENCE (C(327),TET),(C(351),CEB11),(C(355),CEB13)
EQUIVALENCE (C(363),CEB31),(C(367),CEB33)
EQUIVALENCE (C(341),CST),(C(343),SNT)
EQUIVALENCE (C(325),PSI),(C(329),PHI),(C(353),CEB12)
EQUIVALENCE (C(357),CEB21),(C(359),CEB22),(C(361),CEB23)
EQUIVALENCE (C(365),CEB32),(C(345),CSP),(C(347),SNP)
EQUIVALENCE (C(337),CSF),(C(339),SNF)

```

C

```

SNT=DSIN(TET)
CST=DCOS(TET)
SNP=DSIN(PSI)
CSP=DCOS(PSI)
SNF=DSIN(PHI)
CSF=DCOS(PHI)

```

C

```

CEB11=CST*CSP
CEB13=-SNT
CEB31=+SNT*CSF*CSP+SNF*SNP

```

```

CEB33=CST*CSF
CEB12=CST*SNP
CEB21=SNF*SNP*CSF-CSF*SNP
CEB22=SNF*SNP*SNP+CSF*CSF
CEB23=SNF*CSF
CEB32=CSF*SNP*SNP-SNP*CSF
RETURN
END

```

```

SUBROUTINE DITOB(XI,YI,ZI,A11,A12,A13,A21,A22,A23,A31,A32,A33,
1XO,YO,ZO)

```

```

IMPLICIT REAL*8(A-H,O-$)
XO=A11*XI+A13*ZI+A12*YI
ZO=A31*XI+A33*ZI+A32*YI
YO=A21*XI+A22*YI+A23*ZI
RETURN

```

```

ENTRY DBTOI(XI,YI,ZI,A11,A12,A13,A21,A22,A23,A31,A32,A33,
1XO,YO,ZO)

```

```

XO=A11*XI+A31*ZI+A21*YI
ZO=A13*XI+A33*ZI+A23*YI
YO=A12*XI+A22*YI+A32*ZI
RETURN

```

```

END

```

```

SUBROUTINE RKG

```

```

IMPLICIT REAL*8(A-H,O-$)
DIMENSION IPL(100),IPD(100)
COMMON/COM/C(2000)
COMMON/RK/ARK(4),BRK(4),CRK(4),QRK(100)
COMMON/INCOM/IC(500)

```

```

EQUIVALENCE (IC(201),N)
EQUIVALENCE (C(303),H), (IC(241),J)
EQUIVALENCE (IC(1),IPL(1)), (IC(101),IPD(1))

```

```

DO 100 I=1,N

```

```

IL=IPL(I)

```

```

ID=IPD(I)

```

```

X1=C(ID)*H

```

```

X2=(X1-BRK(J)*QRK(I))*ARK(J)

```

```

C(IL)=C(IL)+X2

```

```

100 QRK(I)=QRK(I)+3.0D0*X2-CRK(J)*X1

```

```

RETURN

```

```

END

```

```

C*
C*OPTIMAL SMOOTHING PROGRAM
C*
  IMPLICIT REAL*8(A-H,O-$)
  REAL*4 XS1(11),PS1(9,9),XAS(6,1)
  COMMON/DAT0/PERCNT,DT,TLAM0,OMEGA,AGLOBE,EPS2,IDGT,NSTEP,NXP,SOF
  LOGICAL GO,SOF
  NAMEDLIST/INP/FILE
  INTEGER FILE(2)
  NAMEDLIST/OK/GO
  NAMEDLIST/DAT/SOF,NSTEP,NXP,PERCNT,DT,IDGT,TLAM0
  1,OMEGA,AGLOBE,EPS2
C***
  DEFINE FILE 17( 150,368,L,KSTPG)
  DEFINE FILE 12( 150,2112,L ,KSTPA)
  DIMENSION XPK12(11),XMK12(11),PPK12(11,11),PMK12(11,11)
C*
  DIMENSION XPK1(6),XMK1(6),XPK(6),XMK(6)
  1,PPK1(6,6),PMK1(6,6),PPK(6,6),PMK(6,6)
  2,FK(6,6),THAT(6,6),TMATT(6,6),PTMATT(6,6)
  3,PINV(6,6),WKAREA(60),AK(6,6),AKT(6,6)
  4,DELX(6,1),DELP(6,6),DELXES(6,1),XS(6)
  5,AKDELP(6,6),ADPAT(6,6),PS(6,6)
  6,PMK2(6,6)
C***
  DIMENSION B60(6,6),FKDT(6,6),SUME(6,6),SUME1(6,6)
C***
  1 CONTINUE
  PRINT 1002
  1002 FORMAT(1H,'TYPE &INP FILE= &END')
  READ(5,INP)
  INF1=FILE(1)
  INF2=FILE(2)
  PRINT 2000,FILE
  2000 FORMAT(2I10)
  PRINT 1004
  1004 FORMAT(1H,'TYPE &DAT DATA= &END')
  READ(INF1,DAT)
  IF(SOF)GOTO 92
  PRINT 1003
  1003 FORMAT(1H,'IF EVERYTHING O.K. TYPE &OK GO=.TRUE.&END')
  GO=.TRUE.
  READ(5,OK)
  IF(GO)GOTO 10
  GOTO 1
  10 CONTINUE
C***
C***
  KSTEP=NSTEP
  KSTEP1=0
C***
  KSTPA=KSTEP
C*
  PI=4.0D0*DATAN(1.0D0)
  CRAD=180.0D0/PI

```

```

C***      READ(10) (XAS(I,1),I=1,6)
          READ(12,KSTEPS) (XPK12(I),I=1,11)
          1, (XMK12(I),I=1,11), ((PPK12(I,J),I=1,11),J=1,11)
          2, ((PMK12(I,J),I=1,11),J=1,11)

C*
      DO 431 I=1,NXP
        XPK1(I)=XPK12(I)
431    XMK1(I)=XMK12(I)
      DO 432 I=1,NXP
        DO 432 J=1,NXP
          PPK1(I,J)=PPK12(I,J)
432    PMK1(I,J)=PMK12(I,J)

C***
      DO 581 I=1,NXP
581    XS(I)=XPK1(I)
      DO 582 I=1,NXP
        DO 582 J=1,NXP
          PS(I,J)=PPK1(I,J)
          KSTEPS=KSTEP
      DO 709 I=1,NXP
709    XS1(I)=XS(I)
      DO 710 I=1,NXP
        DO 710 J=1,NXP
          PS1(I,J)=PS(I,J)
710    XS1(7)=XPK12(7)
          XS1(8)=XPK12(8)
          XS1(9)=XPK12(9)
          DO 801 I=7,9
            DO 801 J=1,9
              PS1(I,J)=PPK12(I,J)
          DO 802 I=1,6
            DO 802 J=7,9
              PS1(I,J)=PPK12(I,J)
802    PS1(I,J)=PPK12(I,J)

C***
      XS1(10)=XPK12(10)
      XS1(11)=XPK12(11)
      WRITE(17,KSTEPS) (XS1(I),I=1,11)
      1, ((PS1(I,J),I=1,9),J=1,9)

C***
      DO 591 I=1,NXP
        DO 591 J=1,NXP
591    FK(I,J)=0.

C***
C***
301  CONTINUE
      KSTEP=KSTEP-1
      IF(KSTEP.LT.1) GOTO 311
      KSTEP1=KSTEP+1

C***
      KSTEPS=KSTEP

C***
      READ(10) (XAS(I,1),I=1,6)
      READ(12,KSTEPS) (XPK12(I),I=1,11)
      1, (XMK12(I),I=1,11), ((PPK12(I,J),I=1,11),J=1,11)

```

2, ((PMK12(I,J), I=1,11), J=1,11)

C\*

```
DO 441 I=1,NXP
  XPK(I)=XPK12(I)
441 XMK(I)=XMK12(I)
DO 442 I=1,NXP
  DO 442 J=1,NXP
    PPK(I,J)=PPK12(I,J)
442 PMK(I,J)=PMK12(I,J)
```

C\*\*\*

C\*\*\*FK-MATRIX COMPUTATION

```
WP=XAS(1,1)
WQ=XAS(2,1)
WR=XAS(3,1)
PHI=XAS(4,1)
TET=XAS(5,1)
PSI=XAS(6,1)
SNT=DSIN(TET)
CST=DCOS(TET)
SNP=DSIN(PHI)
CSF=DCOS(PHI)
SNP=DSIN(PSI)
CSP=DCOS(PSI)
```

C\*\*\*

```
CEB11=CST*CSP
CEB12=CST*SNP
CEB13=-SNT
CEB21=SNP*SNT*CSP-CSF*SNP
CEB22=SNP*SNT*SNP+CSF*CSP
CEB23=+SNP*CST
CEB31=SNT*CSF*CSP+SNP*SNP
CEB32=CSF*SNT*SNP-SNP*CSP
CEB33=+CST*CSF
```

C\*\*\*

```
XE=XPK(1)
YE=XPK(2)
ZE=XPK(3)
USPEED=XPK(4)
VSPEED=XPK(5)
WSPEED=XPK(6)
```

C\*\*\*

```
WX=XPK12(7)
WY=XPK12(8)
WZ=XPK12(9)
```

C\*\*\*

```
TLAM=TLAM0+XE/AGLOBE
COST=DCOS(TLAM)
SINT=DSIN(TLAM)
TANT=SINT/COST
SIN2T=2*SINT*COST
COS2T=COST*COST-SINT*SINT
C1111=1.0D0-ZE/AGLOBE-.5D0*EPS2*COS2T
C112=1/C1111
```

C\*

C\*

```

C141=C112*(ZE/AGLOBE+.5*EPS2*COS2T)
C111=(CEB11*USPEED+CEB21*VSPEED+CEB31*WSPEED+WX)/AGLOBE
C211=(CEB12*USPEED+CEB22*VSPEED+CEB32*WSPEED+WY)/AGLOBE
C241=-C112*YE*TANT/AGLOBE
C341=C112*EPS2*SIN2T
C56=OMEGA*(CEB11*COST-CEB13*SINT)
C64=OMEGA*(CEB21*COST-CEB23*SINT)
C45=OMEGA*(CEB31*COST-CEB33*SINT)
C***
C413=OMEGA*(CEB11*SINT+CEB13*COST)
C412=OMEGA*(CEB21*SINT+CEB23*COST)
C411=OMEGA*(CEB31*SINT+CEB33*COST)
CENT1=-OMEGA**2*AGLOBE*C1111*.5*SIN2T
CENT2=-OMEGA**2*AGLOBE*C1111*COST**2
C47=2*(+WR*CEB21-WQ*CEB31)+OMEGA*CEB12*SINT
C48=2*(+WR*CEB22-WQ*CEB32)-C413
C49=2*(+WR*CEB23-WQ*CEB33)-OMEGA*CEB12*COST
C57=2*(-WR*CEB11+WP*CEB31)+OMEGA*CEB22*SINT
C58=2*(-WR*CEB12+WP*CEB32)-C412
C59=2*(-WR*CEB13+WP*CEB33)-OMEGA*CEB22*COST
C67=2*(+WQ*CEB11-WP*CEB21)+OMEGA*CEB32*SINT
C68=2*(+WQ*CEB12-WP*CEB22)-C411
C69=2*(+WQ*CEB13-WP*CEB23)-OMEGA*CEB32*COST
C*
C1122=C112*C112
C2112=C211*C1122
C13=C111*C1122
C11=-EPS2*SIN2T*C13
C31=C111*C112*EPS2*(2*COS2T-C112*EPS2*SIN2T*SIN2T)
C33=C13*EPS2*SIN2T
C21=-EPS2*SIN2T*C2112+C13*(-C1111+.5D0*EPS2*SIN2T*SIN2T)*YE/
1. AGLOBE/COST/COST
C22=-C111*C112*TANT
C23=C2112-C13*TANT*YE/AGLOBE
C14=C141*CEB11
C15=C141*CEB21
C16=C141*CEB31
C24=C241*CEB11+C141*CEB12
C25=C241*CEB21+C141*CEB22
C26=C241*CEB31+C141*CEB32
C34=C341*CEB11
C35=C341*CEB21
C36=C341*CEB31
C17=C141
C27=C241
C28=C141
C37=C341
C411=OMEGA*(CEB31*SINT+CEB33*COST)
C412=OMEGA*(CEB21*SINT+CEB23*COST)
C413=OMEGA*(CEB11*SINT+CEB13*COST)
C433=OMEGA*COST
C43=C433*C413
C53=C433*C412
C63=C433*C411
COST1=COST*OMEGA/AGLOBE

```



```

SINT1=SINT*OMEGA/AGLOBE
C4111=(C1111*COS2T+.5D0*EPS2*SIN2T*SIN2T)*OMEGA*OMEGA
C4112=(C1111*SIN2T-      EPS2*SIN2T*COST*COST)*OMEGA*OMEGA
C41=(WSPEED*C412-VSPEED*C411)/AGLOBE
1-CEB11*C4111+CEB13*C4112+COST1*(WX*CEB12-WY*CEB11)+SINT1*(
2 WY*CEB13+WZ*CEB12)
C51=(USPEED*C411-WSPEED*C413)/AGLOBE
1-CEB21*C4111+CEB23*C4112+COST1*(WX*CEB22-WY*CEB21)+SINT1*(
2 WY*CEB23+WZ*CEB22)
C61=(VSPEED*C413-USPEED*C412)/AGLOBE
1-CEB31*C4111+CEB33*C4112+COST1*(WX*CEB32-WY*CEB31)+SINT1*(
2 WY*CEB33+WZ*CEB32)
C65=-C56
C46=-C64
C54=-C45
FK(1,1)=C11
FK(2,1)=C21
FK(3,1)=C31
FK(4,1)=C41
FK(5,1)=C51
FK(6,1)=C61
FK(2,2)=C22
FK(1,3)=C13
FK(2,3)=C23
FK(3,3)=C33
FK(4,3)=C43
FK(5,3)=C53
FK(6,3)=C63
FK(1,4)=CEB11+C14
FK(2,4)=CEB12+C24
FK(3,4)=+CEB13+C34
FK(1,5)=CEB21+C15
FK(2,5)=CEB22+C25
FK(3,5)=+CEB23+C35
FK(1,6)=CEB31+C16
FK(2,6)=CEB32+C26
FK(3,6)=+CEB33+C36
FK(5,4)=-WR+C54
FK(6,4)=WQ+C64
FK(4,5)=WR+C45
FK(6,5)=-WP+C65
FK(4,6)=-WQ+C46
FK(5,6)=WP+C56

```

C\*

C\*CALLING THE SUBROUTINE FOR COMPUTATION OF THE STATE TRANSITION MATRIX

C\*\*\*

CALL CSTM(FK,PERCNT,DT,THAT,B60,FKDT,SUME,SUME1,NXP,NTERMS)

DO 600 I=1,NXP

DO 600 J=1,NXP

600 THATT(J,I)=THAT(I,J)

C\*\*\*

DO 701 I=1,NXP

DO 701 J=1,NXP

701 PMK2(I,J)=PMK1(I,J)

C\*\*\*

```

CALL LINV1F(PMK2,NXP,NXP,PINV,IDGT,WKAREA,IER1)
CALL VMULFF(PPK,TMATT,NXP,NXP,NXP,NXP,NXP,PTMATT,NXP,IER2)
CALL VMULFF(PTMATT,PINV,NXP,NXP,NXP,NXP,NXP,AK,NXP,IER3)
DO 601 I=1,NXP
DO 601 J=1,NXP
601 AKT(J,I)=AK(I,J)
DO 602 I=1,NXP
602 DELX(I,1)=XS(I)-XMK1(I)
DO 603 I=1,NXP
DO 603 J=1,NXP
603 DELP(I,J)=PS(I,J)-PMK1(I,J)
CALL VMULFF(AK,DELX,NXP,NXP,1,NXP,NXP,DELXES,NXP,IER4)
DO 604 I=1,NXP
604 XS(I)=XPK(I)+DELXES(I,1)
CALL VMULFF(AK,DELP,NXP,NXP,NXP,NXP,NXP,AKDELP,NXP,IER5)
CALL VMULFF(AKDELP,AKT,NXP,NXP,NXP,NXP,NXP,ADPAT,NXP,IER6)
DO 605 I=1,NXP
DO 605 J=1,NXP
605 PS(I,J)=PPK(I,J)+ADPAT(I,J)
C***
IF(KSTEP1.LT.5) GOTO 253
KSTEP1=0
DO 251 I=1,NXP
DO 252 J=1,NXP
IF(I.LE.J) GOTO 252
PS(I,J)=.5D0*(PS(I,J)+PS(J,I))
PS(J,I)=PS(I,J)
252 CONTINUE
251 CONTINUE
253 CONTINUE
C***
DO 711 I=1,NXP
711 XS1(I)=XS(I)
DO 712 I=1,NXP
DO 712 J=1,NXP
712 PS1(I,J)=PS(I,J)
KSTPG=KSTEP
XS1(7)=XPK12(7)
XS1(8)=XPK12(8)
XS1(9)=XPK12(9)
DO 803 I=7,9
DO 803 J=1,9
803 PS1(I,J)=PPK12(I,J)
DO 804 I=1,6
DO 804 J=7,9
804 PS1(I,J)=PPK12(I,J)
XS1(10)=XPK12(10)
XS1(11)=XPK12(11)
WRITE(17,KSTPG) (XS1(I),I=1,11)
1,((PS1(I,J),I=1,9),J=1,9)
C***COPY K-AREAS INTO (K+1)-AREAS I.E. INTO 'PREVIOUS' AREA,
C***--GOING FROM END TO BEGINNING OF FILE.
DO 631 I=1,NXP
DO 631 J=1,NXP
631 PMK1(I,J)=PMK(I,J)

```

```
      DO 632 I=1,NXP
632  XMK1(I)=XMK(I)
C***
      GOTO 301
C***
C***
311  CONTINUE
C***
C***
      GOTO 1
92  CONTINUE
      STOP
      END
      BLOCK DATA
      IMPLICIT REAL*8 (A-H,O-$)
      COMMON/DAT0/PERCNT,DT,TLAM0,OMEGA,AGLOBE,EPS2,IDGT,NSTEP,NXP,SOF
      LOGICAL SOF
      DATA SOF/ .FALSE. /,NSTEP/60/,NXP/6/
      1,PERCNT/.000001D0/,DT/1.0D0/
      2,IDGT/3/
      3,TLAM0/.700D0/
      4,OMEGA/.0000728D0/,AGLOBE/20940000.0D0/,EPS2/.0067D0/
      END
```

C\*\*\*THIS PROGRAM CREATES A NON-DIRECT-ACCESS-DATA-FILE FOR XAS OR  
C\*\*\*XBS FOR OUTPUT OR FURTHER PROCESSING

```

C*
  DIMENSION J(15),Z(11)
1  ,RDME(7),XDME(7),YDME(7),ZDME(7)
  COMMON/DAT0/SOF,J,NSTEP,N,NAMES,TLAM0,AGLOBE
1  ,EPS2,SMEW0,ISTDME,XST(7),YST(7),ZST(7)
  INTEGER FILE(2)
  DIMENSION NAMES(38),NAMES1(38),XS(11),PS(9,9),SUM(14),STDZ(10)
1  ,BIAS(11),SUM1(14),TEMP(14)
  LOGICAL GO,SOF
  NAMELIST/INP/FILE
  NAMELIST/OK/GO
  NAMELIST/DAT/SOF,J,NSTEP,N,TLAM0,AGLOBE
1  ,EPS2,SMEW0,ISTDME,XST,YST,ZST
C***
  DEFINE FILE 10(60,368,L,KSTEP1)
C***
1  CONTINUE
  PRINT 1002
1002 FORMAT(1H,'TYPE &INP FILE= &END')
  READ(5,INP)
  INF1=FILE(1)
  INF2=FILE(2)
  PRINT 2000,FILE
2000 FORMAT(2I10)
  PRINT 1004
1004 FORMAT(1H,'TYPE &DAT DATA= &END')
  READ(INF1,DAT)
  IF(SOF)GOTO 92
  PRINT 1003
1003 FORMAT(1H,'IF EVERYTHING O.K. TYPE &OK GO=.TRUE.&END')
  GO=.TRUE.
  READ(5,OK)
  IF(GO)GOTO 10
  GOTO 1
10 CONTINUE
C***
  DO 331 I=1,14
  SUM1(I)=0.
331 SUM(I)=0.
C***
  DO 991 J1=1,NSTEP
  KSTEP1=J1
  READ(10,KSTEP1)(XS(I),I=1,11)
1,((PS(I,J7),I=1,9),J7=1,9)
C***
  COST=COS(TLAM0+XS(1)/AGLOBE)
  XS(2)=XS(2)/COST
C***
  DO 302 I=1,9
  DO 302 J8=1,9
  IF(PS(I,J8).LT.0.)PS(I,J8)=100.
302 PS(I,J8)=SQRT(PS(I,J8))
C***

```

```

      WRITE(11) (XS(I), I=1, 9)
C***
      READ(14) (Z(I3), I3=1, 11)
      IF(NSTEP.GT.150) GOTO 923
      WRITE(12, 903) J1, (XS(I), I=1, 6), (PS(I, I), I=1, 6)
903  FORMAT(' ', I10, 12F10.3)
      WRITE(12, 905) J1, (XS(I), I=7, 9), (PS(I, I), I=7, 9)
905  FORMAT(' ', I10, 6F20.3)
      923 CONTINUE
C***NOT TO WASTE TDISK SPACE, WHILE ACTUALLY PROCESSING
C****
      ... USPD=XS(4)
      ... VSPD=XS(5)
      ... WSPD=XS(6)
      ... XE=XS(1)
      ... YE=XS(2)*COST
C***XS(2) HAS BEEN REDEFINED AT THE BEGINNING OF THIS PROGRAM.
      ZE=XS(3)
      VAIR=SQRT(USPD**2+VSPD**2+WSPD**2)
      ALPHA=57.3*ATAN2(WSPD, USPD)
      BETA=57.3*ATAN2(VSPD, USPD)
      HM=-ZE
C***
      IF(J1.EQ.1) PRINT 931, XS(1), XS(2)
931  FORMAT(' ', 2F10.0)
C***
      IF(NSTEP.GT.150) GOTO 921
C***
      TLAM=TLAM0+XE/AGLOBE
      COST=COS(TLAM)
      SINT=SIN(TLAM)
      SNEW=SNEW0+YE/AGLOBE/COST
      COSS=COS(SNEW)
      SINS=SIN(SNEW)
      C1111=1.-.5*EPS2*COS(2*TLAM)
      AC1111=AGLOBE*C1111
      DO 301 I=1, ISTDME
      XDME(I)=AC1111*COST*COSS-(-ZST(I)+AGLOBE*(1.-.5*EPS2*COS(2*XST(I))
1) ) *COS(XST(I)) *COS(YST(I))
      YDME(I)=AC1111*COST*SINS-(-ZST(I)+AGLOBE*(1.-.5*EPS2*COS(2*XST(I))
1) ) *COS(XST(I)) *SIN(YST(I))
      ZDME(I)=AC1111*SINT-(-ZST(I)+AGLOBE*(1.-.5*EPS2*COS(2*XST(I))
1) ) *SIN(XST(I))
      RDME(I)=SQRT(XDME(I)**2+YDME(I)**2+ZDME(I)**2)
C*
C*      RDME(I)=SQRT((XE-XST(I))**2+(YE-YST(I))**2+(ZE-ZST(I))**2)
C*
      301 CONTINUE
C***
      WRITE(15, 912) J1, Z(4), VAIR, Z(5), ALPHA, Z(6), BETA, Z(7), HM
1, Z(8), RDME(1), Z(9), RDME(2), XS(7), XS(8), (PS(I, I), I=1, 6)
C*****PRINT 911, J1, Z(4), VAIR, Z(5), ALPHA, Z(6), BETA, Z(7), HM
C*****1, Z(8), RDME(1), Z(9), RDME(2), XS(7), XS(8)
911  FORMAT(I4, F4.0, F4.0, 4F4.1, 2F6.0, 4F8.0, 2F4.0)
912  FORMAT(' ', I5, 2F5.0, 4F4.1, 2F6.0, 4F8.0, 2F4.0, 4X, 3F6.0, 4X, 3F5.1)

```

C\*\*\*

```

TEMP( 1)=Z( 4)-VAIR
TEMP( 2)=Z( 5)-ALPHA
TEMP( 3)=Z( 6)-BETA
TEMP( 4)=Z( 7)-HM
TEMP( 9)=Z( 8)-RDME(1)
TEMP(10)=Z( 9)-RDME(2)
TEMP( 5)=XS(7)
TEMP( 6)=XS(8)
TEMP( 7)=XS(10)
TEMP( 8)=XS(11)
DO 951 I51=1,10

```

```

SUM1(I51)=SUM1(I51)+TEMP(I51)

```

```

951 SUM(I51)=SUM(I51)+TEMP(I51)**2

```

```

GOTO 922

```

```

921 CONTINUE

```

```

WRITE(15,913) J1,Z(4),VAIR,Z(5),ALPHA,Z(6),BETA,Z(7),HM

```

```

1,Z(8),XS(1),Z(9),XS(2),XS(7),XS(8)

```

```

913 FORMAT(' ',I5,2F5.0,4F4.1,2F6.0,4F8.0,2F4.0,4X,18X,4X,15X)

```

```

C*****PRINT 911,J1,Z(4),VAIR,Z(5),ALPHA,Z(6),BETA,Z(7),HM

```

```

C*****1,Z(8),XS(1),Z(9),XS(2),XS(7),XS(8)

```

```

922 CONTINUE

```

C\*\*\*\*

```

C*****PRINT 996,J1,(XS(I),I=1,6)

```

```

996 FORMAT(' ',I7,6F10.3)

```

```

C*****PRINT 997,J1,(XS(I),I=7,9)

```

```

997 FORMAT(' ',I7,3F20.3)

```

```

991 CONTINUE

```

C\*\*\*

```

IF(NSTEP.GT.60) GOTO 953

```

```

DO 952 I=1,8

```

```

BIAS(I)=SUM1(I)/60

```

```

TEMP2=SUM(I)/59-BIAS(I)**2

```

```

IF(TEMP2.LT.0.) TEMP2=100.

```

```

952 STDZ(I)=SQRT(TEMP2)

```

```

BIAS( 9)=SUM1( 9)/60

```

```

BIAS(10)=SUM1(10)/60

```

```

TEMP3=SUM( 9)/59-(BIAS( 9)+BIAS(7))**2

```

```

TEMP4=SUM(10)/59-(BIAS(10)+BIAS(8))**2

```

```

IF(TEMP3.LT.0.) TEMP3=100.

```

```

IF(TEMP4.LT.0.) TEMP4=100.

```

```

STDZ( 9)=SQRT(TEMP3)

```

```

STDZ(10)=SQRT(TEMP4)

```

```

WRITE(15,914) (PS(I,I),I=1,6),(STDZ(I1),I1=1,4),STDZ(9),STDZ(10)

```

```

914 FORMAT(' ',F10.0,2F10.1,3F10.0,4X,F10.0,2F10.1,3F10.0)

```

```

PRINT 915,(BIAS(I),I=1,4),BIAS(9),BIAS(10),(STDZ(I1),I1=1,4)

```

```

1,STDZ(9),STDZ(10)

```

```

915 FORMAT(' ',F6.0,2F6.1,3F6.0,7X,F6.0,2F6.1,3F6.0)

```

```

953 CONTINUE

```

```

ENDFILE 12

```

```

ENDFILE 15

```

C\*\*\*

```

PRINT 995,(PS(I,I),I=1,6)

```

```

995 FORMAT(' ',6F10.3)

```

```

C*** IS THERE ANOTHER RUN TO BE GENERATED?

```

```
GOTO 1
92 CONTINUE
STOP
END
BLOCK DATA
COMMON/DAT0/SOF,J,NSTEP,N,NAMES,TLAM0,AGLOBE
1 ,EPS2,SMEW0,ISTDME,XST(7),YST(7),ZST(7)
DIMENSION J(15),NAMES(38)
LOGICAL SOF
DATA SOF/.FALSE. /,J/38,2,23,5,26,6,27,14,24,15,25,29,18,2*0/,
ANSTEP/60/,N/13/
B,TLAM0/.700/,AGLOBE/20940000./
C,ISTDME/2/,XST/.703,.6985,5*.706/,YST/-1.297,-1.2985,5*-1.294/
D,ZST/7*0./,EPS2/.0067/,SMEW0/-1.300/
1,NAMES/'DME1','CLDE',' Q ',' NZ ',' WHDA',' PEDR',' BETA',' P '
2,' R ',' NY ',' NX ',' ALFA',' DME2',' HADT',' LEDF',' TRDE',' THET'
3,' V ',' PSI ',' PHI ',' TRDR',' TRDA',' PODE',' PODT',' PODF',' PODA'
4,' PODR',' VOR1',' HBAR',' ALS ',' LMLS',' GMLS',' VOR2',' INDF',' HDIG'
5,' LGHT',' MDSW',' TIME'/
END
```

## APPENDIX C

### COMPUTER SYSTEMS FOR PREPROCESSING AND POST-FLIGHT DATA REDUCTION

Post-flight data handling begins using the HP 1000 digital computer located at Princeton University's Gas Dynamics Laboratory. The raw data is transferred to a 9-track, 1600 BPI magnetic tape that can be processed on either the IBM 4341 or the IBM 3033 computer. The following block-diagram summarizes the described procedure:

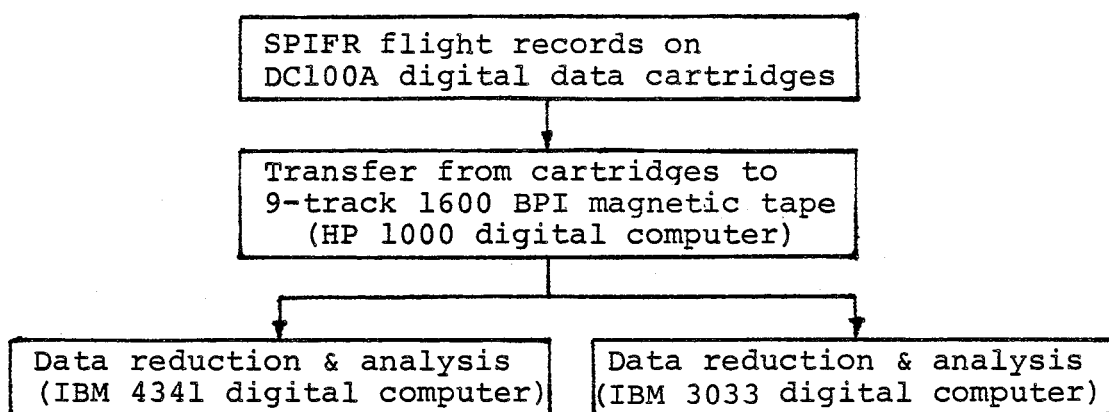


Figure C-1. Data Reduction Procedure.

The FORTRAN program CAT9 controls the transfer from the DC100A cartridges to the 9-track magnetic tape. The FORTRAN program RAWY1 converts 16-bit binary-formatted data into IBM-compatible decimal integer format and arranges the data in physical time vectors. The FORTRAN program SPIFY1 completes the preprocessing by converting the decimal integer time vectors into voltage and then into engineering units, also



converting Indicated Air Speed (IAS) to True Air Speed (TAS).

The SPIFR data storage policy is to preserve both the raw flight-test data and the preprocessed data on magnetic tapes (9-track, 1600 BPI), which makes it compatible for further analysis on both the IBM 4341 and the IBM 3033 machines. Thus, two copies of the raw integer data (RAWY1 output file) and one copy with engineering unit time-vectors (SPIFY1 output file)-for further processing (analysis, tabular printouts or plotting) are preserved.

# TRANSFER FROM CARTRIDGES TO TAPE

&CAT9 T=00004 IS ON CR00005 USING 00012 BLKS R=0000

```
0001 FTN4,L
0002 PROGRAM CAT9(3,99), VERSION OF 4 JUNE 1981
0003 C
0004 C PROGRAM TO COPY BINARY DATA FROM CASSETTE TO IBM COMPATIBLE
0005 C TAPE DRIVE.
0006 C
0007 C LOADING THE PROGRAM
0008 C :RU,LOADR,*F4X,%CAT9
0009 C
0010 C RUNNING THE PROGRAM
0011 C :RU,CAT9,P1,P2
0012 C WHERE P1 - IS THE LOGICAL UNIT NUMBER OF YOUR TERMINAL
0013 C P2 - IS THE LOGICAL UNIT NUMBER OF THE MAG TAPE
0014 C
0015 C
0016 C INTEGER Ibuff(128),IMORE,ISTAT,ITLOG,PARMS(5),NBLCK
0017 C EQUIVALENCE (PARMS(1),LUCRT),(PARMS(2),MTLU)
0018 C CALL RMPAR(PARMS)
0019 C NBLCK=0
0020 C***READ FROM LEFT CARTRIDGE LU 4
0021
0022 21 CONTINUE
0023 CALL EXEC(1,100B+4,IBUFF,128)
0024 C GET STATUS
0025 CALL ABREG(ISTAT,ITLOG)
0026 WRITE(LUCRT,47)ITLOG
0027 47 FORMAT(I10)
0028 C CHECK FOR END OF FILE
0029 IF(IAND(ISTAT,200B).EQ.200B) GO TO 22
0030 C CHECK FOR END OF TAPE
0031 IF(IAND(ISTAT,40B).EQ.40B) GO TO 22
0032 C CHECK FOR END OF DATA
0033 IF(IAND(ISTAT,2).EQ.2)GO TO 22
0034 C***WRITE TO TAPE
0035 CALL EXEC(2,100B+MTLU,IBUFF,128)
0036 NBLCK=NBLCK+1
0037 WRITE(LUCRT,31)NBLCK
0038 31 FORMAT(I7)
0039 GOTO 21
0040 22 CONTINUE
0041 IF(ITLOG.LT.128) GO TO 41
0042 CALL EXEC(2,100B+MTLU,IBUFF,128)
0043 NBLCK=NBLCK+1
0044 WRITE(LUCRT,31)NBLCK
0045 41 WRITE(LUCRT,23)
0046 23 FORMAT('PLUG IN NEXT CARTRIDGE AND TYPE 1 OR IF LAST-TYPE 0')
0047 READ(LUCRT,*)IMORE
0048 IF(IMORE.EQ.1)GOTO 21
0049 C WRITE TWO CONSECUTIVE END OF FILE MARKS
0050 CALL EXEC(3,0100B+MTLU)
0051 CALL EXEC(3,0100B+MTLU)
0052 STOP
```

# PREPROCESSING - STEP I

FILE: RAWY1      FORTRAN    A1    PRINCETON UNIVERSITY TIME-SHARING SYSTEM

```

COMMON/DAT0/SOF,NB
LOGICAL GO,SCF
NAMELIST/INP/FILE
INTEGER*2 A3(1200),A2(1700,38)
INTEGER*2 DATA(128)
LOGICAL*1 DALOG(256)
LOGICAL*1 SWLOG(256)
INTEGER*2 DATA1(128)
INTEGER*2 DATA2(128)
EQUIVALENCE (DATA(1),DALOG(1)),(SWLOG(1),DATA1(1))
INTEGER FILE(2)
NAMELIST/OK/GO
NAMELIST/DAT1/SCF,NB
C***
1 CONTINUE
PRINT 1002
1002 FORMAT(1H,'TYPE 8INP FILE= 8END')
READ(5,INP)
INF1=FILE(1)
INF2=FILE(2)
PRINT 2000,FILE
2000 FORMAT(2I10)
PRINT 1004
1004 FORMAT(1H,'TYPE 8DAT DATA= 8END')
READ(INF1,DAT)
IF(SOF)GOTO 92
PRINT 1003
1003 FORMAT(1H,'IF EVERYTHING O.K. TYPE 8OK GO=.TRUE.8END')
GO=.TRUE.
READ(5,OK)
IF(GO)GOTO 10
GOTO 1
10 CONTINUE
C***
I1=0
I2=0
C***
READ(15,17)DATA
DO 28 I=1,255,2
SWLOG(I)=DALCG(I+1)
SWICG(I+1)=DALOG(I)
28 CONTINUE
GOTO 32
C***
99 CONTINUE
DO 30 I=1,128
30 DATA2(I)=DATA1(I)
READ(15,17,END=100)DATA
17 FORMAT(128A2)
DO 29 I=1,255,2
SWLOG(I)=DALCG(I+1)
SWICG(I+1)=DALOG(I)
29 CONTINUE
C***
DO 31 I=1,128

```

[illegible]

# PREPROCESSING - STEP II

FILE: SPIFY1    FORTRAN    A1    PRINCETON UNIVERSITY TIME-SHARING SYSTEM

```

COMMON/DAT0/SOF,VSLOPE,VCONST,PHSLOP,PHCONS,N11,DPNSTD
INTEGER FILE(2)
DIMENSION A3(1700,38),PHSLOP(55),PHCONS(55)
INTEGER*2 A2(1700,38)
LOGICAL GO,SOF
NAMELIST/INP/FILE
NAMELIST/OK/GO
NAMELIST/DAT/SOF,VSLOPE,VCONST,PHSLOP,PHCONS,N11,DPNSTD
1 CONTINUE
PRINT 1002
1002 FORMAT(1H,'TYPE &INP FILE= &END')
READ(5,INP)
INF1=FILE(1)
INF2=FILE(2)
PRINT 2000,FILE
2000 FORMAT(2I10)
PRINT 1004
1004 FORMAT(1H,'TYPE &DAT DATA= &END')
READ(INF1,DAT)
IF(SOF)GOTO 92
PRINT 1003
1003 FORMAT(1H,'IF EVERYTHING O.K. TYPE &OK GO=.TRUE.&END')
GO=.TRUE.
READ(5,OK)
IF(GO)GOTO 10
GOTO 1
10 CONTINUE
C***
DO 501 J=1,38
501 READ(9)(A2(I,J),I=1,N11)
C***NOW-INTO REAL PHYSICAL DATA.
DO 512 I=1,N11
ISIGN=0
IF(A2(I,1).LT.0)ISIGN=1
C***65535=2**16-1,BECAUSE IF LEFTMOST OF THE 16-ZEROS-AND-ONES-FIELD
C***IS ONE,IT ITSELF IS INTERPRETTED AS MINUS AND EACH OF THE OTHER
C***15 BITS IS CHANGED(ONES TO ZEROS AND ZEROS TO ONES).
C***THUS,E.G.,A 16-ONES-FIELD IS INTERPRETTED AS -0 INSTEAD OF 2**16-1
C***AND A ONE FOLLOWED BY 15 ZEROS IS -(2**15-1) INSTEAD OF 2**15
512 A3(I,1)=A2(I,1)+ISIGN*65535
DO 502 I=1,N11
DO 503 J=2,12
ISIGN=0
IF(A2(I,J).LT.0)ISIGN=1
503 A3(I,J)=((A2(I,J)+ISIGN*65535)*VSLOPE/16.+VCONST)*PHSLOP(J)+
1PHCONS(J)
502 CONTINUE
C***
DO 521 I=1,N11
ISIGN=0
IF(A2(I,13).LT.0)ISIGN=1
521 A3(I,13)=A2(I,13)+ISIGN*65535
DO 522 I=1,N11
DO 523 J=14,34
ISIGN=0

```

```

      IF (A2(I,J).LT.0) ISIGN=1
523  A3(I,J)=(((A2(I,J)+ISIGN*65535)*VSLOPE/16.+VCONST)*PHSLOP(J)+
      1PHCONS(J))
522  CONTINUE
C***
      DO 514 I=1,N11
      DO 515 J=35,38
      ISIGN=0
      IF (A2(I,J).LT.0) ISIGN=1
515  A3(I,J)=A2(I,J)+ISIGN*65535
514  CONTINUE
C***
      DO 591 I=1,N11
591  IF (A3(I,19).LT.0.) A3(I,19)=A3(I,19)+360.
C***
      DO 601 I=2,N11,2
601  A3(I,1)=A3(I,13)
      DO 602 I=3,N11,2
602  A3(I,1)=.5*(A3(I-1,1)+A3(I+1,1))
      A3(1,1)=A3(2,1)
      N111=N11-2
      DO 603 I=2,N111,2
603  A3(I,13)=.5*(A3(I-1,13)+A3(I+1,13))
      A3(N11,13)=A3(N11-1,13)
C***
C***PRAT=PRATIO;RRAT=RRATIO
      DO 611 I=1,N11
      PRAT=(A3(I,29)+DPNSTD)/1013.3
      RRAT=PRAT**.81
      A3(I,18)=1.689*A3(I,18)/SQRT(RRAT)
      HCONST=EXP(ALOG(PRAT)/5.256)
      A3(I,29)=(1-HCONST)/.00000689
611  CONTINUE
C***
C***NOT TO LOSE ACCURACY,THE TIME VECTORS ARE STORED UNFORMATTED,I.E.
C***USING UNFORMATTED READ(AND WRITE WHEN RETRIEVING FOR FURTHER
C***PROCESSING).
      DO 121 J=1,38
121  WRITE(10)(A3(I,J),I=1,N11)
      ENDFILE 10
C***IS THERE ANOTHER RUN TO BE GENERATED?
      GOTC 1
92  CONTINUE
      STOP
      END
      BLOCK DATA
      COMMON/DAT0/SOF,VSLOPE,VCONST,PHSLOP,PHCONS,N11,DPNSTD
      DIMENSION PHSLOP(55),PHCONS(55)
      LOGICAL SOF
      DATA SOF/.FALSE./,VSLOPE/.004884/,VCONST/-10./,
      1PHSLOP/1.,1.6583,-2.7604,-.20555,-8.2085,.2557,
      2-3.0754,4.0811,-3.4664,-.05184,.05519,2.8611,
      31.,.0508,.1020,-5.,3.1338,5.0623,
      418.2787,-8.1864,5.,-5.,2.4703,.0513,
      55.1310,-1.9589,2.4074,1.,15.275,2.8611,

```

6.25,.10,1.,.1,1.,3*1.,	SE
717*1./,	SI
8PHCONS/0.,-3.2009,.458,-.02467,-.5304,.1055,	SE
9-.1019,-.0427,-.2048,-.0019,-.01233,13.7125,	SI
A0.,.492,-.0017,0.,.3805,99.9689,	SE
B.0984,-.4821,0.,0.,-4.0193,.513,	SI
C-23.8869,1.5698,3.5703,0.,950.,13.7125,	SI
D0.,0.,0.,0.,0.,0.,0.,0.,	SI
E17*0./,	SI
FN11/10/	SE
G,DENSTL/0./	SE
END	SE

## APPENDIX D

### INTEGRATION OF DISTANCE MEASURING EQUIPMENT (DME) INTO THE DATA COLLECTION SYSTEM

The DME component of the navigation/communication system has been integrated into the onboard experimental setup with the capability to sequence automatically available navigation stations and process the distance information using microprocessor control. The navigation/communication (NAV/COM) and the DME are part of the Bendix "BX-2000" product line of aircraft avionics. A digital information format is used in the Bendix NAV/COM and DME for frequency tuning. The DME receiver output to the pilot's indicator is a pulse-width signal which is compatible with digital processing techniques.

This appendix is sub-divided into sections relating to the external (microprocessor) tuning, distance signal decoding, and an overview of the DME system and specifications. The first two sections are specific to the Bendix system.



## D-1. EXTERNAL DME TUNING

The Bendix DM-2031A DME receiver/transmitter has provisions for both "2 out of 5" tuning which is compatible with other manufacturers systems and a serial binary-coded-decimal (BCD) tuning. The serial tuning method is used by the Bendix NAV/COM and is implemented in the microprocessor tuning for compatibility. When the Bendix DME is installed with the Bendix NAV/COM, the DME serial tuning signal is the same one which is used for tuning the NAV receivers. As shown in Figure D-1, a switch located on the NAV/COM (Bendix CN-2011A) permits the pilot to select DME tuning paired with either NAV 1 or NAV 2. In the center-off or hold (H) position, no tuning signal is sent to the DME. Under this condition the DME continues to hold the last tuning selection and station frequency. The tuning signal contains a BCD format of the paired NAV frequency. (The NAV frequency is not the actual frequency used in the DME system, as will be explained in the overview section.)

The tuning signal is in the form of a twenty-bit asynchronous pulse-width modulated serial word. The serial data word format is shown in Figure D-2. The basic period of each word is 4.0 msec, and when supplied by the NAV/COM; the word rate is 250 Hz. However, a single word is sufficient to tune the DME. Note that the same format is used for the COM, NAV, DME and GS (glide slope) units in the Bendix product line. The first bit in the word is the synchronizing pulse. Each bit after the first is dedicated to a specific piece of information. The value of bits 2 through 7 is ignored in the current DME, but future units may use these bits as a device code.

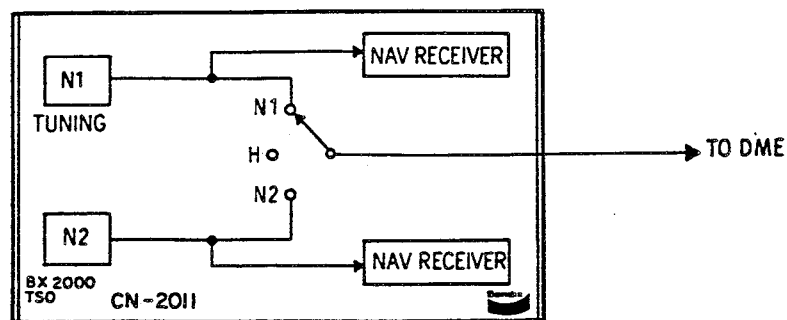


Figure D-1. DME Tuning Via NAV/COM.

	SYN <sub>C</sub>	TEST	X	TX	X	X	X	2	1	8	4	2	1	8	4	2	1	4	2	1
COM																				
NAV/GS		X	X	X	X	X	X	2	1	8	4	2	1	8	4	2	1	4	2	1
DME		X	X	X	X	X	X	2	1	8	4	2	1	8	4	2	1	4	2	1
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20

4.0 MILLISECONDS

0.25 MHz (COM ONLY)  
0.1 MHz

Figure D-2. Serial Data Word Format.

The bit format is shown in Figure D-3. Synchronization, logic "1", and logic "0" bits correspond to 150-, 100- and 50-microsecond duration pulses respectively. The decoder inside the DME (as well as NAV, COM and GS) is relatively tolerant of the actual pulse width (and word length) of the incoming signal. As mentioned previously, the synchronizing pulse (bit 1) indicates the beginning of the serial data word. During the synchronizing pulse, the signal level stays at logic 1 for 150 microseconds (nominal). The Bendix circuitry samples each bit at 125 microseconds to determine if that bit is the synchronizing pulse. A similar sample is made at 75 microseconds to differentiate logic 1 and logic 0 pulses. Hence, the minor variation in the pulse widths of the tuning signal will not compromise the proper functioning of the system.

A microprocessor software program which generates the bit pulses and data word format to tune the DME was written using simple software timing loops. This program was verified using an oscilloscope to check the pulse widths and data word format. Software programming of the station sequencing was not completed in time for implementation on the test program. The alternative tuning method to be described latter is an interim solution.

Electrical (hardware) interfacing for microprocessor tuning output to the DME input is shown in Figure D-4. A signal inversion is employed at the NAV/COM's DME tuning signal output (this was not shown in Figure D-1 for clarity) and the signal is again inverted at the DME. Thus, the signals on the interconnecting wires are inverted with respect to Figure D-3. The high level (pull-up) voltage

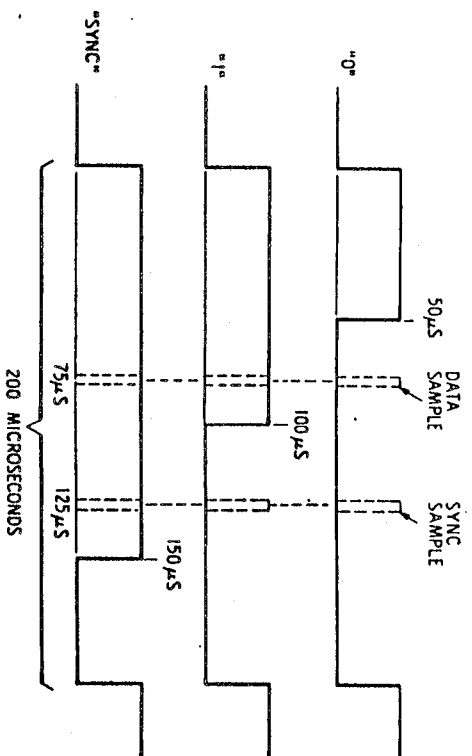


Figure D-3. Bit Format.

is 12 to 15 volts. An open collector buffer, preferably with a 12 volt pull-up, may be used at the microprocessor side of the interface.

The alternative tuning method used in the current testing also is shown in Figure D-4. A switch located on the avionics section of the instrument panel allows the pilot to select normal NAV/COM (N) tuning or remote microprocessor (EXT) tuning. In the EXT position either the NAV 1 or NAV 2 tuning signal is routed to the DME, depending on the position of the relay shown. The relay is driven by a discrete digital output of the microprocessor. No changes in software logic were required for this implementation since the relay was driven in parallel with the "computer functioning" light on the instrument panel. The present rate of 0.5 Hz allows sufficient time for DME station lock-on and measurement of distance.

The selection switch N/EXT provides an additional function. In the EXT position, the displayed DME distance available on the one pilot's electronic course deviation instrument (ECDI) is blanked. The primary center panel DME indicator is not blanked, and the microprocessor station tuning of the DME can be verified by the safety pilot. The primary DME indicator can be switched by the safety pilot to display elapsed time or other function during flight tests.

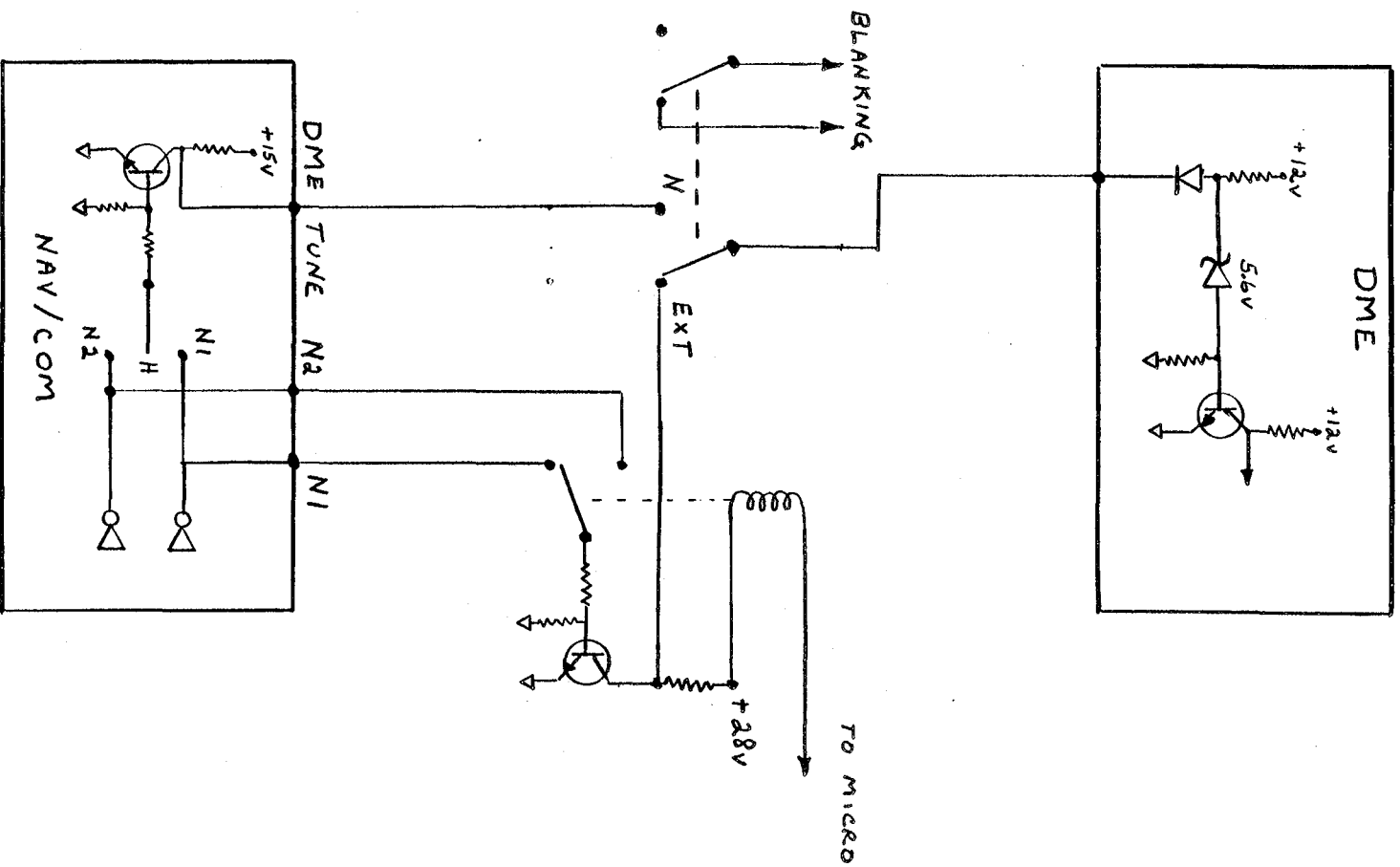


Figure D-4. DME Tuning Electrical Interface.

## D-2. DME DISTANCE SIGNAL DECODING

Three signal outputs are generated by the Bendix DM-2031A DME receiver/transmitter: a pulse pair (RP1 and RP2) and a status signal (SEARCH). The time interval between RP1 and RP2 represents the slant range distance to the DME ground station. The digital logic interface, shown in Figure D-5, processes these three signals upon a DATA READ signal from the microprocessor. The distance represented the difference (RP2 - RP1) is presented to the microprocessor as a 16-bit (2-byte) word. The high-order bit of this data word is used to indicate the DME status (SEARCH).

The difference (RP2 - RP1) is measured by a 16-bit digital counter using a crystal controlled oscillator which operates at a frequency of 18 MHZ. Using the principle that RF energy travels one nautical mile and returns in 12.359 microseconds, the slant range from the aircraft to the ground station can be determined. Since the high-order bit is used for the status SEARCH signal, the maximum distance reading (15 bits) is 147 nautical miles. Although the interface clock frequency of 18 MHZ would suggest a measurement (counter) bit resolution of 27 feet, the actual resolution is determined by the processing within the Bendix DM-2031A. The LSI (large-scale-integration) chip that generates these pulses uses a 1.6 MHZ clock (actually 1.61825 MHZ) which limits the (RP2 - RP1) difference increments to the equivalent of 0.05 nautical miles. Some other factors influencing measurement accuracy are discussed in the overview section.

The digital logic interface is presented in a simplified block diagram form in Figure D-6 for discussion of interface

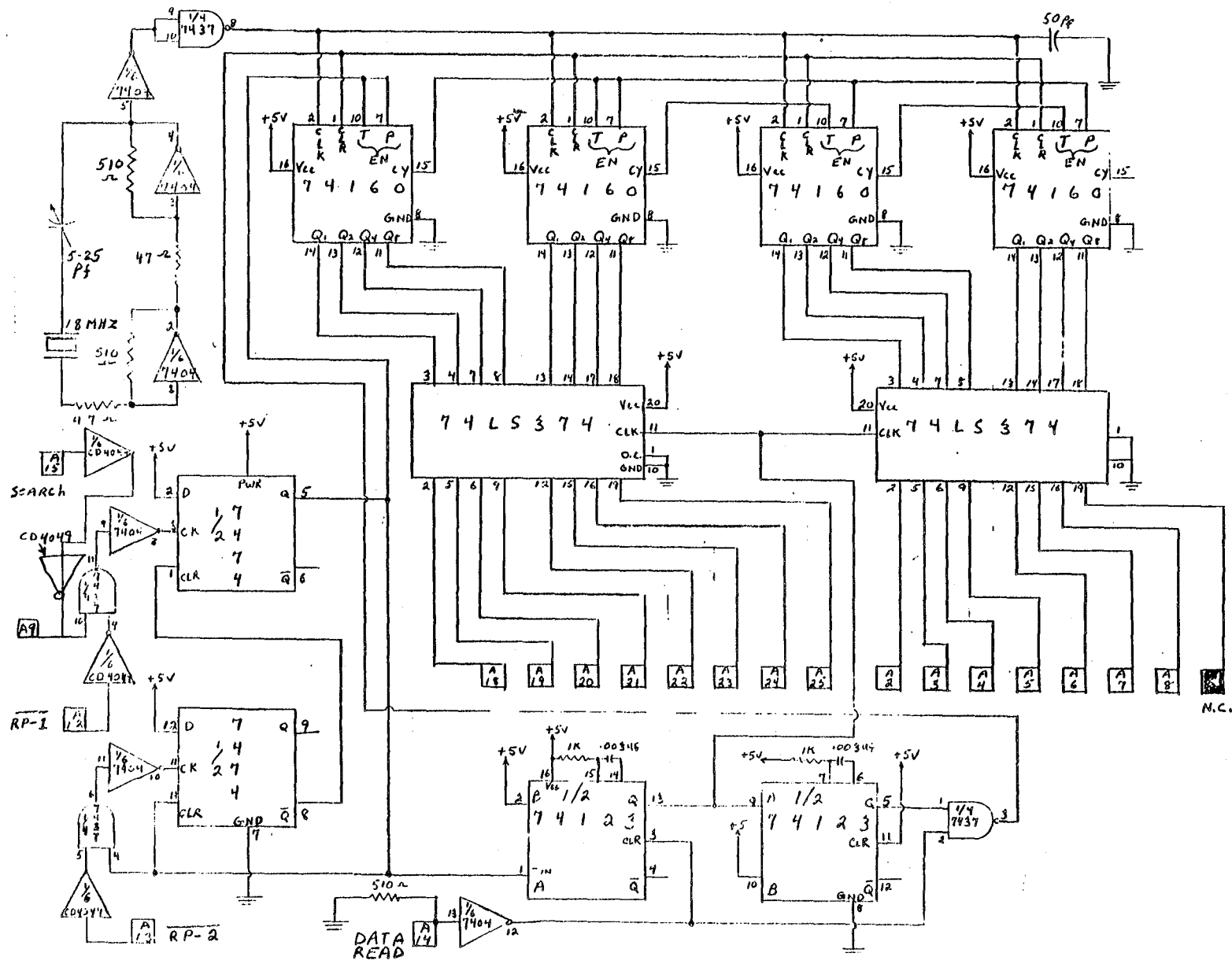


Figure D-5. DME - Microprocessor Electrical Interface.



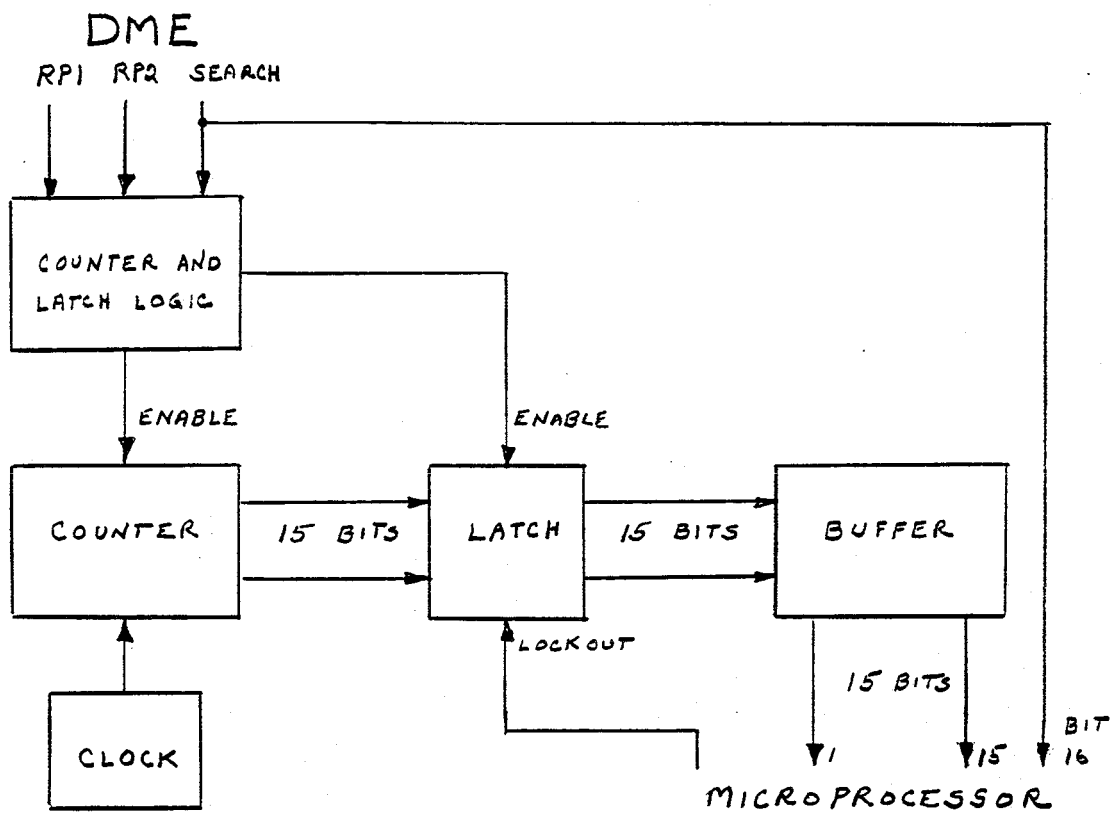


Figure D-6. DME Interface Block Diagram.

operation. The status of SEARCH is used to enable the counter as a precaution, although the absence of pulses RP1 and RP2 would preclude counter operation. The counter is started from a previously cleared (zero) value by the RP1 pulse from the DME. As noted previously, the counter rate is determined by the 18 MHZ reference clock. The count is stopped by the RP2 pulse.

Two other events occur after receipt of RP2. After a very short delay, the count is transferred to the buffer via the latch control; when this operation is completed, the counter is reset or cleared. This chain of events continues to cycle as long as the signal DATA READ is not asserted by the microprocessor data collection system. Counter and buffer updates will take place at a 21 Hz rate during normal DME operation. When the microprocessor generates a DATA READ request, transfer of counter information to the buffer is inhibited. This signal is maintained by the microprocessor until the buffer has been read. This mode of operation guarantees that some data will be available so that the microprocessor will not "hang" in a wait state. The data in the buffer will normally be valid distance information measured within the last .05 sec of receipt of DATA READ. The signals RP1 and RP2 are not the raw pulses used by the DME interrogating a ground station; rather, they are generated by a sophisticated LSI chip. Corrections for delays in turnaround at the ground station and within the Bendix unit are applied so that the  $(RP2 - RP1)$  difference has no bias for true zero distance. Upon loss of the DME station, the  $(RP2 - RP1)$  pulses will continue to be sent by the LSI chip for up to 10 sec. A correction also is made to maintain the same rate of change (groundspeed) as observed

prior to station signal loss. The correction is 80% of the preobserved groundspeed to prevent a "backing up" indication on the pilot's indicator when the signal is reacquired. The consequences of the above and other effects are discussed in the following overview section.

### D-3. DME/DATA COLLECTION OVERVIEW

The purpose of the DME system is to provide the pilot with slant range distance information from the aircraft to a selected DME ground facility. The system transmits interrogation signals in the form of pulse pairs to the selected ground station. The DME ground facility receives the interrogation signal and returns a reply signal (again a pulse pair) for each interrogation received. Multiple aircraft may interrogate the DME ground station.

The DME system operates in the frequency range of 978 MHz to 1212 MHz. There are 200 DME channels which are paired with VHF NAV frequencies between 108.00 MHz and 117.95 MHz (100 "X" channels and 100 "Y" channels). For example DME channel 85X is paired with NAV frequency 113.80 MHz. The aircraft transmits the interrogation pulses at 1109 MHz and receives the reply offset by 63 MHz at 1172 MHz. (Some X channels are offset below the transmission frequency.) On the .05 spacing VHF frequencies such as 113.85 MHz (paired DME channel 85Y) the same transmission frequency is used but the reply is offset opposite to that used for the X channel (1046 MHz). Since some electrical processing delay will take place from receipt of interrogation signal to reply signal, all replies are adjusted to a specific delay to permit accurate measurement of the elapsed time by the airborne distance measuring circuits. This delay is 50  $\mu$ sec for "X" stations and 56  $\mu$ sec for Y stations (measured between the first pulse of interrogation to the first pulse of reply).

The interrogation pulse pairs are spaced at 12  $\mu$ sec for X channels and 36  $\mu$ sec for Y channels. The reply pulse

pairs are 12  $\mu$ sec and 30  $\mu$ sec for X and Y respectively.

The DME ground facility continuously transmits a nominal 2700 pulse pairs per second squitter signal with a 1350 Hz identification morse code signal at 30-second intervals. The 1350 Hz identification signal consists of groups of evenly spaced pulse pairs. The ground station provides a reply pulse pair that replaces a squitter pulse pair 50  $\mu$ sec after receiving an interrogation. The identification signal is available to the pilot as an audio tone to verify tuning and station selection.

When the DME is first tuned to a ground station, it must determine which reply pulses are to its interrogation pulses as opposed to those meant for other aircraft. Old model DME equipment frequently took 20 seconds or longer to achieve a lock-on and track. The Bendix DM-2031A specification for lock-on is less than 1 second. During the search period the interrogation rate is increased to 140 pulse pairs/sec to improve the detection time. This is reduced to 21 interrogations per sec during track. All DME units also use a variable pulse repetition rate to prevent synchronization of distance replies between other DME aircraft interrogators. A random jitter of the interrogation rate about the nominal of  $\pm 1\%$  is used in the Bendix DM-2031A.

The specification measurement accuracy of the Bendix DM-2031A is  $\pm 0.1$  nautical mile or .15 percent, whichever is larger. The minimum indication on the pilot's display of the Bendix DME system is 0.1 nautical mile. The output resolution of the signal to the indicator (RP1 - RP2) pulses is 0.05 nautical mile.

A possible source of error, both at the ground station and in the aircraft processing circuits, is proper pulse delay processing. The DME ground station error specification is  $\pm 0.1$  nautical miles indicating that the pulse delay (50  $\mu$ sec on channel X) is within 1.2  $\mu$ sec. This type of error, at a given ground station, and airborne unit should be predictable and could be removed from the data. Determination of this error is predicated on range measurement of multiple DME stations by the aircraft. A small dynamic error occurs with the data collection system since the measurement time may be in error by the update period (approximately 0.05 sec). In the implementation discussed here, an error due to signal loss is possible. Time difference information can continue up to 10 seconds after signal loss as mentioned previously. With the present scheme of sequencing stations every 2 seconds, the memory circuit is only partially charged, and it is unlikely that a memory generated signal will be obtained.

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1. Report No. NASA CR-165932		2. Government Accession No.		3. Recipient's Catalog No.	
4. Title and Subtitle DEVELOPMENT OF FLYING QUALITIES CRITERIA FOR SINGLE-PILOT INSTRUMENT FLIGHT OPERATIONS: INTERIM REPORT				5. Report Date June 1982	
				6. Performing Organization Code	
7. Author(s) Aharon Bar-Gill, W. Barry Nixon and George E. Miller				8. Performing Organization Report No. MAE-1528	
				10. Work Unit No.	
9. Performing Organization Name and Address Princeton University Department of Mechanical & Aerospace Engineering Flight Research Laboratory Princeton, New Jersey 08544				11. Contract or Grant No. NAS1-15764	
				13. Type of Report and Period Covered Contractor Report Sept.1979 to May 1981	
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Washington, DC 20546				14. Sponsoring Agency Code	
15. Supplementary Notes Langley Technical Monitor: Terrence S. Abbot Interim Report					
16. Abstract  Research is being conducted to develop flying qualities criteria for Single Pilot Instrument Flight Rule (SPIFR) operations. Significant progress has been made with regard to most of the key issues encompassed in the SPIFR research program. The ARA aircraft has been modified and adapted for SPIFR operations. Aircraft configurations to be flight-tested have been chosen and matched on the ARA in-flight simulator, implementing modern control theory algorithms. Mission planning and experimental matrix design have been completed. Microprocessor software for the onboard data acquisition system has been debugged and flight-tested. Flight-path reconstruction procedure and the associated FORTRAN program are at a final stage of development. Work has begun on algorithms associated with the statistical analysis of flight test results and the SPIFR flying qualities criteria deduction.					
17. Key Words (Suggested by Author(s)) Flying qualities criteria;General Aviation; Instrument flight rule;In-flight simulation; Multiple DME scanning;Optimal smoothing; Optimal trajectory reconstruction;Phugoid response;Single pilot operations.			18. Distribution Statement  UNCLASSIFIED-UNLIMITED		
19. Security Classif. (of this report) UNCLASSIFIED		20. Security Classif. (of this page) UNCLASSIFIED		21. No. of Pages 165	
				22. Price	

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